

## Future Carrier-based Tactical Aircraft Study

Jeffrey J. Samuels, Andrew S. Hahn, David R. Schleicher, Samuel B. Wilson III, Kevin B. Carbajal, and Paul A. Gelhausen

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Nomenclature		Medium AW	Medium All-Weather attack aircraft
ACSYNT	AirCraft SYNThesis aircraft design	Medium FW	Medium Flying Wing attack aircraft
	program	Medium IW	Medium Internal Weapons attack
APU	Auxiliary Power Unit		aircraft
ASTOVL	Advanced Short TakeOff and Vertical Landing	MFVT	Mixed Flow/Vectored Thrust propulsion system
ATF	Advanced Tactical Fighter	NASA	National Aeronautics and Space Administration
BCAM	Best Cruise Altitude and Mach number	NFA	Naval Fighter/Attack aircraft
BPR	Bypass Ratio	q	Dynamic Pressure, lb/ft <sup>2</sup>
CAP	Combat Air Patrol	RAM	Radar Absorbing Material
CAS	Close Air Support	RCS	Radar Cross Section
$C_{Do}$	Minimum drag coefficient at zero lift	SEAD	Suppression of Enemy Air Defenses
	based on wing area	SEP	Specific Excess Power (ft/sec)
$C_{Dwet}$	Drag coefficient based on wetted area	SFC	Specific Fuel Consumption
CNA	Center for Naval Analyses		(lbf/(lbt*hr))
DLI	Deck Launched Intercept	SRM	Short Range Missile
DOC	Desired Operational Characteristics	SSF	STOVL Strike Fighter
FPR	Fan Pressure Ratio	STOVL	Short TakeOff and Vertical Landing
HARM	High-speed Anti-Radiation Missile	TAD	Technology Availability Date
LGB	Laser Guided Bomb	TOGW	TakeOff Gross Weight
LRM	Long Range Missile	T/W	Thrust to Weight ratio
M	Mach number	US/UK ASTOVL	United States/United Kingdom ASTOVL Program

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#### **Summary**

This report describes a study of technology trends for several classes of tactical aircraft. Subsonic attack, supersonic fighter, and supersonic multimission classes were designed and then compared in terms of mission capability and fallout range performance. This approach used in this study emphasized consistency so that all aircraft classes can be directly compared in operational utility or cost analysis trends.

Land-based, sea-based, and Short Takeoff and Vertical Landing (STOVL) multimission aircraft were compared to evaluate the influence of technology and mission requirements and to address the impact of aircraft navalization. This study highlights the effect of changing requirements on the penalties associated with STOVL capability and addresses the penalties associated with carrier compatibility. Of course, STOVL and navalization (along with supersonic flight) weight penalties buy additional capability. In a low technology timeframe with no requirement to perform dry supersonic cruise, the STOVL aircraft without hover thrust augmentation was very heavy compared to a mission-equivalent land-based aircraft. However, with advanced technology and a dry supercruise requirement, the

STOVL aircraft with little or no thrust augmentation in hover was much lighter, thus reducing the cost, risk, and/or weight penalties associated with STOVL. With advanced technology, the STOVL aircraft was lighter than the conventional Naval aircraft because the STOVL weight penalties were less than the penalties associated with carrier compatibility.

The subsonic attack aircraft evaluation compared flying wing to conventional designs, single- versus two-place crew, two versus four bombs, and internal versus external weapon carriage. Technology improvements had less effect on the attack aircraft than on the multimission aircraft, due primarily to the lower growth factor of subsonic aircraft. The addition of two more bombs had more impact on the takeoff gross weight than the addition of a second crewmember. Attack aircraft designs with internal weapons are lighter than those with external weapons, given the assumptions and estimates used in this study. This study also identifies the flying wing as the favored concept for attack aircraft and examines the impact of internal weapons carriage for attack aircraft. The flying wing aircraft was lighter than the other four-bomb aircraft mainly because of its reduced drag.

#### Section I - Introduction

The Center for Naval Analyses (CNA) evaluated the future of the carrier task force, including cost and flexibility of operations using different carrier types, tactical aircraft combinations, and operational philosophies. Their study also included different combinations of electronic warfare, anti-submarine warfare, and tactical aircraft, as well as nontraditional air vehicle concepts such as airships, unmanned aerial vehicles, and tilt-rotor tankers. The details of their study involved issues such as deck spotting factor, sortie rates, aircraft availability, mission effectiveness, and affordability. Their findings are reported in reference 1.

In support of the CNA future carrier study, NASA Ames Research Center conducted a conceptual aircraft design study to provide the CNA with a tactical aircraft database. The key to this study is that all of the aircraft were sized with consistent analysis methods, requirements, propulsion modelling, and technology/weight estimates. The study produced an aircraft database which supports evaluations of technology trends, requirement trends, cost, and operational utility. It includes the following data:

Takeoff gross weight

Maneuver performance

Impact of cruise Mach number on Deck Launched Intercept (DLI) mission radius

Impact of number of bombs carried on the Strike mission radius

Impact of loiter time on the Combat Air Patrol (CAP) mission radius

Fallout range on all SSF Desired Operational Characteristics (DOC) missions

Since the CNA was evaluating future carrier force trends, Ames provided them with aircraft developed in two technology timeframes. Mission requirements and aircraft technologies changed between these two timeframes. The first timeframe represents demonstrated technology levels and is referred to in this report as the 1990-TAD (Technology Availability Date) timeframe. The second technology level, referred to as the 1995-TAD timeframe,

uses higher thrust to weight ratio (T/W) engines and advanced materials technologies. Structural weight savings used in this study are conservative compared to those that were agreed upon during the United States/ United Kingdom Advanced Short Takeoff and Vertical Landing (US/UK ASTOVL) program (ref. 2). The assumptions in that study (1986) were the consensus of what technology levels would be demonstrated by 1995. Additional requirements on the aircraft in the 1995-TAD timeframe are low observability (approximately ATF (Advanced Tactical Fighter)-level), nonafterburning supersonic cruise (dry supercruise), and increased maneuver capability. Aircraft using 1990-TAD assumptions have performance that could be expected if aircraft development were started today, while the 1995-TAD designs show what could be expected in the near future. The primary differences between these timeframes are:

Engine technology

Weight of structural material

Supercruise and maneuver requirements

Survivability (Radar Absorbing Material (RAM), internal weapons, stealth planform)

Several aircraft classes were developed so that size and mission effectiveness could be compared between Fighter, Attack, and Multimission aircraft. This study highlights the effect of changing requirements on the Multimission class including the so-called "STOVL penalty" and the impact of the carrier-basing (or navalization) penalty. Several Attack aircraft types were developed to evaluate the impact of crew size, weapons load, internal versus external weapons carriage, and low observables. The study includes the following classes and types of aircraft:

Supersonic Fighter class:

Variable-sweep-wing Fighter (F-14 type)

Subsonic Attack class:

Light (A-4 type)

Medium (A-7 type)

Medium All-Weather (A-6 type) called Medium AW

Medium Internal Weapons (A-3 type) called Medium IW

Medium Flying Wing (A-12 type) called Medium FW

<sup>&</sup>lt;sup>1</sup>The technology availability date is the date at which technologies have been demonstrated and are available for incorporation into full-scale development projects. Currently, first operational capability follows TAD by approximately 10 years.

Supersonic Multimission class:

Land-based MultiRole Fighter (MRF)
Sea-based Naval Fighter/Attack (NFA)
STOVL Strike Fighter (SSF)

Many of the estimates required to size aircraft in this study were difficult to determine accurately. Since the goal of this study was to produce time-based trends for aircraft Takeoff Gross Weight (TOGW), enabling consistent comparisons between aircraft concepts was of more importance than attempting to predict the actual weight of the aircraft in a specific timeframe. Therefore, reasonable estimates were made and applied consistently to all the aircraft for such things as materials technology level, weapon advancement, engine technology, and avionics capabilities/requirements.

In this paper, a distinction is made between aircraft similarities and differentiators. Similarities are estimated technology levels or requirements that are the same for all of the aircraft in a particular class such as Multimission. Differentiators are unique features applied to each aircraft type, such as land-based versus naval Multimission. Aircraft trends found in this study are driven by these differentiators. The similarities and differentiators used in this study are discussed separately in major sections of this paper.

This study was conducted over a four month period by an eight member team in early 1991. The team members were:

Samuel B. Wilson III: technical director

Jeffrey J. Samuels: team leader and aircraft designer

Andrew S. Hahn: chief aircraft designer

David R. Schleicher: aircraft designer

Kevin B. Carbajal: propulsion

J. R. Gloudemans: graphics

Paul A. Gelhausen and Mark D. Moore: ACSYNT

aircraft synthesis code

This aircraft design study was conducted using the NASA Ames aircraft design and synthesis code, ACSYNT (refs. 3–6). ACSYNT was developed in the early 1970s as a flexible conceptual aircraft design and analysis tool. The code has been used at NASA Ames Research Center for a variety of projects and it undergoes continual development through a joint effort by NASA, industry, and academia. ACSYNT is particularly useful for TOGW trends such as those desired by the CNA. ACSYNT was also used to evaluate aircraft TOGW sensitivity to some of the more important aircraft differentiators in this study.

ACSYNT is comprised of several independent analysis codes which have been combined in order to evaluate complete aircraft. These analysis codes are geometry, weights, structures, aerodynamics, propulsion, takeoff performance, and mission performance. ACSYNT includes methodology for determining a design's TOGW for a given mission. An optimization module is coupled to ACSYNT to provide an automatic closed-loop optimization of the vehicle. Designs are optimized for a particular objective function, typically minimum TOGW, while being subject to user-defined constraints. Numerous correlation studies with existing aircraft have been performed and they have shown ACSYNT to be extremely accurate (ref. 7). ACSYNT is useful for determining critical technology items and showing aircraft trends (refs. 8 and 9).

#### Section II - Aircraft Similarities

This section describes the consistent practices and estimates that were applied to all of the aircraft classes during the design process. Design rules or requirements that are unique to a specific aircraft class or aircraft type are discussed later.

#### A. Geometry

The aircraft in this study were based on existing aircraft and limited to only a few geometries. This was done to eliminate differences in ACSYNT's weight and aero-dynamic predictions for aircraft components that were not important drivers in the study (different locations for the horizontal stabilizer, for example). The information presented below is summarized in table 1.

Aircraft length and folded wing span were limited to 64 ft and 34 ft, respectively, to ensure that the aircraft could fit onto a carrier. These constraints only affected the largest SSF aircraft. The minimum allowed fuselage diameter<sup>2</sup> was 4.5 ft for packaging the cockpit and engines. Several of the smaller Attack aircraft were constrained by this limit. Conventional wing planforms have a minimum tip chord of 24 inches for carrying the Short Range Missile (SRM) on the wing tip.

For the Fighter class, the fuselage was based on the F-18 with nose, afterbody, and overall fineness ratios of 5.0, 3.0, and 10.0, respectively. The wing and tail planforms and the tail area ratios were based on an F-14. The vertical and horizontal tails were sized as a fixed percentage of the wing area.

Subsonic Attack aircraft fuselages were optimized by allowing both length and maximum diameter to vary, but they all have the same nose and afterbody fineness ratios based on the A-6 (1.5 and 5.13, respectively). Attack aircraft wing planforms were optimized, while the tail planforms and volume coefficients were based on the A-6.

The Multimission class used the same fuselage shape as the Fighter class. Wings in the 1990-TAD timeframe used a supersonic trapezoidal planform similar to the F-15 because of the emphasis on supersonic flight in the design mission, and the tail configuration was based on the F-18. In the 1995-TAD timeframe, the Multimission wings and tails have low-observable diamond planforms. The vertical and horizontal tails were sized as a fixed percentage of the wing area.

#### **B.** Aerodynamics

ACYSNT's aerodynamic predictions were applied to each conceptual aircraft configuration. Thus lift and drag consistently reflect modifications made to the aircraft geometry during sizing and optimization. ACSYNT's calculation procedures employ both theoretical methods and empirical information. Friction drag estimates are based on the method of Bertram (ref. 10), with an empirical correction for thickness-induced pressure fields. Base drag was computed using base pressure coefficient as a function of Mach number. Lift and induced drag are derived from a combination of potential theory and momentum integration procedures.

#### C. Structural Weight

Airframe weights are based on the geometry definition and are calculated from empirical equations based on correlations of existing aircraft data. The wing weight, for example, is a function of load factor, aspect ratio, leading-edge sweep, taper ratio, thickness-to-chord ratio, design dynamic pressure, and vehicle gross weight. Load factor, surface area, maximum Mach number, and vehicle gross weight are the parameters used to determine the fuselage weight. Weights of the tail surfaces are determined by similar empirical methods.

Between the two study timeframes, technological advances in both materials and construction techniques result in lower structural weight. Structural weight savings in ACSYNT are expressed in terms of savings relative to conventional, all aluminum construction. A 10% and 15% weight reduction over aluminum was used for the 1990-TAD and 1995-TAD structures, respectively. The assumption for 1990-TAD is reasonable since technology at the time of this study was better than the baseline (all aluminum) technology level assumed by ACSYNT's weight equations. The 15% reduction used in the 1995-TAD timeframe is conservative compared to the 1995-TAD assumptions agreed upon in the US/UK ASTOVL program.<sup>3</sup> Although claims for advanced structures and materials exceed the values used in this study, recent industry experience with composites has tempered expectations. Again, the emphasis was on applying the same assumptions to all the aircraft to establish trends.

<sup>&</sup>lt;sup>2</sup>Diameter used here is the equivalent diameter for the fuselage cross section with inlet and nozzle flow-through area removed.

<sup>&</sup>lt;sup>3</sup>Weight savings in the US/UK ASTOVL program ranged from 25% for the wing to 18% for the fuselage.

Table 1. Summary of aerodynamic surface planforms

Aircraft	Wing			H-tail				V-tail			<del></del>
	AR	Λ	λ	AR	Λ	λ	Area	AR	Λ	λ	Area
		c/4			c/4				c/4		
							Area ratio				Area ratio
Fighter	6.79	15.8	0.29	2.81	44.6	0.18	0.3751	1.17	48	0.32	0.1042
							Volume coefficient				Volume coefficient
Attack	4.4-5.2	12.8-18.2	0.312	3.574	30	0.386	0.5	1.02	30	0.302	0.07
Flying wing	3.5	39.1	0	N/A	N/A	N/A	N/A	N/A	N/A	N/A	N/A
							Area ratio				Area ratio
90 NFA and MRF	2.5	36.6	0.2	3	43	0.36	0.3818	1.25	34	0.38	0.1517
90 SSF	2.5	42.8	0.2	3	43	0.36	0.3813	1.25	34	0.38	0.1517
							Area ratio				Area ratio
95 NFA and MRF	2	24.3	0.05	2	24.3	0.05	0.381	1	24.3	0.05	0.151
95 SSF	2	24.3	0.05	2	24.3	0.05	0.3052	1	24.3	0.05	0.121

#### **D. Fixed Equipment**

The fixed equipment weights for each aircraft class were based on current inventory aircraft as shown in table 2. However, the Auxiliary Power Unit (APU) was assumed to be 200 lb for each aircraft class. The technology improvements used for structures (10% and 15%) were applied to fixed equipment weights as well.

#### E. Propulsion Database

To ensure the consistency desired by the design team, only one engine model, Pratt & Whitney's CCD-1178 engine deck, was used to generate families of engines in both timeframes. Several standardized estimates were also used, as follows. High-pressure bleed was 0.5% of compressor mass flow, and power extraction for subsystems was 100 hp. A propulsion installation factor of 16% of engine weight was used for all aircraft. Since cruise nozzle weight generally scales with engine mass flow,

Table 2. Equipment weight and reference aircraft for each aircraft class

System	Fighter (F-14A)	Multimission (F-18A)	Attack (A-6E)
APU	200	200	200
Instruments	169	94	219
Electrical	784	544	817
Avionics	3006	1652	2790
Crew accom- modations	534	375	613
Air conditioning	995	<u>610</u>	398
Total	5688	3475	5037

the afterburning convergent/divergent nozzle weight was empirically derived (nozzle weight equals 1.15 times design mass flow). Also derived empirically, subsonic nonafterburning nozzle weight was 63% of the convergent/divergent nozzle weight. Nozzle weight equations were not modified for technology level. Fuel system weight was 14% of engine weight (STOVL-unique equipment weight was excluded from this calculation). All aircraft use the military specification 5008A inlet recovery schedule. The aircraft are all single engine designs to keep the number of engines from being an aircraft discriminator; however, a sensitivity study was conducted to determine the impact this decision had on aircraft takeoff weight.

Engines in each technology timeframe have the same basic cycle characteristics in terms of overall pressure

ratio, combustor exit temperature, and nozzle cooling as shown in table 3. Several engines were produced in each timeframe for selection in each aircraft class, as shown in tables 4a and 4b. The selected engines for each aircraft class are shown in table 5.

Table 3. Engine technology trends

Time frame	OPR	Combustor exit temperature	Nozzle cooling (% core flow)
1990-TAD	28	3000°F	6.0
1995-TAD	32	3400°F	2.5

Table 4a. 1990-TAD study engines

Engine model	FPR	BPR	T/W <sup>a</sup> dry	T/W <sup>a</sup> A/B	SFC SLS	Throttle setting	Nozzle type
A	1.8	5.00	6.04	_	0.418	Navy waveoff	Fixed-area axisymmetric convergent
В	2.0	4.00	6.55		0.455	Navy waveoff	Fixed-area axisymmetric convergent
С	2.2	3.00	6.23	_	0.505	Navy waveoff	Fixed-area axisymmetric convergent
D	3.0	1.45	7.50	_	0.627	Navy waveoff	Fixed-area axisymmetric convergent
Е	4.1	0.70	7.96	12.72	0.742	Navy waveoff	Variable-area axisymmetric convergent- divergent
F	4.6	0.44	8.53	12.95	0.796	Navy	Variable-area axisymmetric
F STOVL	4.6	0.44	5.80	8.81	0.796	waveoff	convergent- divergent
G	5.2	0.25	9.06	13.10	0.847	Navy waveoff	Variable-area axisymmetric convergent-divergent

<sup>&</sup>lt;sup>a</sup>Uninstalled, unscaled, nozzle weight included.

Table 4b. 1995-TAD study engines

Engine model	FPR	BPR	T/W <sup>a</sup> dry	T/W <sup>a</sup> A/B	SFC SLS	Throttle setting	Nozzle type
A	2.1	5.00	9.12	_	0.449	Navy waveoff	Fixed-area axisymmetric convergent
В	2.3	4.00	9.38	_	0.488	Navy waveoff	Fixed-area axisymmetric convergent
С	2.6	3.00	9.83	_	0.540	Navy waveoff	Fixed-area axisymmetric convergent
D	3.0	2.30	10.36	_	0.587	Navy waveoff	Fixed-area axisymmetric convergent
E	4.1	0.94	9.76	16.21	0.703	Dry supercruise	Variable-area axisymmetric convergent- divergent
F	4.6	0.66	10.51	16.66	0.754	Dry supercruise	
	4.6	0.94	10.69	17.13	0.745	Navy waveoff	Variable-area axisymmetric
F	4.6	0.66	7.15	11.33	0.754	Dry supercruise	convergent- divergent
STOVL	4.6	0.94	7.27	11.65	0.745	Navy waveoff	
G	5.1	0.45	11.21	16.97	0.803	Navy waveoff	Variable-area axisymmetric convergent- divergent

<sup>&</sup>lt;sup>a</sup>Uninstalled, unscaled, nozzle weight included.

Table 5. Engines selected for each class of aircraft

1990-TAD	Engine model	Throttle ratio
Fighter	G	Waveoff
Attack	Α	Waveoff
NFA and MRF	F	Waveoff
SSF	F	Waveoff
1995-TAD	Engine model	Throttle ratio
Fighter	G	Supercruise
Attack	Α	Waveoff
NFA and MRF	F	Supercruise
SSF	F	Supercruise

A comparison of the engines in table 4 shows that the primary impact of the assumed technology advancements was approximately a 25% increase in uninstalled engine T/W. Existing engine development programs have this level of improvement as a goal. Also note that the specific fuel consumption (SFC) of the higher temperature 1995-TAD engines was, in general, no lower than for the 1990-TAD engines. Thus fuel efficiency was not a significant contributor to aircraft weight reduction with technology.

Engine throttle ratio<sup>4</sup> was used to optimize engines for both high- and low-speed missions. In the 1990-TAD timeframe, all aircraft use a throttle ratio which optimizes engine performance at sea level static conditions. This benefits both carrier waveoff and hover performance. In the 1995-TAD timeframe, engines for the supersonic aircraft use a throttle ratio which optimizes performance for supersonic cruise conditions since the engines for all dry supercruising<sup>5</sup> aircraft were sized by the dry supercruise requirement. An additional engine was generated for the 1995-TAD SSF using a waveoff throttle ratio in case hover proved to be the critical engine sizing condition for that aircraft, but the dry-supercruise throttle setting produced the lighter aircraft.

ACSYNT resizes the engine (using engine scale factor, ESF, which sizes thrust, dimensions, and airflow) during the synthesis process to meet thrust requirements. Engine thrust scales directly with ESF while engine weight scales with ESF according to the equation  $W_{ENG} = W_{(ESF=1.0)} * (ESF)^{(EXP)}$ . Typically, the exponent (EXP) is greater than 1.0 in aircraft studies as a weight penalty to discourage disproportionate engine growth. An exponent of 1.05 was used in this study as shown in figure 1, which also shows the constant engine T/W that would result from an exponent of 1.0. Unfortunately, EXP greater than 1.0 also means that engine T/W becomes optimistic when engine data are scaled down. Attack aircraft in this study have engine scale factors as low as 0.4, with a corresponding 5% increase in engine T/W. Since this is one of the less certain influences in this study, the impact of this increased T/W was examined as an attack aircraft sensitivity (see section on sensitivities).

#### F. Design Missions

The design missions used in this study were based on missions in the Navy STOVL Strike Fighter Desired Operational Characteristics (SSF DOC) (ref. 11). The design missions used for the different aircraft classes are as follows: a modified Combat Air Patrol (CAP) for the Fighter aircraft, Interdiction for the Attack aircraft, and a new composite mission for the Multimission aircraft. Each of these missions is described in more detail later.

The SSF DOC supersonic missions required dry supercruise, so it was also required in the 1995-TAD timeframe of this study. Dry supercruise was not required in the 1990-TAD timeframe (i.e., afterburner was allowed for

<sup>4</sup>The ratio of maximum combustor exit temperature to sea level static standard day design temperature. By increasing this ratio, the engine can be made to operate at a higher maximum inlet flow or a higher inlet temperature.

supersonic cruise) to reflect the capability of current inventory aircraft.

For consistency, the following mission-related items were applied. All aircraft:

- Loiter at sea level and 0.3 Mach prior to landing to ensure that enough fuel is available to wait for deck/runway availability
- Complete the design mission with internal fuel
- Carry a gun and 150 rounds of ammunition
- Use takeoff fuel composed of 10 minutes at idle for warmup, taxi, and 30 seconds at maximum power for takeoff
- Have 150 lb of trapped fuel
- Have 15° max angle of attack for maneuvers or landing
- Have no high-lift devices modelled for maneuvers or landing
- Use untrimmed aerodynamics
- Use naval aviation jet fuel, JP-5, with a density of 51.1 lb/ft<sup>3</sup>
- Retain all weapons on the design missions, since both laser guided bombs and air-to-air missiles are considered to be high value stores
- Have no descent or landing phases, no range credit for climb (this had the effect of making the design fuel weight, and therefore design takeoff weight, conservative)
- Have 5% reserve fuel after landing

#### G. Weapons

Aircraft weapons loads were normalized to facilitate comparisons between aircraft (table 6). The Long Range Missile (LRM), Short Range Missile (SRM), and Laser Guided Bomb (LGB) used in this study are the AIM-54 Phoenix, tail-steering AIM-9 Sidewinder, and GBU-16/B MK83, respectively.

The weapon carriage depends on aircraft class and timeframe, but all aircraft use consistent weight and drag values for missiles, bombs, pylons, and support gear (ejectors, rails, etc.). Wing tip installation of the SRM was assumed to have zero net drag. Weapons and support weight were assumed to remain unchanged in both timeframes of this study. Table 7 lists data for some of the weapons and support equipment (increments are per item).

Total weapons and support weight was determined through the addition of standardized component weights. Weapon drag was determined using the method of R. R. Snodgrass (ref. 12) with standardized incremental drags including shielding effects. An example is shown in table 8.

<sup>&</sup>lt;sup>5</sup>Level supersonic cruise without afterburner.

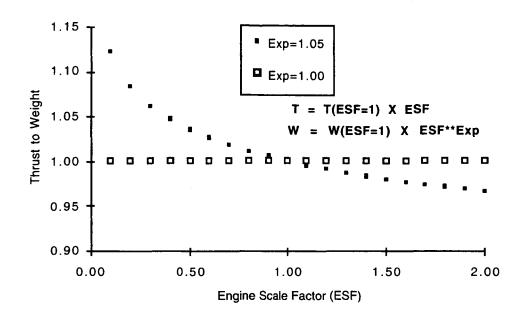


Figure 1. Effect of growth exponent on engine weight.

Table 6. Weapons load for each aircraft class

	LRM	SRM	LGB
Fighter	4	4	0
Attack	0	2	2/4
Multimission	2	2	0

Table 7. Weight and drag for weapons and support equipment

Weapon	Weight, lb	Drag area (0.2M), ft <sup>2</sup>
Laser Guided Bomb (LGB)	1091	0.39
LGB support	100	0.35
Long Range Missile (LRM)	985	0.46
LRM support	470	0.11
Short Range Missile (SRM)	199	0.144*
SRM support	100	0.1*
Heavy pylon	300	0.42
Light pylon	150	0.2
Gun (25 mm)	360	
Installation	252	
Ammo(150 rounds)	287	

<sup>\*</sup>No drag penalty for SRMs on wing tips.

Table 8. Example of external stores weights and drags

Description	Weight, lb	D/q, ft <sup>2</sup> @ 0.3M
4 MK83 Laser Guided Bombs (LGB)	4364	1.56
2 ASRAAMs*	398	0.00
2 Long pylons + 2 triple ejector racks	800	1.54
2 LAU 114 missile launchers*	200	0.00
No external fuel tank	0	0.00
Total	5762	3.10

<sup>\*</sup>Wing tip mounted missiles and launchers have no net drag over a mission.

#### H. Carrier Compatibility

The carrier-based aircraft in this study required several modifications compared to land-based aircraft.

Carrier aircraft fly slower approaches than land-based aircraft and must be able to perform a waveoff at low speed. Therefore, a full power 1.5g turn at 0.2M and sea level with all stores and reserve fuel on board was used as a design requirement to ensure an adequate maneuver margin. This requirement determined the wing loading for many of the sea-based aircraft. The SSF was exempt from this waveoff requirement because it performs vertical landings.

Carrier operations require heavier structures for several reasons: 1) arrested landings require a tail hook and reinforced fuselage, 2) landing gear are designed for 24 ft/s sink rate, and 3) catapult launches require reinforced nose gear and a strengthened fuselage. The SSF was also exempt from these requirements.

These weight increments are difficult to quantify because there are no data for aircraft that were designed for both land-based and sea-based operations with exactly the same mission capability. For example, contrary to the expected navalization penalty, the land-based F-4 actually had a higher empty weight than the carrier-based version. But in this case the land-based version used the increased strength and wing area of the carrier aircraft to carry an increased equipment load, which equates to higher mission capability. Similarly, few aircraft have successfully made the transition from land-based to sea-based operations. The carrier version of the British Hawk did perform catapult launches and arrested landings but required substantial structural reinforcement to do so. Jane's All the World's Aircraft shows that the navalized Hawk is approximately 11% heavier empty, but it can no longer fly as far as the land-based version.

Since historical research did not provide values for fuselage and landing gear weight penalties for carrier operations, an estimate had to be made another way. To this end, the F-14 and F-18 were modelled using ACSYNT's land-based weight equations. The actual aircraft fuselage and landing gear structure weights were approximately 30% greater than those modelled by ACSYNT. Therefore, 30% fuselage and landing gear weight penalties were applied to carrier-based aircraft in this study. Informal comments by U.S. Navy personnel<sup>6</sup> agreed that 30% was a reasonable estimate.

#### I. Maneuver Requirements

Maneuver requirements are important because they can size the wing and/or engine. The maneuver capability desired of the supersonic aircraft with 60% of mission fuel and air-to-air weapons was approximately 4.0g for the 1990-TAD timeframe and 5.0g (approximately ATF-level) for the 1995-TAD timeframe. However, the maneuver constraints used in this study were set somewhat lower than these values because maneuvering flaps were not modelled during the aircraft sizing process. Therefore, in the 1995-TAD timeframe, Fighter and Multimission aircraft were required to perform 3.8g at 0.9M and 30,000 ft. This maneuver requirement was reduced to 3.0g for the 1990-TAD timeframe. Similarly, sea-based aircraft were required to perform a 1.5g turn for approach waveoff.

For completeness, fallout combat maneuver performance was evaluated using maneuver flaps.

#### J. Structural Limits

In the 1990-TAD timeframe, design load limits were based on existing aircraft, as shown in table 9. In the 1995-TAD timeframe, Fighter and Multimission structural requirements were increased to be comparable to F-16 levels of performance. Dynamic pressure requirements were also increased. A safety factor of 1.5 was used to determine the ultimate load factor which was used by ACSYNT's weight estimation routines.

Table 9. Structural limits for aircraft classes

1990-TAD	Aircraft	g-limit	Max q	Max sea level Mach
Attack	A-6	6.5	1140	0.88
Fighter	F-15	6.5	2060	1.18
Multimission	F-18	7.5	1790	1.1
1995-TAD	g-limit	. М	ax q	Max sea level Mach
Attack	6.5	1	336	0.95
Fighter and Multimission	9.0	2	132	1.2

<sup>&</sup>lt;sup>6</sup>Several active and retired U.S. Navy personnel were involved in a review of this material by the CNA.

#### K. Overall Density Constraints

Overall aircraft density is an important constraint used to ensure valid aircraft packaging. As an aircraft becomes more dense it becomes lighter for the same mission, but maintenance access will be difficult. If a sizing study allows an aircraft to become more dense in response to an increase in weight, it will experience less growth than if it had been resized at the same overall density. If, on the other hand, maximum density is constrained, the wing and/or fuselage must increase in size to provide additional volume.

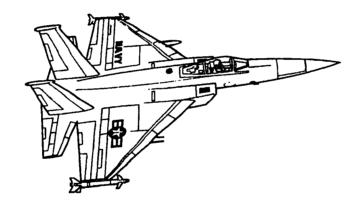
Overall aircraft density provides only a general design constraint and does not address individual component locations or densities. The baseline overall aircraft density for this study was derived by modelling an F/A-18 on ACSYNT. The flow-through volume of the inlet and nozzle was not included in the total volume. The remaining volume was divided into the operational empty

weight, which includes fuel and pilot, and yields an estimated overall aircraft density of 31 lb/ft<sup>3</sup>. A consistent method of accounting was devised to allow aircraft density to vary from this baseline for specific reasons such as internal weapons bays, STOVL-unique features like ducting, and flying-wing packaging constraints.

#### L. Low Observables Design

Since low observables were required for some aircraft in the 1995-TAD timeframe, a simple but consistent approach for design was needed. Therefore, Multimission aircraft evolve into the diamond planform for wing and tail shown in figure 2. Low observables aircraft have an additional 5% weight penalty on the wing, tail, and body structure to model the application of radar absorbing material. The flying wing Attack design has an inherently low-observables planform.

1990-TAD Conventional



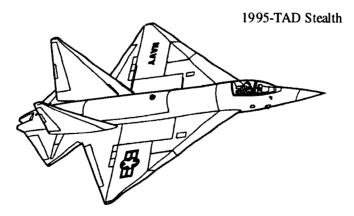


Figure 2. Evolution of Multimission aircraft.

Low-observables aircraft were also required to carry their weapons internally. The increased surface and frontal areas of the fuselage resulting from internal weapon bay volume are accounted for by ACSYNT's aerodynamics module. The volume of the weapon bays was estimated using the length and fin span of the largest munitions the aircraft were required to carry in the SSF DOC missions. The main weapon bay length of 172 inches was determined by the length of an AGM-88A High-speed Anti-Radiation Missile (HARM) with 4 inches clearance on each end. The HARMs require folding fins to fit in the bomb bay. The height and width of 23 inches were determined by the canted span of a GBU-16/B MK83 Laser Guided Bomb with 3 inches of clearance on either side. A similar approach was used for the SRM bays that hold the AIM-9 Sidewinder defensive missiles, yielding dimensions of 128 by 13 by 13 inches. These dimensions yield a volume penalty of 52 ft<sup>3</sup> per bomb bay and 15 ft<sup>3</sup> per missile bay for a total of 234 ft<sup>3</sup>.

Unfortunately, the weight penalty of the internal weapon bays was much harder to determine. It seemed reasonable that a weight penalty should be assessed for doors, actuation, and reinforcement of the cutout. However, this penalty depends on the dynamic pressure at the doors and on the size/location of the cutout. Since there was no simple method of predicting this weight penalty, it was

decided to use a constant weight penalty of 300 lb per bay. This arbitrary penalty is not coincidentally equal to the weight of one pylon. This means that the weight penalty for the two-bomb configurations is exactly the same regardless of whether the bombs are carried internally or externally (there is also a 50 lb increment for weapon ejectors, for both pylon- and bay-mounted weapons). Also, this leads to a direct comparison of the performance advantages of internal carriage, assuming that the assumed weight penalty is adequate.

An additional detail required attention for Attack aircraft with four bombs carried internally. The external pylons, weighing 300 lb each, can carry two bombs each while each internal bay used in this study can only carry one bomb. Therefore, carrying four bombs internally requires the equivalent weight penalty of four pylons which weigh 600 lb more than when carrying them externally.

Obviously, these weight penalties are arbitrary, given that actual internal weapons bay structural penalties are detailed-design dependent. Consequently, a sensitivity study was performed for Attack aircraft with internal bays. This sensitivity study used double and triple the baseline 300 lb weight penalty per bay. The outcome of this sensitivity study is reported in the results section.

#### Section III - Aircraft Differentiators

#### A. Fighter

The Fighter class of aircraft serves in the fleet air defense role by performing supersonic intercept and combat air patrol missions. It features a variable-sweep-wing design for enhanced loiter and supersonic cruise capability. The wing sweeps to maintain 0.75 Mach number perpendicular to the leading edge and also eliminates the need for a wing-fold mechanism. The wing weight was increased 30% to account for the pivot, actuation, and additional wing/fuselage structure. This factor was derived by comparing weights from an ACSYNT model of the F-14 to actual weight data and was supported by reviewing Navy personnel.

The Fighter was not intended to overfly highly defended targets and was assumed to operate its radar in an active search mode. Therefore, this design does not require any compromise for stealth in either timeframe; the missiles are carried externally and the wing, horizontal tail, and twin vertical tails are conventional in design. The LRMs are carried semi-submerged on the fuselage to save weight and drag compared to pylon-mounting them on the moving part of the wing. The SRMs are carried on short pylons on the fixed part of the wing. Finally, in both timeframes, the Fighter has the carrier compatibility weight and waveoff penalties. The differentiators for this aircraft class are summarized in table 10.

Table 10. Fighter class common technologies and requirements

	1990-TAD	1995-TAD
Radar absorbing material	+0%	+0%
Carrier compatable	Yes	Yes
Wing pivot	+30%	+30%
Internal weapons carriage	No	No
Dry supercruise required	No	Yes
Design load factor	6.5	9.0
Maneuver required	3.0g	3.8g
Wing/tail planform	Conventional	Conventional

The Fighter design mission (fig. 3) was a combination of the CAP and DLI missions from the SSF DOC which achieves a balance between supersonic and loiter capability. The original CAP mission had a loiter segment but only had 3 minutes of supersonic flight, whereas the DLI mission emphasized supersonic cruise but did not include loiter. The compromise mission consists of 400 nm cruise at best cruise altitude and Mach (BCAM) to a 60 minute loiter at 35,000 ft. After a lateral 100 nm supersonic dash, the aircraft performs 3 minutes of combat at 1.6 Mach number and 35,000 ft. The mission ends with 400 nm return cruise to the carrier at BCAM, followed by a 20 minute loiter at sea-level and 0.3 Mach to simulate the holding pattern required by carrier operations. The fighter's design weapon load was four AIM-54 Phoenix long-range air-to-air missiles (LRMs), four tail-steering AIM-9 Sidewinder short-range defensive missiles (SRMs), and a gun with 150 rounds of ammunition.

#### B. Attack

A matrix of subsonic Attack designs was developed so that the following four capabilities could be evaluated by the CNA:

Two vs. four bombs

One vs. two crew

External vs. internal weapon carriage

Conventional vs. flying wing planform

The SSF DOC Interdiction mission was used for the Attack design mission. It consists of a 500 nm cruise at BCAM, followed by a 50 nm dash at sea level and 0.80 Mach (fig. 4). The aircraft then performs 2 minutes of combat at 0.85M at sea level. The return leg is similar to the outbound leg with 20 minutes of loiter at sea level at 0.3 Mach added to simulate the holding pattern required by carrier operations. Attack aircraft were required to perform initial climbout in less than 75 nm to ensure that the minimum aircraft T/W was reasonable compared to existing Attack aircraft (~0.5 for the A-4). The aircraft returns with the design weapon load of GBU-16/B Mk-83R laser-guided bombs (LGBs), two AIM-9 Sidewinder short-range defensive missiles (SRMs), and a gun and with 150 rounds of ammunition.

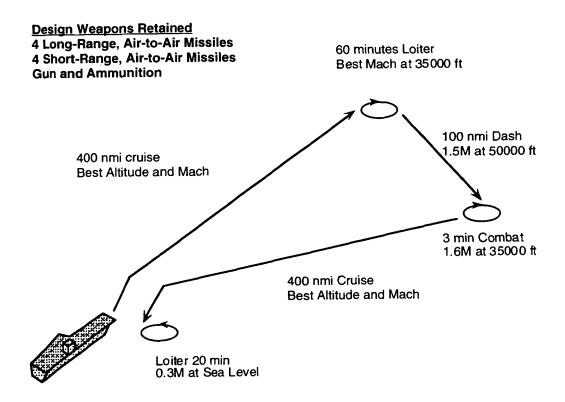


Figure 3. Combat air patrol design mission for Fighter aircraft.

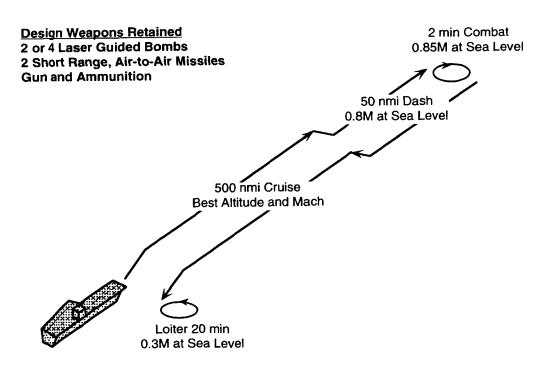


Figure 4. Interdiction design mission for Attack aircraft.

All Attack aircraft were designed to be carrier compatible. Both single and dual place Attack aircraft have 598 lb of fixed weight in the fuselage for cockpit armament, based on A-6 weights. Table 11 lists the items which differentiate the Attack aircraft class from the other classes. The items which differentiate each type of Attack aircraft are described below and in table 12.

#### 1. Conventional Attack

For the four conventional aircraft, aspect ratio and wing sweep were optimized by ACSYNT. To support mission effectiveness studies, the mission capability of the conventional designs was varied as described below.

The Light Attack design is the aircraft from which all Attack types were derived. While not directly based on the A-4 Skyhawk, this aircraft performs in a similar role. It has a single place cockpit, a moderate avionics weight appropriate for daylight missions, and two bombs mounted externally on the fuselage.

Some effort was required to ensure that the fixed equipment weights for this single-place aircraft were consistent with two-place aircraft in this study which used equipment weights from the two-place A-6. When the equipment weights for the F/A-18 and the A-6 were compared, the weight for furnishing, instrumentation, and avionics/ electrical support appeared to be proportional to the number of the crew. Therefore single-seat weights from the Multimission class were used for the Light Attack aircraft with one exception. The A-6 air conditioning weight was used for both single- and dual-place Attack aircraft because it was inappropriate to assume that the Light Attack aircraft had the same cooling requirements as the supersonic F-18. It should be noted that these weights for a two-place aircraft are not exactly double

those of a single-place aircraft, since there is some economy of scale.

The second attack aircraft type is Medium Attack and performs in the same role as the A-7 Corsair II. This aircraft is the Light Attack aircraft redesigned to carry four bombs instead of two, but otherwise meets the same requirements and constraints.

The Medium All-Weather (Medium AW) type is the Medium Attack aircraft redesigned to carry a second crewmember and substantially more avionics/electrical equipment. This resulted in an aircraft similar to the A-6 Intruder which can perform night, all-weather missions, and handle higher threat environments.

The Medium Internal Weapons (Medium IW) type is the Medium AW aircraft redesigned to carry the design weapons internally, with an additional weight and volume penalty.

Table 11. Attack class common technologies and requirements

	1990-TAD	1995-TAD
Radar absorbing material	+0%	+5% (FW only)
Carrier compatible	Yes	Yes
Armor	598 lb	598 lb
Design load factor	6.5	6.5
Wing/tail planform	Conventional/ FW	Conventional/ FW
Wing fold	150 lb	150 lb

Table 12. Attack aircraft type differentiators

	Light	Medium	Medium AW	Medium IW
Number of crew	1	1	2	2
Number of bombs	2	4	4	4
Weapons carriage	Tandem	Pylon	Pylon	Internal
Weapons related weight (lb)	4079	6661	6661	7261
Internal weapons bay volume (ft <sup>3</sup> )	0	0	0	238

#### 2. Flying Wing

The last Attack type is the Medium Flying Wing (Medium FW), which is the Medium IW aircraft redesigned with considerations given to low observables. This aircraft performs the same role as the proposed A-12 Avenger II, but has less range and a smaller bomb capacity.

The Medium FW design had three aerodynamic benefits. Since flying wings eliminate most of the fuselage, the separation drag was reduced by 50%. The interference drag between the fuselage and wing was eliminated for the same reason. And, of course, there was no drag contribution from tail surfaces. These and other aerodynamic considerations are summarized in table 13.

The Medium FW was, however, penalized for internal volume and packaging efficiency. First, the swept-wing Medium FW had a density disadvantage. Not only is the shape difficult for packaging payload and equipment, but only the front half of the wing chord is available due to balance considerations. This packaging inefficiency was modelled by requiring 25% more volume than a conventional pod and wing configuration. Second, 15% root thickness-to-chord ratio (t/c) was selected for the Medium FW to increase the volume available. While this is unusually high, the planform and t/c tapers to the tip, yielding a mean aerodynamic chord t/c of 10% compared to 8% which is a typical value for conventional aircraft.

Additional Medium FW differentiators result from lowobservables considerations. The sweep, aspect ratio, and taper ratio were fixed by radar cross-section considerations, while the conventional aircraft's values were optimized for the mission. Also, the Medium FW does not have horizontal or vertical tail surfaces and relies on active controls for stability. Finally, radar absorbing materials were applied to the 1995-TAD Medium FW by assessing a 5% structural weight penalty.

#### C. Multimission

No single SSF DOC mission provided a combination of Fighter and Attack mission capabilities. A new design mission was therefore created for the Multimission class (fig. 5). It is comprised of a 250 nm cruise at sea level

Table 13. Aerodynamic considerations for flying wing designs

	Conventional	Flying wing
Separation drag factor	1.0	0.5
Interference drag factor	1.0	0.0
Wing thickness to chord	0.09	0.15
Taper ratio	0.31	0.0

and 0.85 Mach, then a 60 minute loiter at 35,000 ft at best-endurance speed. The mission continues with a 150 nm supersonic dash at 50,000 ft, 2 minutes of combat at 1.5M and 50,000 ft, and a return leg to the carrier of 400 nm at BCAM. All Multimission aircraft loiter at sea level and 0.3 Mach prior to landing to ensure that enough fuel was available to wait for deck/runway availability. Design weapon load was two LRMs, two SRMs, and a gun with 150 rounds of ammunition.

Three Multimission aircraft were developed: a STOVL Strike Fighter (SSF), a sea-based Naval Fighter/Attack (NFA), and a land-based MultiRole Fighter (MRF). Table 14 lists items which differentiate this aircraft class from the others. The 1990-TAD Multimission aircraft are conventional and carry weapons externally. All three types evolve into a low-observables, ATF-type planform with internal weapons in the 1995-TAD timeframe (see fig. 2).

Table 15 lists items that differentiate between the SSF, NFA, and MRF types. The SSF aircraft was exempt from the waveoff requirement because it can maneuver at low speeds with thrust vectoring and reaction controls. The STOVL propulsion system is described below. The MRF was exempt from the waveoff requirement because it had a long runway available and makes approaches at higher speed. Multimission aircraft in the 1990-TAD timeframe carry the two LRMs on wing pylons and two SRMs on the wing tips. In the 1995-TAD timeframe, Multimission aircraft carry all of the weapons internally.

<sup>&</sup>lt;sup>7</sup>Balance considerations are relieved somewhat with the advent of digital fly-by-wire flight controls.

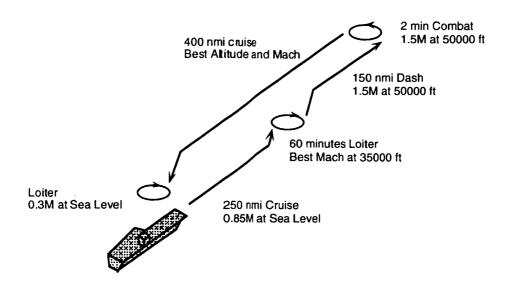


Figure 5. Multimission design mission.

Table 14. Multimission class common technologies and requirements

	1990-TAD	1995-TAD
Radar absorbing material	+ 0%	+ 5%
Internal weapons carriage	No	Yes
Dry supercruise required	No	Yes
Design load factor	7.5	9.0
Maneuver required	3.0g	3.8g
Wing/tail planform	Conventional	Diamond

Table 15. Multimission aircraft type differentiators

	SSF	NFA	MRF
Navalization penalty			
Fuselage structure	0	+30%	0
Landing gear weight	0	+30%	0
Wave off maneuver	No	Yes	No
Wing fold	150 lb	150 lb	
STOVL penalty			
Propulsion weight	+47%	0	0
Landing hover T/W	1.16	N/A	N/A
Reaction control system	Yes	No	No
Duct volume penalty	10%	0	0
Loiter in pattern	10 min	20 min	20 min
Fuselage fineness ratio	9	10	10

To minimize unnecessary differences in this study, the SSF and conventional Multimission aircraft have the same tail designs in each timeframe. This eliminates any differences in ACSYNT's weight and aerodynamic predictions for different types of tails. In addition, the vertical and horizontal tail area for Multimission aircraft were a specified fraction of the wing. The 1990-TAD SSF tail area ratios were reduced to 80% of the MRF and NFA tail area ratios to allow the SSF to benefit from its vectoring cruise nozzle which provides pitch and yaw trim/control. It turned out that, even with its reduced tail area ratio, the SSF aircraft has more tail volume than the conventional aircraft because it has a longer fuselage.

#### 1. STOVL Strike Fighter (SSF)

The SSF aircraft has a number of unique features and sizing constraints. The SSF Multimission aircraft uses the Mixed-Flow/Vectored-Thrust (MFVT) propulsion concept developed during the US/UK ASTOVL study (ref. 2) as shown in figure 6. This system was selected for

study based on its simplicity and superior transition performance.

From US/UK ASTOVL study, the propulsion system weighs 47% more than the conventional Multimission engine in both timeframes for STOVL-unique propulsion components (ducts, nozzles, etc.). The mixed flow cycle requires the fan and core to have the same pressure ratio so that the fan and core exhaust flows can be combined in the cruise nozzle. This propulsion system has an afterburning cruise nozzle which is capable of ±20° vectoring in both pitch and yaw. A butterfly valve controls flow into the ducts which supply the variable area, flushmounted clamshell lift nozzles. The lift nozzles have ±20° vectoring capability fore and aft around vertical to enhance short takeoff performance. Total thrust vectoring is provided by flow shifting between the lift and cruise nozzles combined with the limited rotation capability of the lift nozzles. The lift nozzles are oriented 8° aft from perpendicular to the body, since the aircraft maintains an 8° nose-up pitch attitude on the ground and during hover.

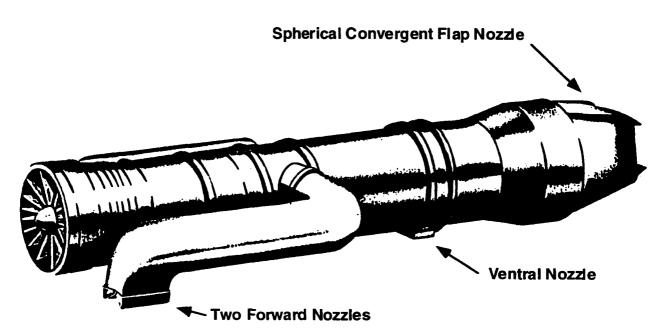


Figure 6. STOVL propulsion system.

The SSF lands vertically with the exhaust completely blocked from the cruise nozzle and most of the flow exiting the lift nozzles and up to 10% of the flow exiting the ventral trim nozzle. Vertical landings are performed with unaugmented, mixed flow.

The MFVT concept can perform takeoff in three modes. The first is a conventional takeoff using maximum afterburner. The second is a maximum nonafterburning power, vectored thrust, short takeoff which provides shorter takeoff rolls than the first method (ref. 13). The third takeoff method begins with maximum afterburner in conventional mode, followed by shutting off the afterburner and vectoring the thrust at, or prior to, rotation. This method should provide the shortest takeoff roll but is more complicated.

This propulsion concept only requires a yaw reaction control system in hover and at low speed because the engine exhaust can be transferred between the right and left lift nozzles for roll and between the lift nozzles and ventral nozzle for pitch. The reaction control system weight will therefore be much less than for typical multi-axis control systems. The reaction control system was scaled as 3.4% of the fuselage weight, based on the US/UK ASTOVL study. No weight penalty for lift improvement devices (fuselage fences) was included.

The SSF's overall density was reduced to 28 lb/ft<sup>3</sup> (about 90% of the conventional aircraft) to account for the large internal-flow transfer ducts associated with the propulsion system. This had the effect of increasing aircraft volume

which increased weight, skin friction, and wave drag. The density of the rest of the aircraft, without the STOVL ducts, was still close to the baseline 31 lb/ft<sup>3</sup>. This density adjustment was based on the MFVT design from the US/UK ASTOVL program (ref. 2) and accounts for 122 ft<sup>3</sup> of duct volume (two ducts that are 23 inches in diameter and 21 feet long).

Next, to ensure adequate thrust margin, the SSF aircraft was required to hover with an aircraft  $T/W \ge 1.16$  (Sea Level, Standard Day) at the end of the mission with all weapons retained and 10% fuel. This T/W margin provides a 0.05g vertical acceleration capability with 1.12% thrust loss due to 8.8 lbm/sec compressor air flow bleed for the reaction control system and 8.7% suckdown for hover at 10 ft. Because it was difficult to estimate jet-induced interactions for conceptual design with much precision, the sensitivity of SSF aircraft weight to required hover T/W was evaluated (TOGW proved to be relatively insensitive to higher hover T/W requirements).

The SSF design mission only requires 10 minutes of loiter in the landing pattern since flexible STOVL operational procedures shorten the time required to recover aircraft compared to the conventional carrier recovery cycle. The 1990-TAD SSF required so much additional volume to meet the density requirement that the maximum fuselage length (to fit carrier elevator) was reached. In this case, the body length was held at the maximum and the diameter was increased even though the resulting fineness ratio was no longer consistent with the other aircraft.

<sup>&</sup>lt;sup>8</sup>This hover condition is the same one that was used in the US/UK ASTOVL program even though the aircraft lands with only a 5% fuel reserve.

#### Section IV - Results

This section describes the results of sizing the aircraft to the above groundrules. Basic data include weights, dimensions, and maneuver performance for each aircraft. Separate sections cover Attack aircraft comparisons, SSF versus land-based and sea-based conventional Multimission aircraft, operational mission analyses, fallout range performance on all of the SSF DOC missions, and propulsion sensitivities.

#### A. Basic Aircraft Data

Table 16 presents a summary of the baseline aircraft developed in this study. Detailed weight, propulsion, aerodynamic, maneuver, mission, and geometry data for each aircraft can be found in Appendix A. The last three columns in table 16 indicate some of the constraints for each aircraft. Values are outlined to indicate that the constraint was active. The sizing constraints shown are:

Carrier waveoff capability as modelled by sustained 1.5g turn capability at 0.2M and sea level

ATF levels of up-and-away maneuverability as modelled by sustained turn capability at 0.9M and 30,000 ft with maximum afterburner

Dry supercruise capability as modelled by sustained 1.0g Specific Excess Power (SEP) at 1.5M, 50,000 ft without afterburner

Figure 7 provides an overall comparison at one scale of all of the aircraft generated in this study. Figures 8–12 compare all of the 1990-TAD and 1995-TAD aircraft by class at a larger drawing scale.

A check was made of the maneuver performance of supersonic 1995-TAD aircraft, as summarized in table 17.

All of the Multimission aircraft had similar maneuver performance which is reported as "Multimission" in the table. This table also includes a comparison with requirements from the US/UK ASTOVL study of 1995-TAD aircraft. Maneuver performance was determined with an approximation for enhanced lift due to maneuvering flaps.

Aircraft growth factor is used frequently in the following discussion. It indicates the sensitivity of an aircraft design's TOGW to aircraft size. It is measured by the change in TOGW that results from adding (or deleting) fixed weight to the aircraft. Growth factor =  $\Delta TOGW/\Delta W_{fixed}$ . It is not feasible to develop an aircraft with a large growth factor because it will rapidly gain weight, or lose range/payload capability, in response to any additional airframe weight added during engineering and manufacturing development. A high growth factor reflects a risky design and means that meeting technology goals for weight reduction becomes very critical.

#### B. Attack Aircraft Trends

A comparison of the Attack aircraft designs highlights the influence of the differentiators used to define them. In table 16, for example, the conventional external carriage aircraft are similar in wing loading and aircraft T/W, indicating no fundamental difference between them. The Medium IW aircraft has a significantly lower wing loading and T/W, which is mostly due to the reduced parasite drag of the weapons. The Flying Wing's reduced drag produced the lowest T/W and the lightest TOGW of the medium sized Attack aircraft. Individual Attack aircraft types are discussed below, starting with the influence of payload size.

Table 16. Baseline aircraft summary

dry         A/B         empty         gross           0.51         0.74         0.60         0.56           0.58         0.88         0.62         0.56           0.51         -         0.50         0.56           0.51         -         0.54         0.57           0.51         -         0.57         0.60           0.45         -         0.52         0.60           0.53         -         0.52         0.50           0.53         -         0.55         0.51           0.53         -         0.55         0.51           0.54         -         0.55         0.51           0.53         -         0.55         0.51           0.54         -         0.55         0.51           0.54         -         0.55         0.51           0.54         -         0.55         0.51           0.54         -         0.55         0.56           0.55         -         0.55         0.58           0.54         0.59         0.53         0.45           0.77         1.22         0.55         0.46           0.78         0.79	TOGW Wing T/W	T/W	Structure/	Empty/	Fuel	Body	Body	T/W		Constraints	raints
57619         69.0         0.51         0.74         0.60         0.56         0.30           53356         67.2         0.58         0.88         0.62         0.56         0.28           24777         75.2         0.51         -         0.50         0.59         0.22           33438         72.8         0.52         -         0.54         0.57         0.23           34486         68.4         0.45         -         0.51         0.59         0.18           26392         31.8         0.53         -         0.50         0.59         0.18           21046         73.6         0.51         -         0.50         0.18           21047         73.8         0.53         -         0.59         0.17           21048         73.6         0.53         0.55         0.23           27728         73.8         0.50         -         0.55         0.23           29095         67.3         0.43         -         0.55         0.55         0.24           25078         33.4         0.36         -         0.53         0.48         0.44           80510         90.0         0.78         1.18<	loading (psf)	A/B	empty	gross	fraction (%)	diamete0r (ft)	length (ft)	hover	0.2M (g)	0.9M (g)	1.5M (SEP)
53356       67.2       0.58       0.62       0.56       0.28         24777       75.2       0.51       -       0.50       0.59       0.22         33438       72.8       0.52       -       0.54       0.57       0.23         34486       68.4       0.45       -       0.51       0.59       0.22         21046       73.6       0.51       -       0.50       0.18         21046       73.6       0.51       -       0.50       0.18         21046       73.6       0.51       -       0.50       0.18         21046       73.8       0.53       -       0.50       0.18         21046       73.8       0.50       0.55       0.51         29095       67.3       0.43       -       0.52       0.53       0.16         29095       67.3       0.43       -       0.52       0.53       0.16       0.18         64315       81.3       0.57       0.87       0.58       0.46       0.46         80510       90.0       0.78       1.18       0.48       0.41       0.41         49471       66.1       0.77       1.22       0	0.69	0.74	09.0	0.56	0.30	5.0	50.4	I	1.9	3.6	1
24777       75.2       0.51       -       0.50       0.59       0.22         33438       72.8       0.52       -       0.54       0.57       0.23         34486       68.4       0.45       -       0.51       0.59       0.22         26392       31.8       0.43       -       0.50       0.59       0.18         21046       73.6       0.53       -       0.50       0.17         27728       72.9       0.53       -       0.55       0.23         27728       73.8       0.50       -       0.55       0.51       0.24         27728       73.8       0.53       -       0.55       0.51       0.24         29095       67.3       0.43       -       0.56       0.50       0.18         25078       33.4       0.36       -       0.53       0.58       0.16         64315       81.3       0.57       0.87       0.58       0.45       0.46         80510       90.0       0.78       1.18       0.48       0.41         49471       66.1       0.77       1.22       0.55       0.49       0.41         41604       67.6	67.2	0.88	0.62	0.56	0.28	4.9	49.0	i	2.0	3.9	0
33438       72.8       0.52       —       0.54       0.57       0.23         347573       72.9       0.51       —       0.51       0.59       0.22         34486       68.4       0.45       —       0.52       0.60       0.18         25392       31.8       0.33       —       0.52       0.59       0.17         21046       73.6       0.51       —       0.52       0.59       0.17         27728       73.8       0.53       —       0.55       0.51       0.24         27728       73.8       0.53       —       0.55       0.51       0.24         29095       67.3       0.43       —       0.55       0.50       0.18         25078       33.4       0.36       —       0.55       0.50       0.16         64315       81.3       0.57       0.87       0.58       0.44       0.44         80510       90.0       0.78       1.18       0.48       0.41         49471       66.1       0.77       1.22       0.50       0.46       0.41         49471       67.6       0.78       0.50       0.50       0.46       0.41	75.2	1	0.50	0.59	0.22	4.6	38.2	I	1.5	1	I
x       37573       72.9       0.51       -       0.51       0.59       0.22         34486       68.4       0.45       -       0.52       0.60       0.18         26392       31.8       0.33       -       0.50       0.59       0.17         21046       73.6       0.51       -       0.52       0.53       0.23         27728       72.9       0.53       -       0.55       0.23         29095       67.3       0.43       -       0.56       0.50       0.18         29095       67.3       0.43       -       0.56       0.50       0.18         64315       81.3       0.57       0.87       0.58       0.44         64315       81.3       0.59       0.90       0.53       0.45       0.46         80510       90.0       0.78       1.18       0.48       0.51       0.41         49471       66.1       0.77       1.22       0.55       0.49       0.41         41604       67.6       0.78       0.50       0.50       0.46       0.41	72.8	ı	0.54	0.57	0.23	4.5	45.2	ı	1.5	ı	ı
34486       68.4       0.45        0.52       0.60       0.18         26392       31.8       0.33        0.50       0.59       0.17         21046       73.6       0.51        0.52       0.53       0.23         27728       72.9       0.53        0.55       0.23         27728       72.9       0.53        0.55       0.24         29095       67.3       0.43        0.56       0.50       0.18         25078       33.4       0.36        0.53       0.58       0.16         64315       81.3       0.57       0.87       0.58       0.44         53072       91.5       0.59       0.90       0.53       0.45       0.46         80510       90.0       0.78       1.18       0.45       0.41         49471       66.1       0.77       1.22       0.55       0.49       0.41         41604       67.6       0.78       1.24       0.50       0.46       0.42	72.9	ı	0.51	0.59	0.22	4.5	48.2	ı	1.5	I	I
26392       31.8       0.33       -       0.50       0.59       0.17         21046       73.6       0.51       -       0.52       0.53       0.23         27728       72.9       0.53       -       0.55       0.51       0.24         29095       67.3       0.43       -       0.56       0.60       0.18         25078       33.4       0.36       -       0.53       0.58       0.16         64315       81.3       0.57       0.87       0.58       0.44         53072       91.5       0.59       0.90       0.53       0.45       0.46         80510       90.0       0.78       1.18       0.48       0.51       0.41         49471       66.1       0.77       1.22       0.55       0.49       0.41         41604       67.6       0.78       1.24       0.50       0.46       0.42	68.4	t	0.52	09.0	0.18	4.6	49.8	I	1.5	ŀ	ı
21046       73.6       0.51       -       0.52       0.53       0.23         27728       72.9       0.53       -       0.55       0.51       0.24         29095       67.3       0.43       -       0.56       0.60       0.18         25078       33.4       0.36       -       0.53       0.58       0.16         64315       81.3       0.57       0.87       0.58       0.46         83072       91.5       0.59       0.90       0.53       0.45       0.46         80510       90.0       0.78       1.18       0.45       0.41         49471       66.1       0.77       1.22       0.55       0.46       0.41         41604       67.6       0.78       1.24       0.50       0.46       0.42	31.8	t	0.50	0.59	0.17	4.5	I	ı	2.0	ı	ı
27728       72.9       0.53       -       0.55       0.51       0.24         31072       73.8       0.50       -       0.52       0.55       0.23         29095       67.3       0.43       -       0.56       0.60       0.18         :       25078       33.4       0.36       -       0.53       0.58       0.16         64315       81.3       0.57       0.87       0.58       0.48       0.44         53072       91.5       0.59       0.90       0.53       0.45       0.46         80510       90.0       0.78       1.18       0.45       0.41         49471       66.1       0.77       1.22       0.55       0.49       0.41         41604       67.6       0.78       1.24       0.50       0.46       0.42	73.6	1	0.52	0.55	0.23	4.5	35.0	1	1.5	ţ	ι
4       31072       73.8       0.50       -       0.52       0.55       0.23         29095       67.3       0.43       -       0.56       0.60       0.18         25078       33.4       0.36       -       0.53       0.58       0.16         64315       81.3       0.57       0.87       0.58       0.48       0.44         53072       91.5       0.59       0.90       0.53       0.45       0.46         80510       90.0       0.78       1.18       0.48       0.53       0.41         49471       66.1       0.77       1.22       0.55       0.49       0.41         41604       67.6       0.78       1.24       0.50       0.46       0.42	72.9	ĺ	0.55	0.51	0.24	4.5	40.3	I	1.5	ı	I
29095       67.3       0.43       -       0.56       0.60       0.18         25078       33.4       0.36       -       0.53       0.58       0.16         64315       81.3       0.57       0.87       0.58       0.48       0.44         53072       91.5       0.59       0.90       0.53       0.45       0.46         80510       90.0       0.78       1.18       0.48       0.53       0.41         49471       66.1       0.77       1.22       0.55       0.49       0.41         41604       67.6       0.78       1.24       0.50       0.46       0.42	73.8	I	0.52	0.55	0.23	4.6	44.3	ı	1.5	ı	ı
um FW Attack         25078         33.4         0.36         -         0.53         0.58         0.16           vL         64315         81.3         0.57         0.87         0.58         0.48         0.44           vL         53072         91.5         0.59         0.90         0.53         0.45         0.46           vL         80510         90.0         0.78         1.18         0.48         0.53         0.41           s         49471         66.1         0.77         1.22         0.55         0.49         0.41           s         41604         67.6         0.78         1.24         0.50         0.46         0.42	67.3	ı	0.56	09.0	0.18	4.6	45.4	ı	1.5	I	I
64315       81.3       0.57       0.87       0.58       0.48       0.44         VL       80510       91.5       0.59       0.90       0.53       0.45       0.46         VL       80510       90.0       0.78       1.18       0.48       0.53       0.41         49471       66.1       0.77       1.22       0.55       0.49       0.41         41604       67.6       0.78       1.24       0.50       0.46       0.42	33.4	i	0.53	0.58	0.16	4.5	ı	ı	1.9	ı	1
53072       91.5       0.59       0.90       0.53       0.45       0.46         80510       90.0       0.78       1.18       0.48       0.53       0.41         49471       66.1       0.77       1.22       0.55       0.49       0.41         41604       67.6       0.78       1.24       0.50       0.46       0.42	81.3	0.87	0.58	0.48	0.44	0.9	59.9	ı	1.5	3.1	-131
80510         90.0         0.78         1.18         0.48         0.53         0.41           49471         66.1         0.77         1.22         0.55         0.49         0.41           41604         67.6         0.78         1.24         0.50         0.46         0.42	91.5	06:0	0.53	0.45	0.46	5.9	58.5	1	1.5	3.0	-128
49471     66.1     0.77     1.22     0.55     0.49     0.41       41604     67.6     0.78     1.24     0.50     0.46     0.42	0.06	1.18	0.48	0.53	0.41	7.1	64.0	1.16	ı	3.4	15
41604 67.6 0.78 1.24 0.50 0.46 0.42	66.1	1.22	0.55	0.49	0.41	5.3	52.7	1	1.7	3.8	0
	9.79	1.24	0.50	0.46	0.42	5.1	51.5	I	1.6	3.8	0
	63.9	1.22	0.48	0.50	0.40	9.6	56.1	1.19	ı	3.8	0

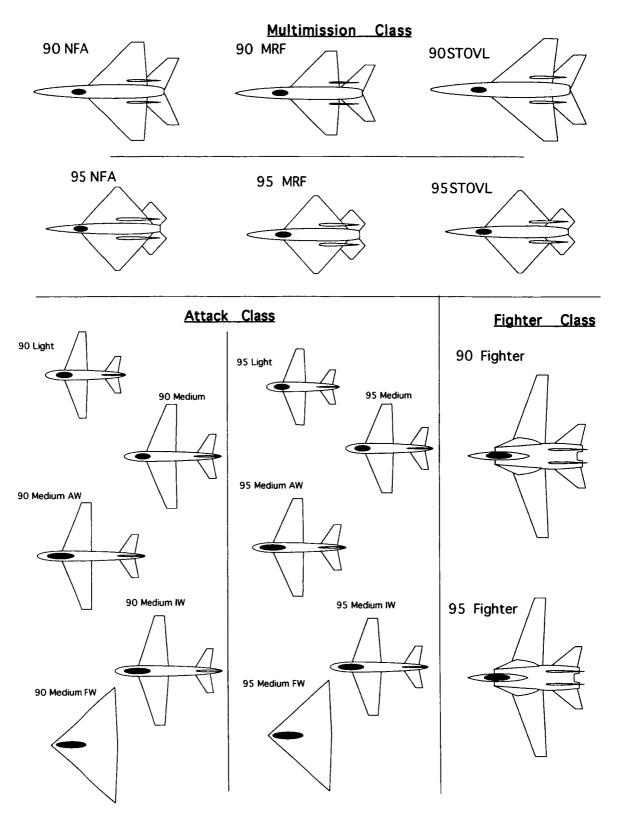
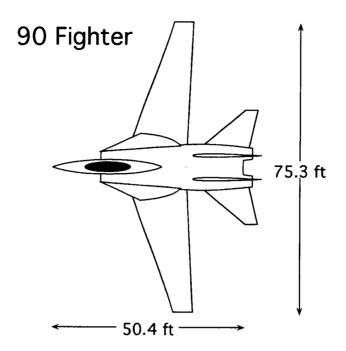


Figure 7. Comparison of aircraft classes.



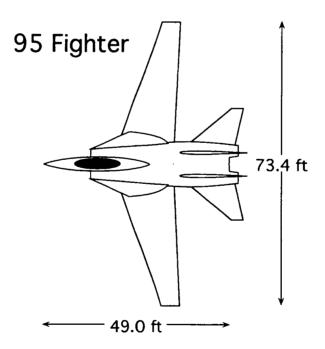


Figure 8. Fighter aircraft dimensions.

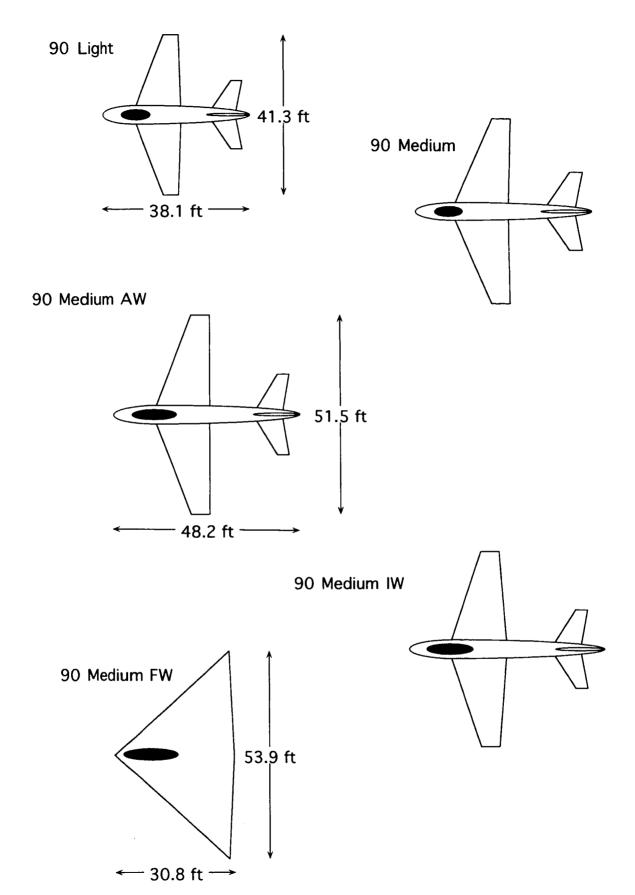


Figure 9. 1990-TAD Attack aircraft dimensions.

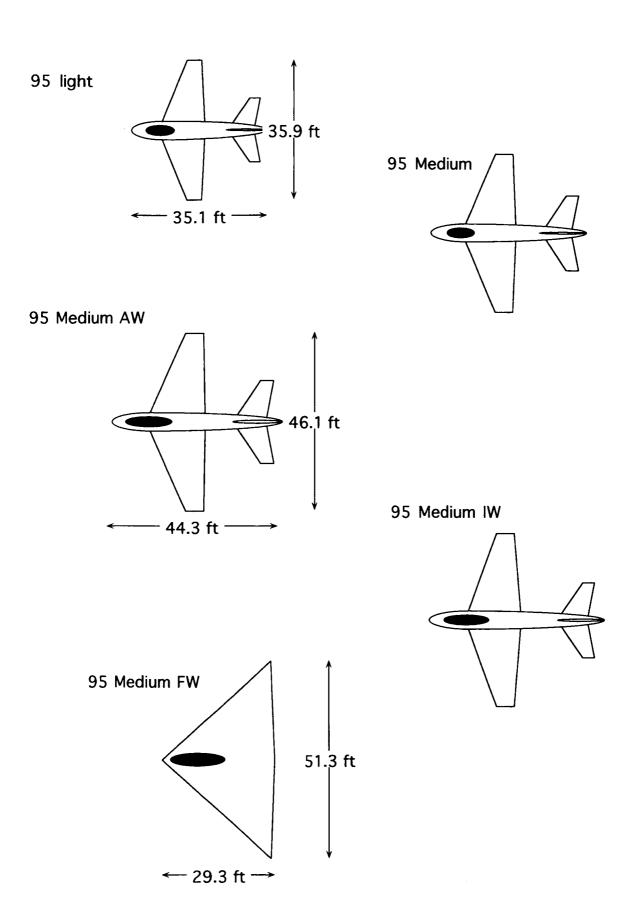
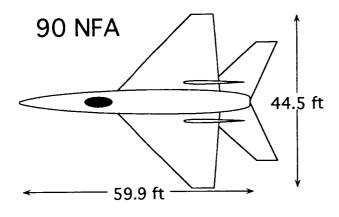
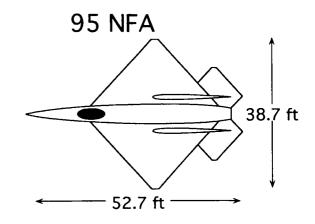
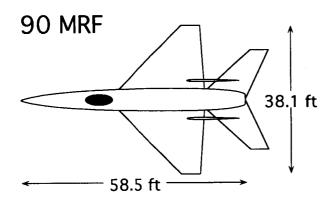
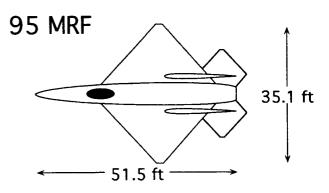


Figure 10. 1995-TAD Attack aircraft dimensions.









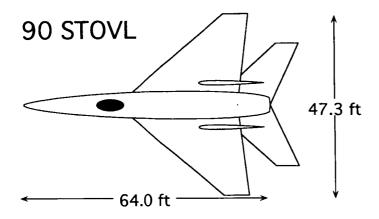


Figure 11. 1990-TAD Multimission aircraft dimensions.

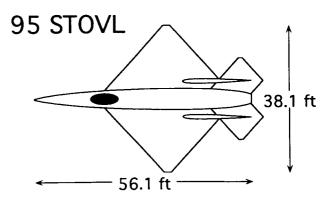


Figure 12. 1995-TAD Multimission aircraft dimensions.

Table 17. Maneuver performance of 1995-TAD Multimission and Fighter aircraft

		Multimission	Fighter
Wing area		724	794
Combat weight*		36606	41832
SLST AB		56610	46818
SLST dry		35731	30930
W/S		51	64
T/W AB		1.55	1.12
T/W dry		0.98	0.74
*Missiles away, 60	% fuel		
Condition	Required (US/UK ASTOVL)	Multimission	Fighter
Sustained g's			
0.5M SL dry	5	6	8.2
0.9M SL dry	6.1	7.1	9
0.9M 20k AB	6.2	7.3	7.8
1.2M 20k AB	5.5	8.7	8.7
0.2M SL AB		1.5	2.3
0.6M 15k AB		5.8	6.4
0.7M 30k AB		3.7	4.2
0.9M 30k AB		4.9	5.2
1.2M 40k AB		3.9	3.7
1.5M 50k AB		3	1.7
SEP			
1.4M 30k AB	500	902	748
0.9M 20k AB	620	875	573
0.9M SL AB	1000	1341	822
0.9M 30k dry		239	379
1.5M 50k dry		-2	82
0.9M SL dry		503	247

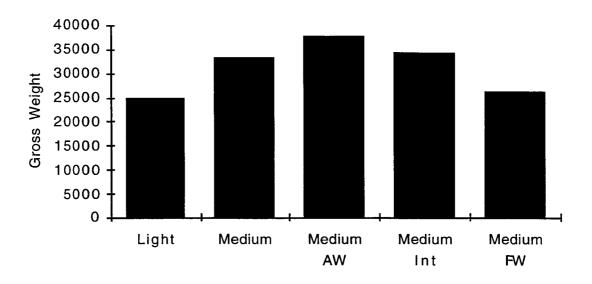


Figure 13. 1990-TAD Attack Aircraft TOGWs.

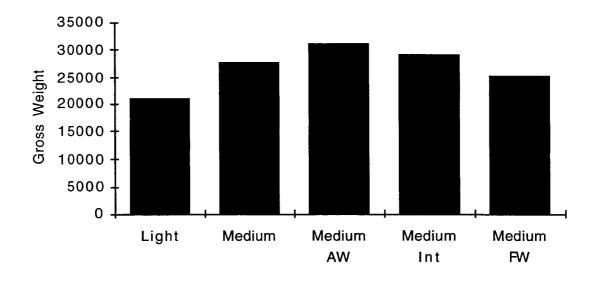


Figure 14. 1995-TAD Attack Aircraft TOGWs.

#### 1. Two vs. Four Bombs

The only difference between the Light and Medium Attack types is the bomb load. Figures 13 and 14 show that carrying four bombs would require two Light Attack aircraft which outweigh a single Medium Attack by a factor of 1.5. This indicates that there is an economy of scale for a larger design payload weight. On the other hand, the additional 2,182 lb of payload results in a gross weight increase of 8,661 lb due to the increased weight

and parasite drag, which means that carrying two extra bombs is a relatively severe weight penalty for the Light Attack aircraft.

#### 2. One vs. Two Crewmembers

The sensitivity to having a second crewmember is shown by the difference in TOGW between the Medium and the Medium AW designs (figs. 13 and 14). The second crewmember and additional equipment weight of 1,954 lb

yields an increase in gross weight of 4,135 lb (growth factor of 2.1). It was beyond the scope of this study to quantify the increased mission effectiveness of the all-weather aircraft. However, the change between the Light and the Medium designs (two to four bombs) was greater than the change between the Medium and the Medium AW in terms of both weight and growth factor, even though the weight increases were approximately the same for each change. This is partly explained by the fact that there was no direct drag penalty for the additional equipment weight inside the Medium AW while there was a drag penalty for the additional external bombs.

#### 3. External vs. Internal Weapons

Figures 13 and 14 also show that the Medium IW is lighter than the Medium AW. The reduced drag of the internal weapon carriage more than compensates for the increased fuselage weight and volume associated with the internal weapons bays. To understand this, the impact of internal bays is discussed further. Also, keep in mind the assumptions made to model internal weapons carriage.

First, many successful aircraft have internal weapon bays so the benefits outweigh the penalties in at least some cases. Internal bays are competitive when mission requirements favor reduced parasite drag over the additional structure weight and volume. For example, the increased volume (and therefore drag and weight) incurred by carrying weapons internally has less impact for a subsonic aircraft than it might have for an area ruled supersonic aircraft. Also, since the weight of internal bays depends on their size, weapon loads that are small in relation to the aircraft size have a smaller weight penalty.

The internal bay structural weight penalty used for these Attack aircraft was an arbitrary 300 lb per bomb. A sensitivity study was performed to evaluate the impact on TOGW of doubling and tripling the bay structural weight penalty (table 18). It is significant that the Medium IW with double, and the Medium FW with triple, the bay weight are still lighter than the baseline Medium AW design.

There are two reasons why this penalty was not very significant in this study. First, finned weapons increase the internal bay volume required. Tail steering AIM-9 Sidewinders were used for self-defense and it was assumed that folding fin HARM missiles would be available.

Second, fuselage parasite drag did not increase significantly in response to the increased fuselage volume. Separation drag scales with body diameter which scales roughly to the one third power of volume. This means separation drag is very insensitive to volume changes.

Table 18. Attack aircraft sensitivity to internal weapons bay weight

	Baseline penalty	Double penalty	Triple penalty
1990 Medium IW	32459	35185	37478
1990 Medium FW	26392	29093	32201
1995 Medium IW	29095	31103	33736
1995 Medium FW	25077	26875	28913

Skin friction scales with the surface area which scales roughly to the two thirds power of volume. While this is more sensitive than separation drag, it is still not a major penalty. The one source of drag that does vary more or less directly with volume is compressibility, or wave drag. Since the maximum Mach number was 0.85, the effects of compressibility were small.

Another issue with internal bays is that they tend to be operationally restrictive; some loads may be too bulky to carry. In this study, for example, the four cluster bombs used in the Close Air Support (CAS) fallout mission weigh less than half of the design payload weight but still use all four bomb bays. In this case, additional fuel had to be carried externally even though there was volume wasted in each bay.

#### 4. Conventional vs. Medium FW Planform

Figures 13 and 14 also show that the Medium FW designs are lighter than the other Medium Attack aircraft. They also have the lowest aircraft T/W, the lowest fuel weight, and the best waveoff capability of all of the aircraft. This impressive performance resulted from eliminating the vertical and horizontal tails which saved weight, wetted area, and interference drag. The Medium FW traded these penalties for the additional cost and complexity of fly-bywire control systems and artificial stability that would probably be required to achieve acceptable lateral/directional handling qualities.

Also, the Medium FW does not have to meet tail volume requirements which can size the fuselage on conventional aircraft. All other things being equal, increasing the tail's moment arm (to reduce tail size) lengthens the fuselage which is less structurally efficient than a shorter fuselage of the same volume.

As stated before, the Medium FW has no interference drag and only half of the separation drag of a conventional fuselage and wing configuration. When clean minimum drag coefficient ( $C_{Do}$ ) was examined, the Medium FW  $C_{Do}$  initially appeared to be very optimistic,

with about one third of the drag of the other Attack designs (fig. 15). However, the Medium FW's large wing area artificially reduces C<sub>Do</sub>.

To better understand this, drag coefficient is again plotted in figure 16, this time normalized by the aircraft total wetted area ( $C_{\mathrm{Dwet}}$ ) rather than wing planform area. Since skin friction typically accounts for 70% of subsonic

drag in a well designed aircraft, C<sub>Dwet</sub> is a better figure of merit for comparing Medium FW and conventional designs. Wetted area is a characteristic area that includes all of the drag-producing airframe components rather than just the wing. C<sub>Dwet</sub> shows that the Medium FW does not have an excessive drag advantage. The 16% lower C<sub>Dwet</sub> was expected and was due to the reduced boattail and interference drag of the Medium FW.

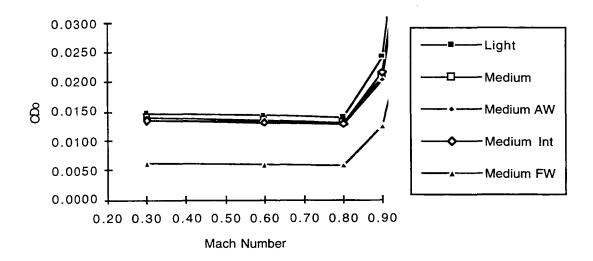


Figure 15. Zero lift drag coefficient vs. Mach number for 1995-TAD Attack aircraft without stores ( $C_{Do}$  referenced to wing area).

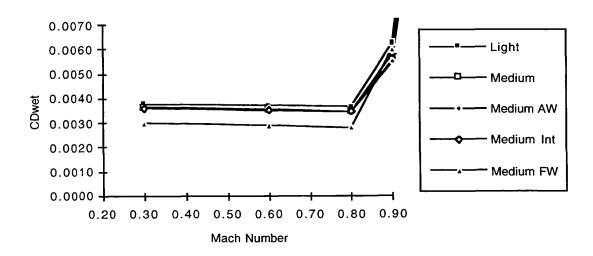


Figure 16. Zero lift drag coefficient vs. Mach number for 1995-TAD Attack aircraft without external stores ( $C_{Dwet}$  referenced to total wetted area).

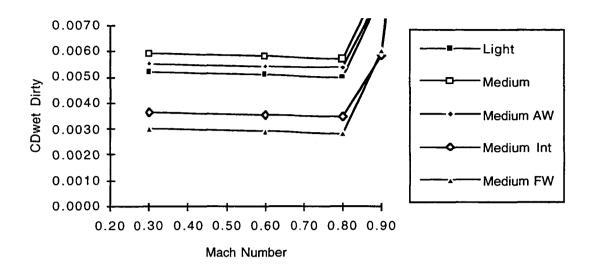


Figure 17. Zero lift drag coefficient vs. Mach number for 1995-TAD Attack aircraft with stores (C<sub>Dwet</sub> referenced to total aircraft wetted area).

Figure 16 shows that the Medium IW drag was similar to the external carriage designs because the drag plotted does not include stores. Figure 17 compares the drag of these aircraft with weapons, which is perhaps the most appropriate way to compare these aircraft. The aircraft with internal weapons show no increase in zero lift drag, but the parasite drag of the external stores adds 35% to the drag of the other designs. This is why the aircraft T/W for the external carriage designs, and therefore the TOGWs, are higher. Even without the bombs, the drag of just the external carriage equipment typically increases  $C_{\mathrm{Do}}$  by 17%.

Finally, in the event that our estimated  $C_{Do}$  was too low, the sensitivity of the Medium FW to  $C_{Do}$  was evaluated. The impact of a 50% increase in minimum drag (from 0.06 to 0.09) was to increase TOGW by 9.9% and the

Medium FW was still the lightest aircraft. This also demonstrates that the Medium FW's low  $C_{Do}$  contributed less to its low TOGW than did eliminating the vertical tail weight and drag, and the boattail, interference, and external weapon drags.

#### 5. Technology

Figures 13 and 14 do not show much change in Attack aircraft TOGW between the two technology timeframes. Figure 18 combines these data to show the aircraft weights decreasing slightly with improving technology. The improvements with increased technology levels are not very pronounced compared to the supersonic aircraft because the subsonic aircraft are less sensitive to weight changes (low growth factor) and the Interdiction design mission did not challenge the Attack aircraft at the technology levels used.

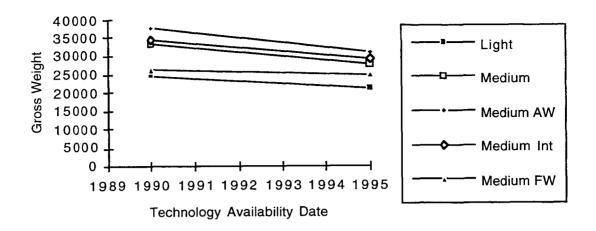


Figure 18. Effect of technology on Attack aircraft.

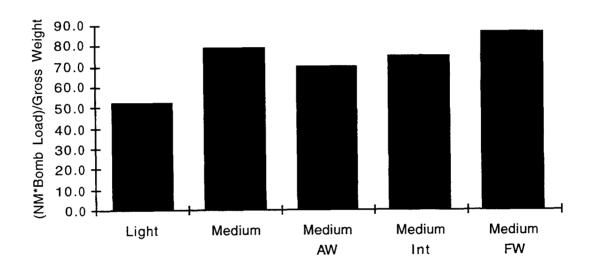


Figure 19. Comparison of range/payload capability of 1995-TAD Attack aircraft on the design mission.

#### 6. Range-Payload Efficiency

Figure 19 compares the relative range-payload efficiency of the 1995-TAD Attack aircraft types on their design mission since they do not have the same weapon load. Since aircraft weight is an indicator of cost, normalizing by TOGW was a simple way of evaluating the relative cost effectiveness of these aircraft. There appears to be an

economy of scale for the Medium Attack aircraft since one Medium Attack aircraft has the same range-payload capability as two Light aircraft even though it weighs 65% of the two Light aircraft. This analysis, of course, does not address the increased reliability and operational flexibility of operating two small aircraft compared to a single larger one.

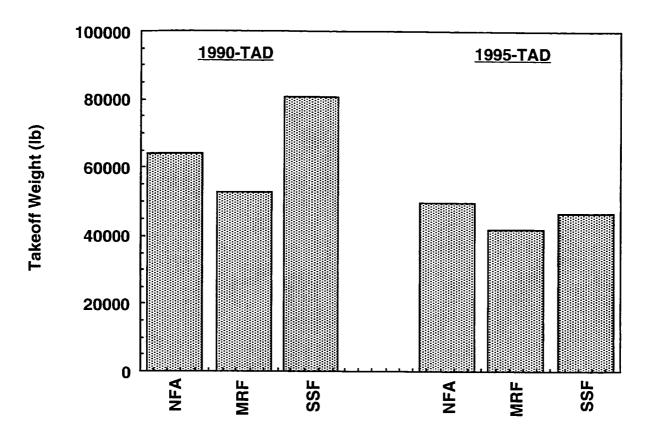


Figure 20. Comparison of baseline Multimission aircraft.

#### C. Multimission Aircraft Trends

Figure 20 shows that, as expected, the land-based aircraft (MRF) was the lightest in both timeframes. Access to a long runway yields the lightest aircraft design because the carrier slow approach requirement and structural reinforcements are weight drivers for the NFA.

The TOGW trends between the 1990-TAD and 1995-TAD timeframes in figure 20 are driven by the balance between improved technology and tougher requirements. These two trends oppose each other but figure 20 indicates that, for all of the aircraft, the technology improvements used in this study more than compensate for the tougher requirements. Since external weapons and carriage equipment increase drag by 25% over the clean aircraft at 0.6M, it is also reasonable to believe internal weapons benefit the supersonic Multimission aircraft.

Figure 20 also shows the surprising result that the SSF, for all the unique capability it offers, is approximately the same size as the NFA in the 1995-TAD timeframe.

Contrast this to the 1990-TAD timeframe where the SSF aircraft is by far the heaviest aircraft, which agrees with the long-held perception that STOVL capability costs a 20% increase in TOGW. Understanding the influence of requirements and technology level on the relative ranking of the SSF aircraft can shed light on this perhaps surprising result.

#### 1. Impact of Requirements

Table 19 summarizes the active sizing constraints for all of the Multimission aircraft. The most important change was that the 1995-TAD SSF's engine was sized, not by hover as in the 1990-TAD timeframe, but by the same dry supercruise requirement that sizes the engine for the other Multimission aircraft. The SSF was relatively insensitive to the additional supercruise and maneuver requirements of the 1995-TAD timeframe because it already had a high aircraft T/W in the 1990-TAD timeframe (its engine was sized for hover without thrust augmentation such as ejectors or burners).

Table 19. Active sizing constraints for Multimission aircraft

-	SSF	NFA	MRF
1990-TAD		-	
Wing size	Unconstrained	Waveoff	Maneuver
Engine size	Unconstrained Hover	Maneuver	Maneuver
1995-TAD			
Wing size	Maneuver	Maneuver	Maneuver
Wing size Engine size	1.5M dry	1.5M dry	1.5M dry

To explore this further, figure 21 shows the impact of requiring all three of the 1990-TAD aircraft to perform a dry supercruise. In this case, the aircraft TOGWs are closer because they are all being sized by the same requirements. The SSF weight in this figure is the same as the 1990-TAD SSF in figure 20 because it could already dry supercruise; the weight penalty associated

with its higher T/W provides the SSF with additional capability beyond merely improving maneuver and dash performance. Additionally, the dry supercruise requirement has a larger impact on the NFA than on the MRF because of the NFA's navalization weight penalties.

Since the wing and engine for all of the 1995-TAD aircraft were sized by the same requirements (table 19), it was the sum impact of the aircraft differentiators which determines the ranking of these aircraft. In this case, the SSF has a similar TOGW to the NFA because the two aircraft have roughly equal weight "penalties" (structural for the NFA versus propulsion system for the SSF).

It is also interesting to compare these dry supercruise aircraft to the 1990-TAD SSF because the effect of technology improvement is more nearly isolated from the dry supercruise requirement. The effect of changes in the maneuver requirements and weapon carriage is that the 1995-TAD aircraft are about 35% lighter than the 1990-TAD aircraft.

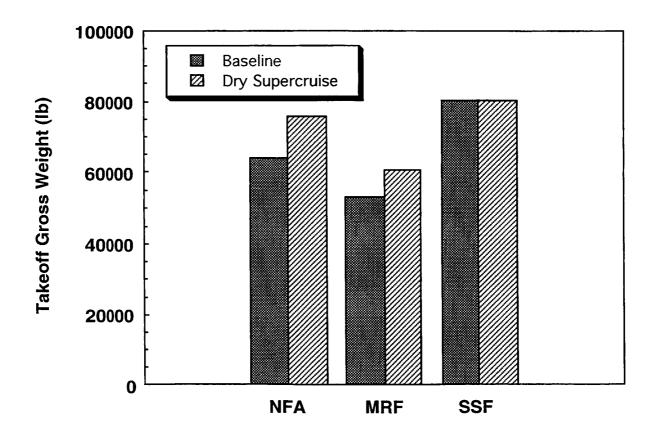


Figure 21. Effect of requiring dry supercruise for 1990-TAD Multimission aircraft.

The impact of allowing the 1990-TAD SSF aircraft to augment its thrust in hover was also evaluated. The 1990-TAD SSF (fig. 20) propulsion system operates in hover mode without augmentation (such as ejectors or burners). This produced the high aircraft T/W which allows the aircraft to perform a dry supercruise. Figure 22 compares the baseline MRF and NFA to an SSF aircraft with thrust augmentation in hover. In this case, the SSF's engine is sized for up-and-away performance like the NFA and its weight is similar to the NFA. Again, the carrier-landing penalties are similar to the STOVL weight penalties. For this study, hover thrust augmentation was provided by afterburners in the lift nozzles without any weight penalty. In other words, this was an ideal augmentation scheme and the resulting aircraft was somewhat optimistic.

These comparisons highlight the tremendous impact mission requirements have on these aircraft. The bottom line is that with dry supercruise, or perhaps some other maneuver requirement, the T/W required for both hover and up-and-away mission requirements are well matched, even for STOVL concepts with little or no augmentation. In this study, the 1995-TAD mission requirements are similar to ATF-level requirements, even though the 1995-TAD technology levels in this study are higher than ATF levels.

It is interesting that the hover sizing of the engine has historically been STOVL's Achilles' heel. Typically, to have sufficient thrust for hover required an oversized engine with its excessive propulsion weight and fuel consumption during cruise. This led to the development of numerous vertical thrust augmentation schemes, all of which increase weight, cost, and development risk (e.g., poor transition performance). With increasing mission requirements for tactical aircraft in the future, hover may cease to be the engine sizing condition and may not be the major STOVL TOGW driver it has been in the past.

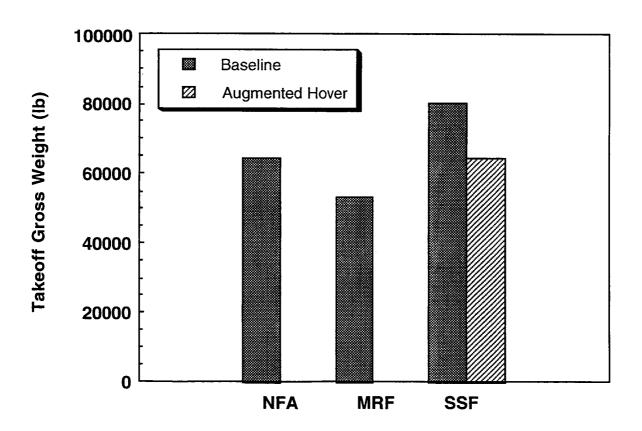


Figure 22. Effect of hover thrust augmentation on 1990-TAD SSF.

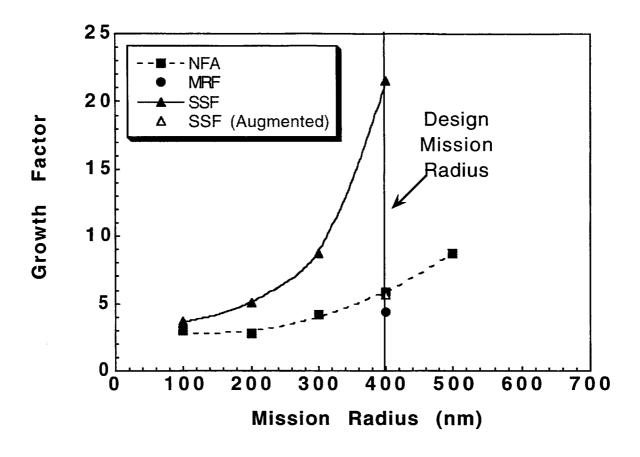


Figure 23. Comparison of growth factor for the 1990-TAD aircraft.

#### 2. Impact of Technology

The impact of changing technology on Multimission aircraft can be understood in terms of aircraft growth factor. In turn, growth factor trends (as a function of aircraft TOGW) can be generated by resizing aircraft with varying mission requirements. The growth factor data for the 1990-TAD aircraft presented in figure 23 were calculated by first sizing each aircraft type for missions of varying length and then resizing the resulting aircraft with an a small fixed weight added. For completeness the growth factor for the augmented SSF (from fig. 22) is also shown. For reference, currently existing aircraft in the Multimission class typically have a growth factor of approximately 3.5–4.0.

At the mission range of interest, the NFA growth factor

Even though STOVL aircraft tend to grow very quickly at comparatively lower requirement levels, all aircraft have mission requirements that result in unacceptable growth factor. For example, 400 nm range appears to be a difficult requirement for the NFA in the 1990-TAD timeframe.

is fairly high, but the SSF growth factor is unacceptable. The SSF is heavy enough that its TOGW is much more sensitive to mission requirements than the NFA at this range. The SSF growth factor is excessive because it has no thrust augmentation in hover and must support its entire empty weight in hover. This drove engine size up with a subsequent cyclic increase in empty weight, which resulted in the engine being oversized for the up-and-away parts of the mission. Contrast this to conventional aircraft which generate lift relatively efficiently at landing speed with its wings.

<sup>&</sup>lt;sup>9</sup>Aircraft also have growth factor trends relating to other requirements such as weapons load, speeds, maneuver requirements, etc.

One option to bring the 1990-TAD SSF's growth factor to a level comparable to the other aircraft's is to reduce the mission requirements. This is historically what has been done to produce a viable STOVL concept without augmentation, such as the Harrier AV-8A which did not have the mission capability of its conventional counterparts. Another option is vertical thrust augmentation to prevent over-sizing the engine. However, development of an augmented propulsion system incurs additional weight, development risk, and cost.

Figure 24 shows the growth factors for the 1995-TAD aircraft. More difficult requirements tend to shift the curves to the left and technology improvements shift the curves to the right. The curves in the figure have shifted to the right so that at the desired mission range, the growth factor for the SSF is nearly the same as the NFA. Improvements in engine T/W and structural weight from

the 1990-TAD to 1995-TAD timeframe confer greater benefits on the SSF than the other aircraft because they both directly affect hover weight which was the engine sizer using lower technology. This is an important factor in understanding why the SSF aircraft is in the same weight class as the conventional aircraft in the 1995-TAD timeframe. Note that the MRF still has the lowest growth factor.

Note that if the 1995-TAD range requirement had been increased to 600 nm, for example, the SSF would have again been an unfeasible design without some type of thrust augmentation in hover. This growth factor sensitivity shows that STOVL aircraft competitiveness with conventional aircraft depends on its size. STOVL aircraft will not be competitive with conventional aircraft beyond a certain level of requirements such as mission range.

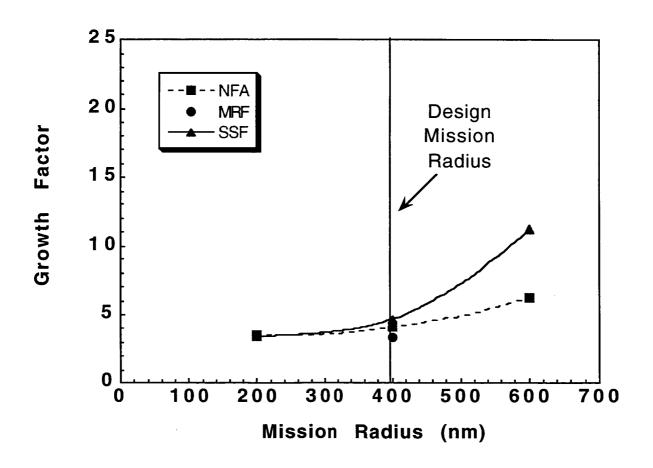


Figure 24. Comparison of growth factors for the 1995-TAD aircraft.

Figure 25 compares the fuel fraction (weight of fuel divided by TOGW) of the 1990-TAD Multimission aircraft to existing inventory aircraft. Both the SSF and NFA have fuel fractions that are considerably higher than existing aircraft at 400 nm and comparable to them at 200 nm. Notice that a reasonable growth factor (fig. 23) also occurs at 200 nm. If a fuel fraction of 30% is taken to be a practical upper limit, one could conclude that the upper limit to mission radius for these aircraft in this timeframe is 200–250 nm and that a growth factor of 5 represents a maximum upper limit.

From the foregoing discussion, it is clear that the SSF aircraft was more sensitive than its conventional counterparts to the 400 nm mission range used in this study. Also, remember that the design mission used in this study was somewhat oversized. These two factors together explain the extreme size of the 1990-TAD SSF.

#### 3. Impact of Hover T/W required

Hover T/W was one of the most important aircraft design parameters for the STOVL aircraft. Unfortunately, this

value is made up of several elements that are difficult to estimate at the conceptual design stage (suckdown, hot gas reingestion, power extraction for attitude control, etc.). Since the 1995-TAD SSF's engine was not sized by the required 1.16 hover T/W, the impact of a T/Whover requirement of 1.257 and 1.345 was analyzed. This shows the impact of requiring an increase in hover T/W in the event that, for example, unexpectedly high levels of suckdown were encountered during development. Figure 26 shows the SSF TOGW compared to the baseline NFA and MRF (indicated by horizontal lines). The TOGW of the SSF is relatively insensitive to T/Whover. The SSF was actually lighter than the NFA until a T/Whover of ~1.3 was required. Since this study was conceptual in nature, it is not very important which aircraft was actually lighter, but it is important that the required T/Whover assumed in this study does not invalidate the conclusion that the 1995-TAD SSF is comparable in weight to the NFA.

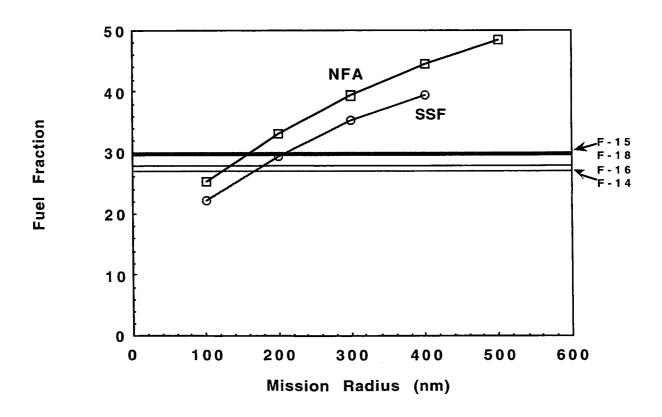


Figure 25. Fuel fraction of 1990-TAD Multimission aircraft as a function of mission radius.

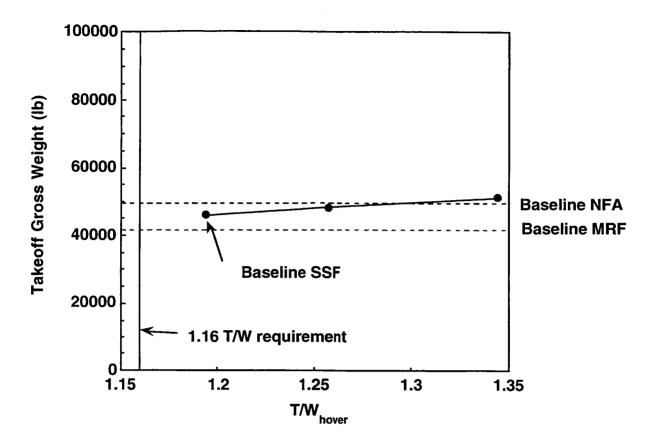


Figure 26. Effect of hover thrust-to-weight on the 1995-TAD SSF aircraft.

#### D. Operational Mission Performance Data

Some of the aircraft were evaluated to determine their operational capability in the DLI, CAP, and Strike roles. NFA, SSF, and MRF performance is so similar that they are reported here (and in the figures) as "Multimission." Also, mission radius reported in this section is only for the fallout cruise segment and does not include climb, combat, and acceleration. See Appendix C for a description of these SSF DOC missions.

The Strike and DLI missions were flown exactly as specified in the SSF DOC. The Strike mission was used to determine the mission radius as a function of the number of bombs carried. The DLI mission was used to evaluate the effect of cruise Mach number on mission radius and dash capability. To evaluate CAP capability, the Fighter design mission was used to examine the impact of loiter time on mission radius. The original SSF DOC CAP mission was not used because it did not have a supersonic cruise segment. On all of these fallout missions, weapons were released, as specified in the SSF DOC missions, rather than retained as they are in the design missions.

#### 1. Strike Range vs. Payload

The strike mission operational fallout measures the tradeoff between the number of bombs carried and mission radius. Results are shown in figure 27 for the 1995-TAD aircraft. The 50 nm ingress phase was added to the fallout cruise segment so that total radius is reported.

In general, fallout performance at design TOGW with extra payload was poor because a high percentage of fuel was off-loaded to maintain TOGW. Since the Fighter and the Medium Attack aircraft were designed to carry four weapons, fuel was added to maintain design TOGW when carrying only two bombs. Similarly, a payload of four or more bombs exceeds design load for the Light Attack and Multimission aircraft so fuel was removed to maintain design TOGW. For all of the Medium Attack designs, the fifth bomb was mounted on a short, centerline pylon and fuel was removed to maintain design TOGW. The maximum number of bombs carried is ten for the Multimission and eight for the Fighter with dramatic reductions in the fuel load.

Performance of the 1995 Medium FW falls off dramatically when carrying five bombs. This was due to the addition of parasite drag and weight for the fifth bomb and, more importantly, the loss of fuel. Of the total 4,127 lb of design fuel load, only 1,803 lb was used for the original design mission cruise phases. Subtracting 1,291 lb for the fifth bomb and its carriage equipment yields only 512 lb of fuel (a 60% decrease) for the Strike cruise phase. Notice that, at design TOGW, the Multimission aircraft can carry four bombs further than the Light Attack aircraft (Attack weighs half as much as the Multimission). This is because the Light Attack aircraft was small and, as a result of its all-subsonic mission, has a low fuel fraction compared to aircraft with supersonic mission segments.

Another important consideration is that an aircraft may not be able to land with all of the bombs it took off with. The Medium Attack aircraft, for example, was designed to meet the 1.5g waveoff maneuver carrying the design

bomb load and any extra load must be jettisoned prior to landing. Only the Medium FW has the excess waveoff capability to bring back the extra bomb.

A second method of evaluating strike performance is at an overload TOGW condition (called overload in fig. 27) that takes advantage of the extra capability inherent in Fighter and Multimission aircraft with their high T/W and high structural limits. The range of aircraft operated this way was considerably better than for aircraft with less than design fuel. The maximum overload TOGW (~120% of TOGW) for each aircraft includes full design fuel load and either ten bombs for the Multimission aircraft or eight for the Fighter aircraft. To evaluate an aircraft and hold its maximum overload TOGW constant, bombs were traded for fuel in external tanks to generate these sensitivity numbers. In other words, overload weight is determined by adding the maximum number of bombs. This overload weight is held constant by adding external fuel as

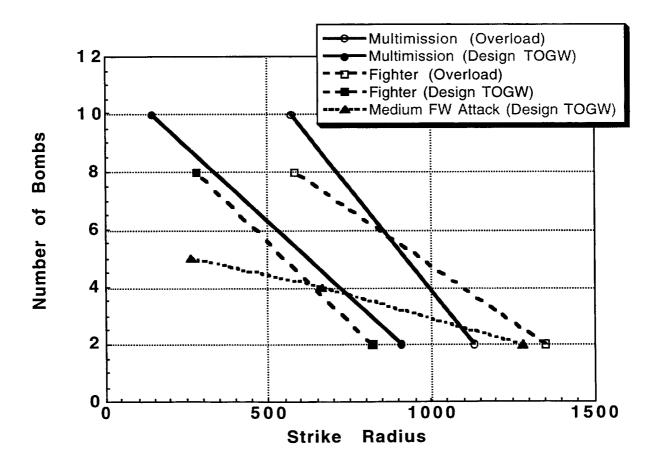


Figure 27. 1995-TAD strike fallout performance.

weapons are removed. External tanks were dropped when all external fuel was consumed. Of course, these aircraft operated above design TOGW have reduced speed and maneuver capability and most cannot land on a carrier with more weapons than their design load because of the increased wing loading.

#### 2. DLI Range vs. Mach Number

The SSF DOC DLI mission was used to evaluate the influence of outbound dash Mach number on mission

radius. Since the DLI mission requires two SRMs and four LRMs, the Multimission aircraft carry two additional LRMs and are slightly above design TOGW. Results are shown in figures 28 and 29. Range increases steadily with Mach number until 0.9 Mach because SFC for the low bypass supersonic engines improves more quickly with Mach number than the drag increases. At 0.9M, mission capability falls off dramatically due to the increase in compressibility drag.

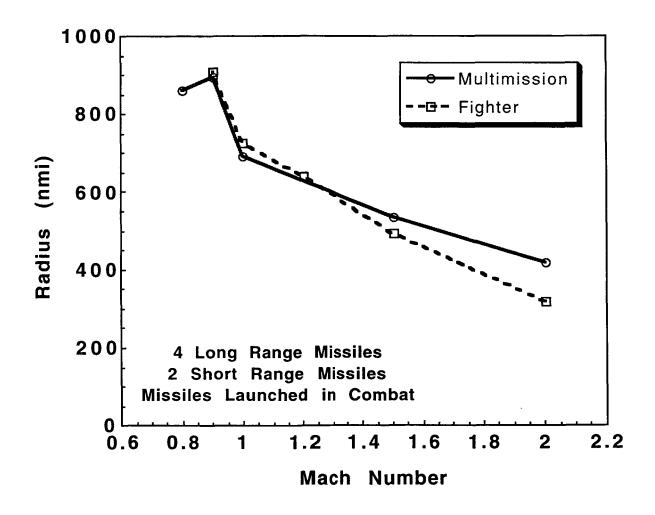


Figure 28. 1990-TAD DLI fallout performance.

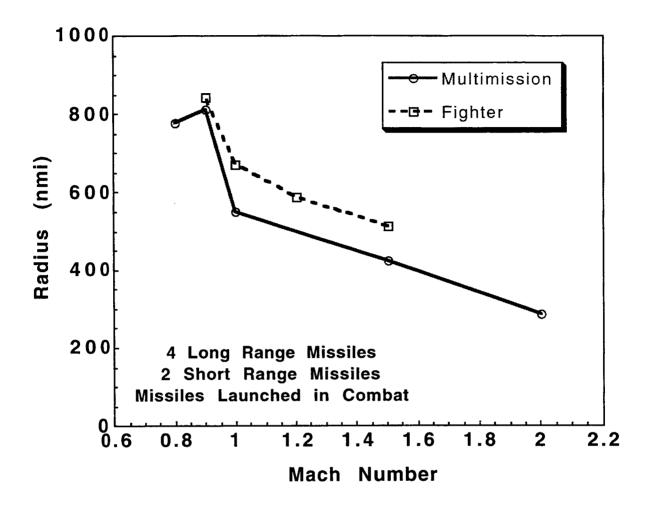


Figure 29. 1995-TAD DLI fallout performance.

In the 1995-TAD timeframe, the performance of the Multimission aircraft is degraded compared to the Fighter. This is because the 1990-TAD Multimission class carries all four LRMs for the DLI mission externally, while stealth versions in the 1995-TAD timeframe carry the second set of LRMs externally. Adding two more LRMs to the existing pylons on the 1990-TAD aircraft was a relatively small addition to total aircraft

drag. However, in the 1995-TAD timeframe, the addition of two pylons and the missiles was a significant penalty. The Fighter aircraft has approximately the same performance in both timeframes because it was designed to perform the same mission in each timeframe and there were no configuration changes.

For the Multimission aircraft, an appropriate outbound cruise altitude was determined for each Mach number to ensure efficient engine operation, as shown in figure 30. The Fighter aircraft was able to cruise efficiently at 50,000 ft over the Mach number range examined. Acceleration and climb phases were also modified to preserve mission continuity as cruise altitude and Mach number varied. For example, an aircraft was required to climb to the appropriate cruise altitude and also had to accelerate for combat at 1.5M if cruising below 1.5M. No range credit was given for descent from cruise to combat altitude or for deceleration from cruise to combat Mach number.

#### 3. CAP Range vs. Loiter Time

The trade-off between mission radius and loiter time on station was evaluated for the Fighter and Multimission classes using the Fighter design mission (the modified SSF DOC CAP mission). This fallout was analyzed both with the mission radius held constant and with the dash range held constant. The weapons, two SRMs and two LRMs, were released as specified in the original mission. For the Fighter, the two extra LRMs and mounting hardware were removed and extra fuel was added to maintain design TOGW.

Figures 31 and 32 show results for supersonic dash capability versus loiter time at a fixed mission radius in both timeframes. Supersonic dash range was determined with a fixed 400 nm subsonic cruise out and back to the loiter station. As before, the fighter's fallout performance did not change significantly from the 1990-TAD to the 1995-TAD timeframe. This is because it was designed for the same capability in each timeframe. However, the Multimission aircraft improved in the 1995-TAD timeframe because the weapons were carried internally.

Note that the Fighter flies further on the fallout mission with 60 minutes of loiter than it does on the design mission with 60 minutes of loiter. This is because the fallout weapon load used in the fallout mission is one half of the design weapon load and the weapons are dropped during the fallout mission, reducing weight and drag for the return cruise.

Figures 33 and 34 show very similar results for subsonic mission radius capability versus loiter time with a fixed supersonic dash in both timeframes. The fallout data shown is the mission radius using a constant 100 nm lateral supersonic dash to intercept.

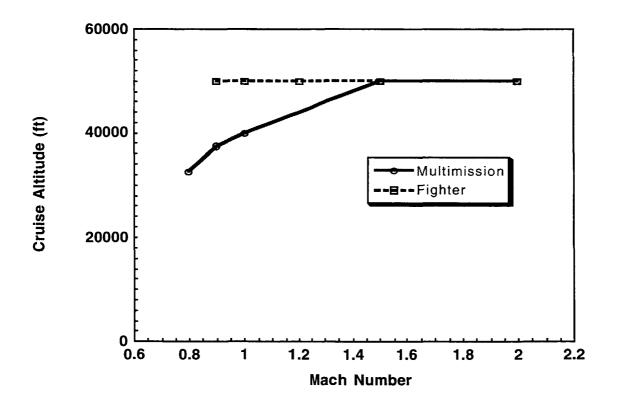


Figure 30. 1995 DLI cruise altitude.

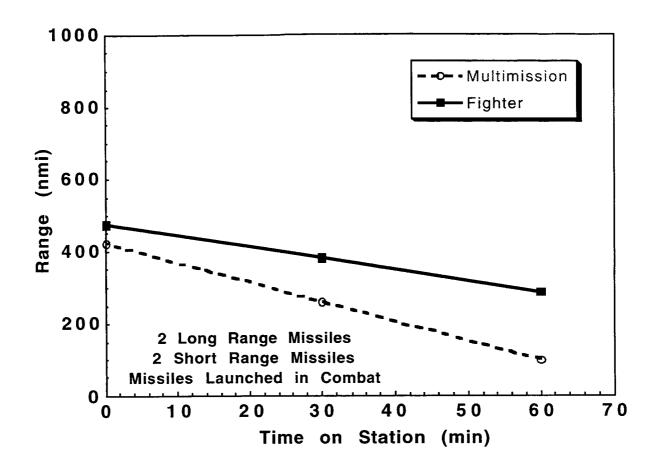


Figure 31. 1990-TAD CAP supersonic dash fallout performance with 400 nmi subsonic cruise.

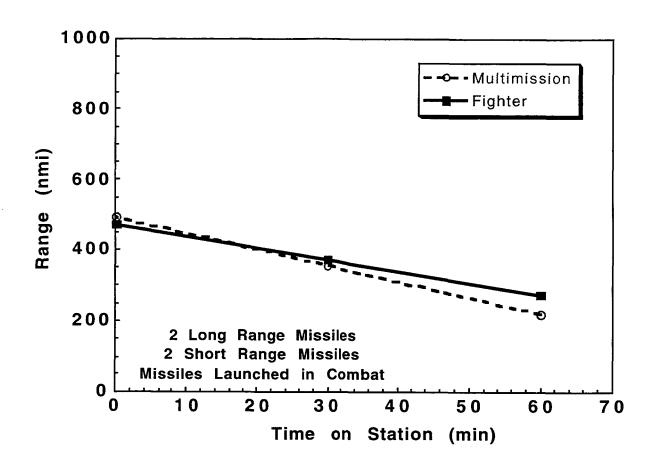


Figure 32. 1995-TAD CAP supersonic dash fallout performance with 400 nmi subsonic cruise.

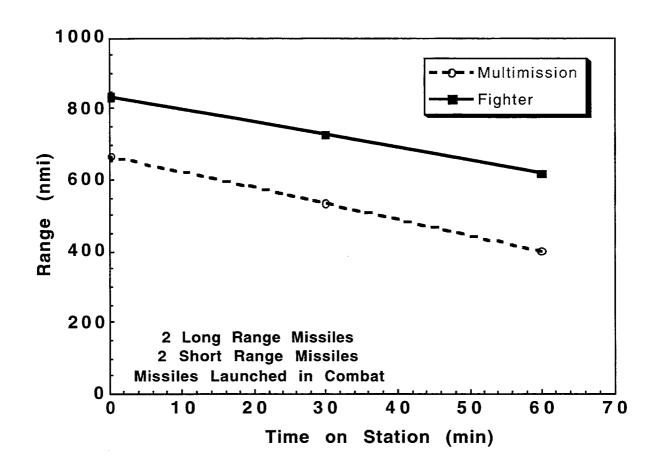


Figure 33. 1990-TAD CAP subsonic cruise fallout performance with 100 nmi supersonic dash.

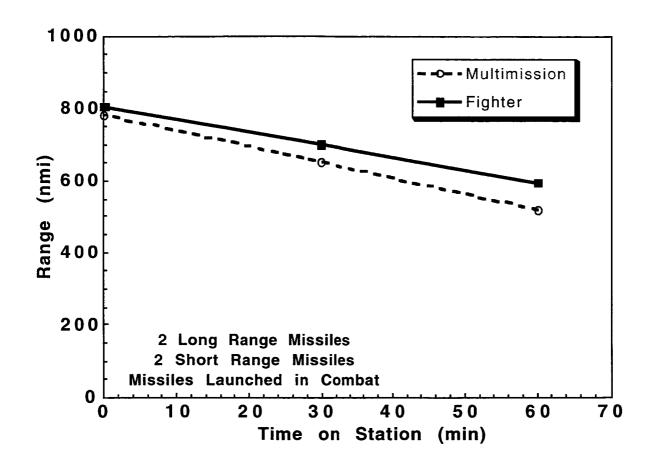


Figure 34. 1995-TAD CAP subsonic cruise performance with 100 nmi supersonic dash.

## E. SSF DOC Mission Fallout Range Performance Data

Each aircraft class was evaluated to determine its radius of action on the original SSF DOC missions (see Appendix B for mission definitions). These missions were run as nearly as possible to the SSF DOC specification, and the offensive/defensive weapons were released during combat. The results can be used with the payload specified in each mission to evaluate operational effectiveness.

An attempt was made to keep TOGW within 3% of design by either adding or removing fuel depending on the difference between the DOC mission's weapon load and design weapon load. For the Fighter and Medium Attack aircraft, the SSF DOC weapon loads were lighter than the design weapon load so additional fuel and external tanks were added. For the Light Attack aircraft, the TOGW was within 2% of design with each of the SSF DOC weapon loads so no modifications were made. The

Multimission aircraft were slightly above design TOGW on all the missions, except for the reconnaissance and Suppression of Enemy Air Defenses (SEAD) which required additional fuel (carried internally for reconnaissance) to maintain design TOGW. Additional tankage was provided by either a single fuel tank mounted on a short, centerline pylon or a single, form fitting fuel tank mounted in an empty bomb bay. Since the amount of fuel necessary to bring each aircraft up to design TOGW varied, most of the extra tanks were only partially filled. External tanks were dropped when they were empty.

In the following figures, total mission radius is reported consistently for all missions. This means that for missions with a specified 50 nm ingress/egress, the 50 nm was added to the fallout cruise range so that total mission radius is being reported. Also, results for the Medium FW aircraft are used to represent the Attack class because it was the lightest of the Medium Attack aircraft. SSF, NFA, and MRF performance are essentially the same and

are reported in this section as "Multimission." Finally, for the Reconnaissance mission the sensor package was assumed to weigh the same as the gun plus ammunition (899 lb). Table 20 lists the primary weapons for each of the fallout missions.

#### 1. Aircraft Class Comparison

Figure 35 shows fallout range performance for the 1995-TAD Fighter, Multimission, and Attack classes on subsonic SSF DOC missions. All aircraft classes exceed the DOC range requirements, even the aircraft designed for supersonic flight. This results from the large fuel capacity of the supersonic aircraft and, for the fighter, additional fuel carried because the payload weight for these fallout missions was less than design weapon load. Figure 36 compares the relative range-payload efficiency for the same aircraft and missions. Since aircraft weight is an indicator of cost, normalizing by TOGW was a simple way of evaluating the relative cost effectiveness of these

Table 20. Primary weapons for fallout missions

Fallout mission	Primary weapons load		
Multimission design mission	2 LRMs		
Deck launched intercept	4 LRMs		
Air defense/combat air patrol	2 LRMs		
Suppression of enemy air defenses	2 HARMs		
Close air support	4 Rockeyes		
Interdiction	2 LGBs		
Recon	Sensors (899 lb)		

aircraft. This metric shows that, for these subsonic missions, the subsonic aircraft actually have a 2-to-1 advantage in capability versus cost when compared to the supersonic aircraft.

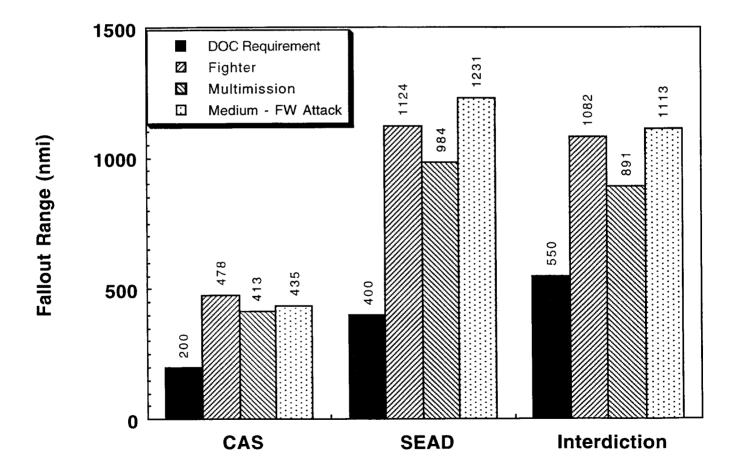


Figure 35. 1995-TAD fallout range performance on the SSF DOC subsonic missions.

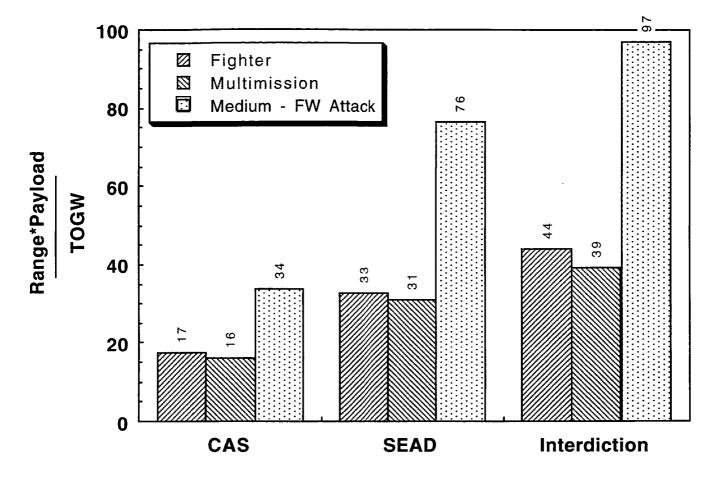


Figure 36. 1995-TAD mission effectiveness on SSF DOC subsonic missions.

Figure 37 shows fallout range performance for the supersonic SSF DOC missions. Both aircraft classes exceed these requirements; the Multimission aircraft range substantially exceeds the requirements because the design mission created for this study was quite demanding. This is shown by the fuel fraction of the Multimission aircraft (0.40–0.45) which is high compared to typical F-14, F-15, F-16, and F-18 fuel fractions (~0.3). Also included in this figure is aircraft performance on the Multimission design mission created for this study. The

Multimission aircraft performance is slightly different due to different rules applied to fallout missions. Figure 38 shows the relative range-payload efficiency of the supersonic aircraft on the fallout missions. Comparing figure 36 to figure 38 quantifies the tremendous impact supersonic flight has on aircraft range-payload efficiency. These results also indicate that increasing the ratio of supersonic cruise to subsonic cruise in the Multimission design mission would yield an aircraft with capability that was more balanced for meeting the SSF DOC missions.

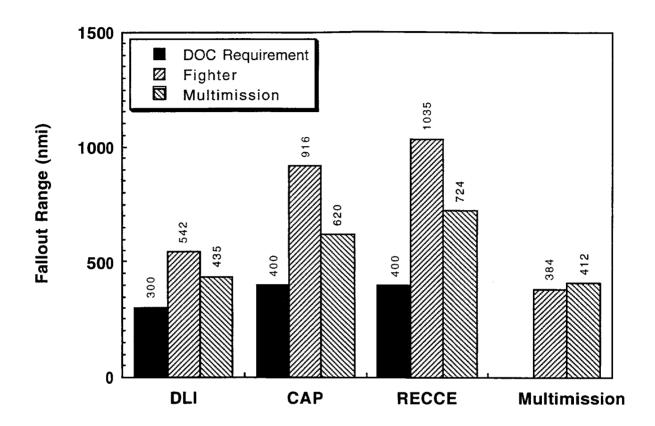


Figure 37. 1995-TAD fallout range performance on the SSF DOC supersonic missions.

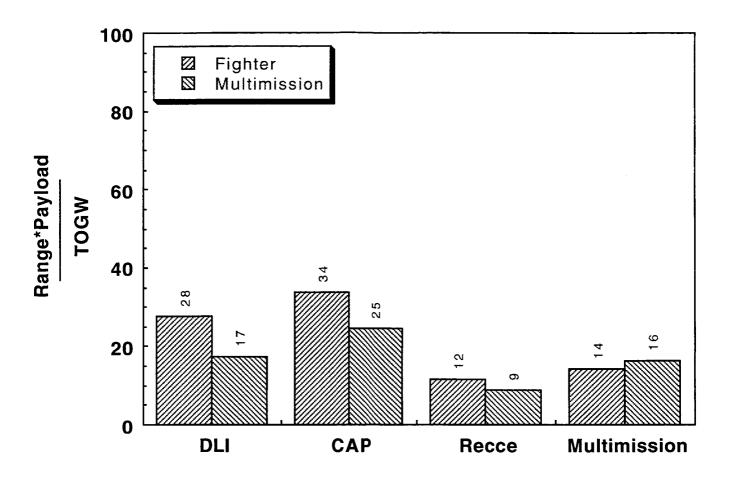


Figure 38. 1995-TAD mission effectiveness on the SSF DOC supersonic missions.

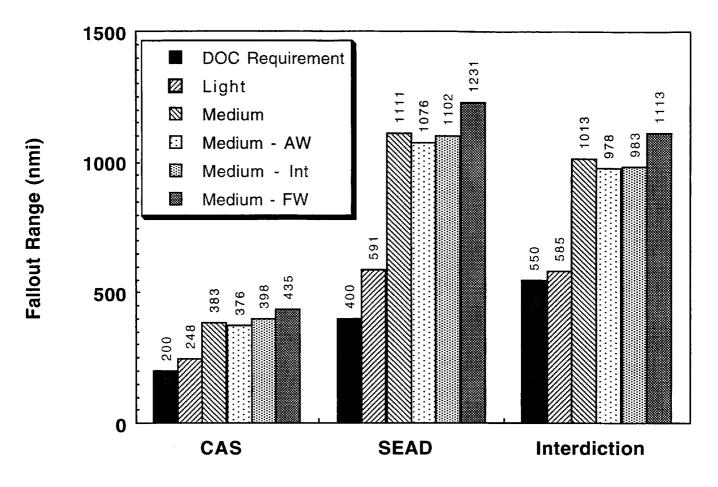


Figure 39. 1995-TAD Attack aircraft fallout range performance on the SSF DOC subsonic missions.

#### 2. Attack Aircraft Comparison

Figure 39 compares the fallout range performance for all of the 1995-TAD Attack aircraft on the subsonic CAS, SEAD, and Interdiction missions. All the Medium aircraft have similar performance.

The CAS mission is unique because it is the only fallout mission that is executed entirely at sea level. The primary weapon load for this mission is four Mark-20 Rockeye Mod II bombs which together are lighter than, but have more drag than, the design weapon loads for each of the aircraft. Figure 39 shows that all aircraft exceed the 200 nm requirement and the Medium Attack designs exceed it by more than a factor of 2.

No fuel was added to the Light Attack because the fallout weapon load only differed from the design load by 138 lb, which is less than the weight of the short pylon required for the drop tank. Therefore, the Light Attack started the mission slightly under design TOGW with full internal fuel.

The Medium and Medium AW aircraft were able to take advantage of the reduced weapon load and carry additional fuel externally as was previously described.

The Medium IW and Medium FW were not able to carry the additional fuel internally because most of each bay was occupied by a Rockeye bomb. Additional fuel was therefore carried in a single drop tank mounted on a short centerline pylon. This arrangement does not interfere with the Medium IW's weapon bay doors because the tank was assumed to be dropped before the bombs. The Medium FW's weapon bays are located outboard of the centerline and do not interfere with the external tank.

The SEAD fallout mission results are also shown in figure 39. The primary weapon load for this mission is two AGM-88A HARM missiles, which is lighter than the design load for each of the Attack aircraft. All aircraft exceed the 400 nm requirement and the Medium designs have more than twice the required range. The Light Attack aircraft did not carry any additional fuel while the Medium designs carried enough to maintain TOGW.

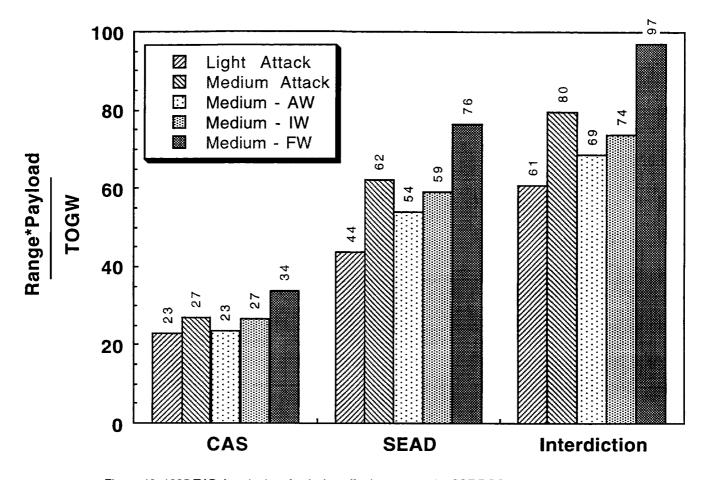


Figure 40. 1995-TAD Attack aircraft mission effectiveness on the SSF DOC subsonic missions.

Since two missiles fit in one of the weapon bays, additional fuel for the Medium IW and Medium FW was placed in the second bay.

The Light Attack aircraft has the least range on the Interdiction mission (fig. 39) because its original design load consists of two bombs so it did not receive any additional fuel like the other aircraft. All of the designs exceed the 550 nm requirement, and the range performance of all of the Medium Attack designs exceeds this requirement by approximately a factor of 2. The Medium FW has the best range.

For comparison with figure 36, figure 40 shows relative range-payload efficiency data for all aircraft in the Attack class.

#### F. Propulsion Sensitivities

Several independent sensitivities (table 21) were evaluated to understand the influence on TOGW of

propulsion modelling in this study. TOGW was quite insensitive to the items examined.

Table 21. Propulsion sensitivities

Sensitivity	ΔTOGW (%)
Twin vs. single engine 1990 Fighter	5.0
Engine weight growth exponent from 1.05 to 1.0 (1995 STOVL)	-1.6
Constant engine T/W for Attack aircraft	~1
Constant core size engines (new T/W and EXWT = 1.0):	
Fighter	0.6
Attack	-1.0
Multimission	-0.6

The first sensitivity assessed the impact of the decision to size all aircraft in this study with a single engine. The single engine in the 1990-TAD Fighter aircraft was replaced by two engines that were scaled 50% in thrust and weight. The resulting aircraft was 4.1% heavier due to engine installation penalties.

The sensitivity of TOGW to engine T/W was evaluated for the Attack aircraft class. All Attack aircraft use the same engine but the engine scale factor varies by as much as a factor of 2. As previously mentioned, engine T/W varies slightly with engine scale. To check the possible impact this T/W variation had on the study, the heaviest Attack aircraft's engine was modified to have the same T/W as the engine in the lightest aircraft. The impact on TOGW was 1%.

Two additional propulsion sensitivities were performed to address whether or not the approach used to generate the

engine database had any major effect on this study. First, to evaluate the influence of the engine weight growth exponent on TOGW, the 1995-TAD SSF was resized using an exponent of 1.0 (instead of 1.05) which increased the engine T/W. The TOGW of this aircraft was reduced by only 1.6%. Second, engine families could have been generated by the engine software with either constant inlet mass flow or constant core mass flow. This choice affects engines T/W slightly. A constant inlet mass flow was used to generate the basic, unscaled engine decks used in this study. To determine the impact this had on TOGW, aircraft from each class were resized with new engines that were generated using a constant core mass flow. The resulting change in TOGW was 1% or less for all of the aircraft.

#### **Section V – Conclusions**

This study highlights the effect of changing requirements on the penalties associated with STOVL capability and addresses the penalties associated with carrier compatibility. Of course, each of these weight penalties results from increased aircraft capability. This study also identifies the Medium FW as the favored concept for Attack aircraft and examines the impact of internal weapons carriage on subsonic Attack aircraft. The success of this study rests on its ability to establish trends amongst aircraft sized with consistent methods.

#### A. Multimission Aircraft Comparison

The "STOVL penalty" is largest in a low technology timeframe compared to a land-based aircraft that has no dry supercruise requirement. This accounts for the long held perception that STOVL capability costs a 20% increase in TOGW. However, the SSF has little or no penalty, compared to future technology multimission seabased aircraft, when dry supercruise is a requirement. In addition, STOVL aircraft derive greater benefits from improved structures, materials, and propulsion system T/W than their conventional counterparts.

The requirements imposed on the 1995-TAD aircraft in this study are similar to current requirements for new aircraft. These dry supersonic cruise and maneuverability requirements result in aircraft with a T/W which is high compared to current inventory aircraft. An SSF aircraft designed to these requirements will require little or no augmentation in hover, thus reducing the cost, risk, and weight penalties associated with STOVL. In fact, in the 1995-TAD timeframe of this study, the SSF weight penalty was comparable to the navalization weight penalty but STOVL aircraft should provide additional operational and safety advantages for carrier operations.

Many of the technologies for STOVL-related systems are already being developed for conventional and/or current aircraft. Examples are 1) high T/W engines, 2) the current development in thrust vectoring/reversing systems (F-15 STOL/Maneuvering Technology Demonstrator (S/MTD)), and 3) advanced control systems for STOVL aircraft (NASA Ames' Harrier V/STOL Research Aircraft, ref 14).

#### **B.** Attack Aircraft Comparison

Technology improvements had less effect on the Attack aircraft than on the Multimission aircraft, due primarily to

the lower growth factor of subsonic aircraft. The addition of two more laser guided bombs on the Light Attack aircraft had more impact on the TOGW than the addition of a second crewmember.

The Medium FW aircraft is the lightest design in the Medium Attack class mainly because of its reduced interference and boattail drag. It is important to compare the drag coefficient of flying wings to conventional aircraft using C<sub>D</sub> based on total wetted area rather than on wing area.

Attack aircraft designs with internal weapons are lighter than those with external weapons, given the assumptions and estimates used in this study. This is because the reduction in stores drag more than compensated for the impact of the increased weight and volume of the internal weapons bays.

#### C. Design Study Recommendations

Clear conclusions are most easily made when a conceptual aircraft sizing study is performed as a trend or sensitivity study. Attempting to compare study results to existing aircraft requires that study aircraft be sized to the same constraints and requirements as the reference aircraft, which is very difficult. Similarly, it is impossible to predict actual technologies that will be available, so it is more valuable to make reasonable estimates and apply them consistently to all aircraft. It is very important in any conceptual design study to isolate configuration similarities from differentiators that will drive aircraft trends. Similarities, like technology assumptions, can be relatively simple estimates since they are applied to all aircraft, including the reference aircraft. The study results and trends can then be interpreted in terms of the differentiators. It is a good practice to determine TOGW sensitivities to changes in the more important, or less certain, differentiators. In large design studies several organizations may contribute designs to the database. In this case, any similarities that are not important to the study being conducted (e.g., equipment, weapons and carriage, engine decks, or mission details) should be agreed upon as part of the study groundrules and then applied to all designs so that different assumptions do not have to be normalized out of the final designs to allow fair comparison.

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# **Appendix A – Detailed Information for Aircraft**

#### **Summary Description**

Standard English units are used throughout the aircraft data in this appendix unless specifically noted: weight is in pounds, dimensions are in feet, angles are in degrees, time is in minutes, and ranges are in nautical miles. Abbreviations used only in this appendix are listed here rather than in the body of the report. Aircraft are listed in the same order as in the summary data in table 16. For most of the aircraft, instantaneous combat specific excess power (PSI) is positive for one or more maneuver conditions. This is because the turn capability at the 15° alpha limit (ALI) is sustainable. The takeoff fuel allowance is for 10.5 minutes: 10 minutes at idle and 30 seconds at maximum thrust.

#### General:

TOCW

TOGW	Takeoff Gross Weight (lb)		
W/S	Wing loading (lb/ft <sup>2</sup> )		
T/W Dry	Aircraft Thrust/Weight – Maximum Dry Thrust		
T/W A/B	Aircraft Thrust/Weight – Maximum Afterburning Thrust		
N(Z) Ult	Ultimate Load Factor (g)		
Engine:			
Length	(ft)		
Diam.	(ft)		
Weight	(lb)		
TSLS	Thrust, Sea Level Static (lb)		
SFCSLS	Specific Fuel Consumption, Sea Level Static (lbfuel/[lbthrust*hr])		
Fuselage:			

Toksoff Gross Waight (lh)

#### Fuselage:

Length	(ft)		
Diameter	(ft)		
Volume	$(ft^3)$		
Wetted Area	(ft <sup>2</sup> )		

#### Geometry:

T/C	Thickness-to-chord ratio
M.A.	Mean Aerodynamic
L.E.	Leading Edge

#### Mission Summary:

g)
ht
us

#### **Weights Description**

The individual fixed equipment component weights reported on the detailed weight statements are not adjusted for technology factor; the fixed equipment total is adjusted, however. Therefore, the sum of the individual fixed equipment weights does not equal the total group weight listed. To calculate the individual fixed equipment component weight, multiply the weight shown by the technology factor indicated.

#### **Propulsion Description**

Detailed engine data presented are scaled. In the case of engines with afterburners, the first engine point listed as 100% power is for maximum afterburner and the second 100% power point is for maximum dry thrust.

ESF	Engine Scale Factor, relative to engine table at ESF = 1.0
T/W	Thrust/Weight
FFLOW	Fuel flow
WAF	Weight of engine airflow
POWER	Power setting (%)
SFC	Specific fuel consumption (lbfuel/[lbthrust*hr])

#### **Aerodynamics Description**

Sample aerodynamics are shown for a few conditions of interest. The buildup of minimum drag is shown along with drag polar information. Note that wing-sweep geometry is shown for the Fighter aircraft.

Cm	Pitching moment coefficient
e	Oswald efficiency factor
CLALPHA	CL $\alpha$ or $\partial$ CL $/\partial\alpha$
Cdl^.5Alpha	$(CD_{induced})^{\alpha/2}$

#### **Maneuver Performance Description**

Maneuver performance is shown for several flight conditions of interest. For each condition, sustained level flight, sustained turn, and instantaneous turn performance are shown. Combat weight is 60% of fuel on board and missiles/bombs away. Note that angle of attack was limited to 15° which can limit the instantaneous maneuver. In this case the instantaneous specific excess power (PS) is positive.

#### CONDITIONS PS NZ TDOT RADIUS ALPHA CL CD

where:	PS	Specific Excess Power (ft/sec)
	NZ	Load factor (g)
	TDOT	Turn rate (deg/sec)
	RADIUS	Turn radius (ft)

#### **Mission Performance Description**

Conditions for the end of each mission phase are shown in the following format:

PHASE M H  $C_L$  ALPHA WFUEL TIME VEL SFC(I) THRUST(I)  $C_D$  GAMMA W WA Q SFC(U) THRUST(U) CDINST L/D THR/THA PR X

•	C(O) IIICO	1(0) CDINGT LID TIMOTHATIKA
	H	Altitude at the end of the phase (ft)
	(I)	Installed
	(U)	Uninstalled
	CDINST*	Drag Coefficient for Engine Installation
	GAMMA	Flight path angle (deg)
	THR/THA	Thrust required/Thrust available where 1.00 is maximum dry thrust
	PR*	Pressure Recovery
	X	Distance in nm
	Q	Dynamic pressure associated with Mach number and altitude (lb/ft²)
	VEL	Velocity (ft/sec)
	WA*	Engine Airflow (lb/sec)
	W	Aircraft weight at the end of the phase (lb)
	TIME	Time to complete the segment (sec)
	WFUEL	Fuel used in the segment (lb)
	ALPHA	Angle of attack at the end of the segment (deg)
*Zero in this study because engine tables were used		

<sup>\*</sup>Zero in this study because engine tables were used.

#### **Geometry Description**

Aero surface locations listed are referenced as follows: Fuselage station measured from the nose, butt line is measured from the plane of symmetry, and water line measured from the center of the cylindrical fuselage.

The wing plan area listed is the theoretical area to the aircraft centerline. The wing surface area and volume listed are for the exposed part of the wing based on the fuselage maximum diameter and wing vertical location.

The aircraft density reported with the geometry data may differ from the baseline of 31 lb/ft<sup>3</sup>. This occurs for two reasons. First, designs with internal ducts or external weapons carriage have a lower density. Second, in some cases, the wing or fuselage was sized by other constraints, in which case the density is less than required for that particular aircraft.

#### Aircraft Data (pages 59-185)

#### 1990 Fighter Summary

#### Standard English Units

GENERAL	FUSELAGE		WING	HTAIL	VTAIL
TOGW 57619.	LENGTH 50.4	AREA	834.5	312.9	87.2
W/S 69.0	DIAMETER 5.0	WETTED AREA	1556.6	458.2	174.5
T/W DRY 0.51	VOLUME 760.5	SPAN	75.3	29.7	10.1
T/W A/B 0.74	WETTED AREA 669.3	L.E. SWEEP	20.0	51.0	57.1
CREW 2	FINENESS RATIO 10.0	C/4 SWEEP	15.8	44.6	48.0
N(Z) ULT 9.8		ASPECT RATIO	6.79	2.81	1.17
		TAPER RATIO	0.29	0.18	0.32
ENGINE	WEIGHTS	T/C ROOT	0.12	0.05	0.05
		T/C TIP	0.09	0.04	0.04
NUMBER 1	W %	ROOT CHORD	17.1	17.9	13.0
LENGTH 15.2	STRUCT. 19269. 33.4	TIP CHORD	5.0	3.2	4.2
DIAM. 3.4	PROPUL. 5232. 9.1	M.A. CHORD	12.2	12.3	9.4
WEIGHT 3255.0	FIX. EQ. 7511. 13.0	LOC. OF L.E.	18.2	32.5	37.4
TSLS 29489.	FUEL 17024. 29.5				
SFCSLS 0.85	PAYLOAD 8583. 14.9				

#### MISSION SUMMARY

PHASE	MACH	ALT	FUEL	TIME	DIST	L/D	THRUST	SFC	Q
======	====	=====	=====	=====	=====	=====		=====	=====
TAKEOFF	0.00	0.	656.	10.5					
CLIMB	0.89	50000.	1992.	12.4	102.2	14.72	4709.4	0.992	135.3
CRUISE	0.85	50000.	2605.	49.2	400.0	16.05	3301.6	0.928	123.2
LOITER	0.55	35674.	2650.	60.0	316.6	16.25	3140.3	0.832	103.0
CLIMB	0.89	50000.	753.	2.5	18.1	14.68	8066.2	1.847	135.7
ACCEL	1.50	50000.	1157.	3.4	40.2	5.29	14021.6	1.949	383.7
CRUISE	1.50	50000.	1467.	7.0	100.0	5.20	9001.6	1.393	383.7
COMBAT	1.60	35000.	1664.	3.0	46.1	4.48	20584.0	1.617	894.8
CRUISE	0.80	50000.	2119.	52.3	400.0	16.27	2648.1	0.903	109.1
LOITER	0.30	100.	1006.	20.0	66.1	14.60	2915.8	1.035	132.8

BLOCK TIME = 3.499 HR BLOCK RANGE = 1490.5 NM

#### COMBAT PHASES

MACH ALT PS1G NZS CLS CDS ALS NZI PSI CLI CDI ALI CBE 1.60 35000. 332. 3.9 0.124 0.0276 1.1 6.5 -794. 0.393 0.0703 7.2 59689. 0.20 100. 207. 1.9 1.400 0.1274 15.0 1.9 181. 1.400 0.1274 15.0 1244. 0.90 30000. 248. 3.6 0.340 0.0259 3.1 6.5 -1091. 1.092 0.2747 12.6 1489.

## 1990 Fighter Geometry

T.E. SWEEP	EG.)  EG.)  EG.)  EG.)
C/4 TIP AT 33.133 51.571 51.864 0.000 (FT	.) .)

AIRCRAFT WEIGHT = 57620.148 Lbs. AIRCRAFT VOLUME = 1694.631 Cu.Ft. AIRCRAFT DENSITY = 34.002 Lbs./Cu.Ft.

1990 Fighter Mission Performance

PHASE	M	H	CL	ALPHA	WFUEL	TIME	VEL
	SFC(I)	THRUST(I)	CD	GAMMA	W	WA	Q
	SFC(U)	THRUST(U)	CDINST	L/D	THR/THA	PR	X
CLIMB	0.89	50000.	0.4914	4.47	1991.8	12.37	862.
	0.99	4709.	0.0334	0.98	54972.4	0.00	135.
	0.00	0.	0.0000	14.72	1.00	0.00	102.
CRUISE	0.85	50000.	0.5155	4.45	2605.4	49.23	823.
	0.93	3302.	0.0321	0.00	52367.0	0.00	123.
	0.00	4705.	0.0000	16.05	0.73	0.00	400.
LOITER	0.55	35674.	0.5935	5.52	2650.0	60.00	534.
	0.83	3140.	0.0365	0.00	49717.0	0.00	103.
	0.00	4229.	0.0000	16.25	0.43	0.00	317.
CLIMB	0.89	50000.	0.4315	3.92	753.2	2.47	863.
	1.85	8066.	0.0294	5.55	48963.8	0.00	136.
	0.00	0.	0.0000	14.68	1.71	0.00	18.
ACCEL	1.50	50000.	0.1497	1.20	1156.9	3.37	1452.
	1.95	14022.	0.0283	0.00	47806.9	0.00	384.
	0.00	19762.	0.0000	5.29	1.80	0.00	40.
CRUISE	1.50	50000.	0.1462	1.12	1467.2	6.97	1452.
	1.39	9002.	0.0281	0.00	46339.6	0.00	384.
	0.00	14742.	0.0000	5.20	1.16	0.00	100.
COMBAT	1.60	35000.	0.1236	1.06	1664.4	3.00	1557.
	1.62	20584.	0.0276	0.51	44675.2	0.00	895.
	0.00	42706.	0.0000	4.48	1.33	0.00	46.
CRUISE	0.80	50000.	0.4730	3.81	2119.3	52.30	774.
	0.90	2648.	0.0291	0.00	42555.9	0.00	109.
	0.00	3771.	0.0000	16.27	0.61	0.00	400.
LOITER	0.30	100.	0.3839	3.83	1006.4	20.00	335.
	1.04	2916.	0.0263	0.00	41549.6	0.00	133.
	0.00	4186.	0.0000	14.60	0.11	0.00	66.

#### FUEL SUMMARIES

MISSION FUEL = 16071.
RESERVE FUEL = 804.
TRAPPED FUEL = 150.

TOTAL FUEL = 17024.

## 1990 Fighter Maneuver Performance

	CONDITIONS	PS	NZ	TDOT	RADIUS	ALPHA	CL	CD
M= 1.60 H=35000.	1 G FLIGHT SUSTAINED MAX. INST. COMBAT ENERC	331.6 0.0 -793.6 GY = 0.5	1.00 3.91 6.50 96891E	0.00 4.47 7.60 +05	0. 19957. 11732.	0.34 1.06 7.21	0.062 0.124 0.393	0.0258 0.0276 0.0703
M= 0.20 H= 100.	1 G FLIGHT SUSTAINED MAX. INST. COMBAT ENERG	207.3 0.0 181.1 GY = 0.1	1.00 1.92 1.92 24387E	0.00 13.52 13.52 +04	0. 946. 946.	8.79 15.00 15.00	0.843 1.400 1.400	0.0570 0.1274 0.1274
M= 0.90 H=30000.		248.2 0.0 -1090.6 GY = 0.1	1.00 3.58 6.50 48926E	0.00 7.07 13.22 :+04	0. 7253. 3880.	1.54 3.11 12.59	0.171 0.340 1.092	0.0211 0.0259 0.2747

## 1990 Fighter Aerodynamics

Mach =	0.80	Altitude	= 400	00.				
Parasite Drag	.0110 .0019	Induced Alpha 0.0	Drag Cl 0.000	Cd 0.0140	L/D	Cm	e	
Body Wing Strakes H. Tail	.0019 .0063 .0000	2.0 3.0 4.0	0.252 0.375 0.497	0.0140 0.0172 0.0211 0.0264	0.0 14.6 17.8 18.8		0.00 0.95 0.94 0.94	
V. Tail Canard Pods	.0013 .0000 .0000	5.0 6.0 8.0	0.618 0.709 0.883	0.0401 0.0737 0.1165	15.4 9.6	025 029	0.69 0.40 0.36	
Engine Cowl Boattail	.0000 .0000 .0000	10.0 12.0 15.0	1.049 1.206 1.369	0.1710 0.2369 0.3933	5.1	072	0.33 0.31 0.23	
Interference Wave	.0025			Q]	- 5			
External Tanks Bombs	.0005			cī	e Fact Alpha 1^.5Al			0.0913 0.0411
Stores Extra Camber	.0000 .0005 .0000	•						
Cdmin	.0140							
For a variable c/4 sweet yawed ast mean aero t/c span	o ect rati	2 io 6 1	0.41 .747 2.23 1179 5.03					

## 1990 Fighter Aerodynamics

Mach = 1.	50 Altitude = 50	0000.					
Body Wing Strakes H. Tail V. Tail Canard Pods Engine Cowl Boattail Interference	0016         0.0         0.0           0045         2.0         0.1           0000         3.0         0.2           0014         4.0         0.2           0011         5.0         0.3           0000         6.0         0.3           0000         8.0         0.4           0000         10.0         0.5           0000         12.0         0.6           0000         15.0         0.7           0002         0.02         0.7	87       0.0247       7.6      051         34       0.0294       7.9      069         81       0.0358       7.8      086         29       0.0439       7.5      104         76       0.0537       7.0      123         73       0.0788       6.0      161         70       0.1117       5.1      202         60       0.1843       3.6      176	e 0.00 0.55 0.47 0.42 0.39 0.37 0.34 0.32 0.24 0.23				
External . Tanks . Bombs . Stores . Extra .	0093 0008 0000 0000 0000 0008 0000	Slope Factors ClAlpha Cdl^.5Alpha					
Cdmin .  For a variable c/4 sweep yawed aspective mean aero continuous to to the span .	60.05 et ratio 3.488						

#### 1990 Fighter Propulsion

#### PHYSICAL ATTRIBUTES

ESF = 1.000 WEIGHT = 3255.000 LENGTH = 15.200 DIAM = 3.390

DIAM =	3.390					
POWER	MACH	ALT (ft)	THRUST (lb)	SFC	FFLOW (lb/hr)	WAF (lb/sec)
100.00 100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.0 0.0 0.0 0.0 0.0 0.0 0.0	42645. 29489. 25803. 22117. 18431. 14745. 11058. 7372. 3686.	1.694 0.847 0.815 0.790 0.756 0.729 0.725 0.717	72240.6 24977.2 21021.2 17475.3 13929.5 10746.2 8016.3 5286.4 2859.5	315. 315. 291. 265. 243. 214. 180. 154. 102.
100.00 100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.600 0.600 0.600 0.600 0.600 0.600 0.600	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	16134. 9594. 8395. 7195. 5996. 4797. 3598. 2398. 1199.	1.840 0.915 0.893 0.864 0.853 0.854 0.856 0.891 1.032	29686.6 8778.5 7497.6 6216.4 5112.3 4095.7 3079.1 2136.1 1237.7	315. 315. 294. 276. 247. 217. 192. 158. 127.
100.00 100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.900 0.900 0.900 0.900 0.900 0.900 0.900	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	20380. 12018. 10516. 9013. 7511. 6009. 4507. 3004. 1502.	1.862 1.030 1.014 0.995 0.998 1.024 1.067 1.173 1.548	37953.1 12372.6 10667.5 8965.1 7493.4 6150.9 4808.5 3525.7 2326.0	315. 315. 296. 279. 253. 225. 202. 174. 143.
100.00 100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	1.500 1.500 1.500 1.500 1.500 1.500 1.500	50000.0 50000.0 50000.0 50000.0 50000.0 50000.0 50000.0	14022. 7771. 6799. 5828. 4857. 3885. 2914. 1943. 971.	1.949 1.147 1.133 1.130 1.127 1.143 1.213 1.352 1.814	27325.4 8909.6 7700.6 6585.9 5471.3 4442.2 3534.8 2627.4 1761.7	309. 309. 290. 268. 249. 225. 197. 175.

## 1990 Fighter Weights

COMPONENT	POUNDS	KILOGRAMS	PERCENT
AIRFRAME STRUCTURE WING FUSELAGE HORIZONTAL TAIL VERTICAL TAIL REACTION CONTROL SYSTEM WING FOLD INTERNAL BAY STRUCTURE ALIGHTING GEAR	3982. 1156. 746. 0. 0.	8741. 4818. 1806. 524. 338. 0. 0. 0. 1254.	33.44 18.44 6.91 2.01 1.29 0.00 0.00 0.00 4.80
PROPULSION ENGINES (1) FUEL SYSTEM	5232. 3776. 1456.	2373. 1713. 660.	9.08 6.55 2.53
FIXED EQUIPMENT  (COMPONENTS BELOW DO NOT HYD. + PNEU. ELECTRICAL AVIONICS INSTRUMENTATION DE-ICE/AIR CONDITION AUXILIARY GEAR FURNISH. + EQPT. FLIGHT CONTROLS	7511. INCLUDE TECH 837. 784. 3006. 169. 995. 200. 534. 1820.	FACTOR=0.9) 380. 356.	1.45 1.36
FUEL	17024.	7722.	29.55
PAYLOAD  FLIGHT CREW ( 2)  ARMAMENT  AMMUNITION  LONG RANGE MISSILES  LRM PYLONS & LAUNCHERS  SHORT RANGE MISSILES  SRM LAUNCHERS  EXTERNAL TANKS	8583. 360. 612. 287. 3948. 1880. 796. 700.	3893. 163. 278. 130. 1791. 853. 361. 318. 0.	14.90 0.62 1.06 0.50 6.85 3.26 1.38 1.21 0.00
TOTAL WEIGHT	57619.	26136.	100.00

#### 1990 Light Attack Summary

#### Standard English Units

GENERAL	FUSELAGE		WING	HTAIL	VTAIL
TOGW 24777.	LENGTH 38.2	AREA	329.3	76.9	50.2
W/S 75.2	DIAMETER 4.6	WETTED AREA	553.1	98.0	100.7
T/W 0.51	VOLUME 547.8	SPAN	41.3	16.6	7.2
CREW 1	WETTED AREA 505.7	L.E. SWEEP	18.2	35.0	47.8
N(Z) ULT 9.8	FINENESS RATIO 8.3	C/4 SWEEP	12.8	30.0	30.0
	•	ASPECT RATIO	5.17	3.57	1.02
		TAPER RATIO	0.31	0.39	0.30
ENGINE	WEIGHTS	T/C ROOT	0.09	0.09	0.08
		T/C TIP	0.06	0.07	0.06
NUMBER 1	₩ %	ROOT CHORD	12.2	6.7	10.8
LENGTH 10.8	STRUCT. 7356. 29.7	TIP CHORD	3.8	2.6	3.3
DIAM. 3.4	PROPUL. 3248. 13.1	M.A. CHORD	8.7	4.9	7.7
WEIGHT 2077.6	FIX. EQ. 4091. 16.5	LOC. OF L.E.	7.9	27.8	27.4
TSLS 12749.	FUEL 5524. 22.3				
SFCSLS 0.42	PAYLOAD 4559. 18.4				

#### MISSION SUMMARY

PHASE	MACH	ALT	FUEL	TIME	DIST	L/D	THRUST	SFC	Q
======	====	=====	=====	=====	=====	=====	======	=====	=====
TAKEOFF	0.00	0.	130.	10.5					
CLIMB	0.82	36500.	481.	10.2	74.8	12.74	2566.7	0.662	217.1
CRUISE	0.80	36500.	1360.	65.4	500.0	12.75	1814.8	0.680	208.3
CRUISE	0.80	100.	464.	5.7	50.0	3.68	6132.8	0.800	944.6
COMBAT	0.85	100.	197.	2.0	18.7	6.12	7289.8	0.813	1066.4
CRUISE	0.80	100.	463.	5.7	50.0	3.58	6126.9	0.800	944.6
CLIMB	0.81	39500.	453.	10.5	77.0	12.87	2225.6	0.659	186.5
CRUISE	0.80	39500.	1179.	65.4	500.0	12.84	1584.4	0.675	180.4
LOITER	0.30	100.	390.	20.0	66.1	13.53	1481.9	0.789	132.8

BLOCK TIME = 3.082 HR BLOCK RANGE = 1336.9 NM

#### COMBAT PHASES

MACH	$\mathtt{ALT}$	PS1G	NZS	CLS	CDS	ALS	NZI	PSI	CLI	CDI	$\mathtt{ALI}$	CBE
0.85	100.	44.	3.6	0.127	0.0208	0.9	6.5	-106.	0.408	0.0300	2.8	5257.
0.20	100.	104.	1.5	1.372	0.1496	15.0	1.5	86.	1.372	0.1496	15.0	623.

### 1990 Light Attack Geometry

	WING	H.TAIL	V.TAIL	CANARD	UNITS
PLAN AREA	329.3	76.9	50.2	0.0	(SQ.FT.)
SURFACE AREA	553.1	98.0	100.7	0.0	(SQ.FT.)
VOLUME	139.2	22.0	20.1	0.0	(CU.FT.)
SPAN	41.268	16.580	7.156	0.000	(FT.)
L.E. SWEEP	18.160	35.042	40.035	0.000	(DEG.)
C/4 SWEEP	12.768	30.000	30.000	0.000	(DEG.)
T.E. SWEEP	-4.438	11.612	-11.916	0.000	(DEG.)
ASPECT RATIO	5.171	3.574	1.020	0.000	
ROOT CHORD	12.165	6.694	10.777	0.000	(FT.)
ROOT THICKNESS	13.138	7.230	10.216	0.000	(IN.)
ROOT T/C	0.090	0.090	0.079	0.000	
TIP CHORD	3.795	2.584	3.255	0.000	(FT.)
TIP THICKNESS	2.733	2.170	2.539	0.000	(IN.)
TIP T/C	0.060	0.070	0.065	0.000	
TAPER RATIO	0.312	0.386	0.302	0.000	
MEAN AERO CHORD	8.712	4.942	7.688	0.000	(FT.)
LE ROOT AT	7.880	27.788	27.409	0.000	(FT.)
C/4 ROOT AT	10.921	29.461	30.104	0.000	(FT.)
TE ROOT AT	20.045	34.482	38.186	0.000	(FT.)
LE M.A.C. AT	10.673	30.266	29.878	0.000	(FT.)
C/4 M.A.C. AT	12.850	31.501	31.800	0.000	(FT.)
TE M.A.C. AT	19.384	35.208	37.566	0.000	(FT.)
Y M.A.C. AT	8.514	3.533	2.939	0.000	
LE TIP AT	14.648	33.602	33.421	0.000	(FT.)
C/4 TIP AT	15.597	34.248	34.235	0.000	(FT.)
TE TIP AT	18.444	36.185	36.676	0.000	(FT.)
ELEVATION	0.000	0.000	2.289	0.000	(FT.)
VOLUME COEFF		0.500	0.070	0.000	

AIRCRAFT WEIGHT = 24775.445 Lbs. AIRCRAFT VOLUME = 729.090 Cu.Ft. AIRCRAFT DENSITY = 33.981 Lbs./Cu.Ft.

1990 Light Attack Mission Performance

PHASE	M	H	CL	ALPHA	WFUEL	TIME	VEL
	SFC(I)	THRUST(I)	CD	GAMMA	W	WA	Q
	SFC(U)	THRUST(U)	CDINST	L/D	THR/THA	PR	X
CLIMB	0.82	36500.	0.3354	2.40	480.8	10.18	791.
	0.66	2567.	0.0263	1.62	24164.2	0.00	217.
	0.00	0.	0.0000	12.74	1.00	0.00	75.
CRUISE	0.80	36500.	0.3374	2.47	1359.8	65.38	774.
	0.68	1815.	0.0265	0.00	22804.5	0.00	208.
	0.00	4423.	0.0000	12.74	0.71	0.00	500.
CRUISE	0.80	100.	0.0726	0.52	463.7	5.67	893.
	0.80	6133.	0.0197	0.00	22340.8	0.00	945.
	0.00	16987.	0.0000	3.68	0.73	0.00	50.
COMBAT	0.85	100.	0.1269	0.85	197.5	2.00	949.
	0.81	7290.	0.0208	0.15	22143.3	0.00	1066.
	0.00	21242.	0.0000	6.12	0.73	0.00	19.
CRUISE	0.80	100.	0.0704	0.51	463.4	5.67	893.
	0.80	6127.	0.0197	0.00	21679.9	0.00	945.
	0.00	16978.	0.0000	3.58	0.73	0.00	50.
CLIMB	0.81	39500.	0.3427	2.47	453.0	10.52	787.
	0.66	2226.	0.0266	1.59	21226.9	0.00	186.
	0.00	0.	0.0000	12.78	1.00	0.00	77.
CRUISE	0.80	39500.	0.3424	2.51	1179.4	65.38	774.
	0.68	1584.	0.0267	0.00	20047.6	0.00	180.
	0.00	3822.	0.0000	12.84	0.72	0.00	500.
LOITER	0.30	100.	0.4583	4.54	389.8	20.00	335.
	0.79	1482.	0.0339	0.00	19657.8	0.00	133.
	0.00	3276.	0.0000	13.53	0.14	0.00	66.

### FUEL SUMMARIES

MISSION FUEL = 5118.
RESERVE FUEL = 256.
TRAPPED FUEL = 150.

TOTAL FUEL = 5524.

# 1990 Light Attack Maneuver Performance

	CONDITIONS	PS	NZ	TDOT	RADIUS	ALPHA	CL	CD
M= 0.85 H= 100.	1 G FLIGHT SUSTAINED MAX. INST. COMBAT ENERG	43.8 0.0 -105.7		0.00 6.70 12.48	0. 8117. 4355.	0.42 0.85 2.80	0.064 0.127 0.408	0.0200 0.0208 0.0300
M= 0.20 H= 100.	1 G FLIGHT SUSTAINED MAX. INST.	103.8 0.0 86.2	1.00 1.50 1.50 22524E	0.00 9.24 9.24	0. 1384. 1384.	10.71 15.00 15.00	1.011 1.372 1.372	0.0891 0.1496 0.1496

# 1990 Light Attack Propulsion

Mach =	0.90	Altitude :	100.				
Parasite Dra Friction Body Wing Strakes H. Tail V. Tail Canard Pods Engine Cowl Boattail Interference	.0112 .0037 .0055 .0000 .0011 .0010 .0000 .0000 .0000 .0000	Induced Drag Alpha C.  0.0 0.000 2.0 0.329 3.0 0.483 4.0 0.582 5.0 0.676 6.0 0.768 8.0 0.93 10.0 1.03 12.0 1.130 15.0 1.253	0.0314 0.0378 0.0501 0.0701 0.0874 0.1080 0.1841 0.2381 0.2986	L/D 0.0 8.6 9.6 8.3 7.7 7.1 5.1 4.4 3.8 3.1	093 124	e 0.00 1.01 0.77 0.54 0.50 0.47 0.35 0.32 0.29	
Wave External	.0138			e Fact	ors		
Tanks Bombs Stores Extra Camber	.0000 .0000 .0000 .0051		C) Cá	Alpha N.5Al	.pha		0.0835 0.0405
Cdmin	.0314						
Mach =	0 60	33-4	35000.				
riacii –	0.60	Altitude =	. 55000.				
Parasite Dra Friction Body Wing Strakes H. Tail V. Tail Canard Pods Engine Cowl Boattail Interference	9 .0118 .0039 .0057 .0000 .0011 .0010 .0000 .0000 .0000 .0000 .0000 .0000 .0021	Induced Drag Alpha C1 0.0 0.000 2.0 0.232 3.0 0.349 4.0 0.459 5.0 0.569 6.0 0.652 8.0 0.819 10.0 0.976 12.0 1.124	Cd 0.0173 0.0208 0.0249 0.0306 0.0416 0.0732 0.1140 0.1658 0.2282			e 0.00 0.97 0.97 0.96 0.81 0.47 0.43 0.40 0.37	
Parasite Dra Friction Body Wing Strakes H. Tail V. Tail Canard Pods Engine Cowl Boattail	9 .0118 .0039 .0057 .0000 .0011 .0010 .0000 .0000 .0000 .0000 .0000 .0000 .0000	Induced Drag Alpha C1 0.0 0.000 2.0 0.232 3.0 0.345 4.0 0.455 5.0 0.569 6.0 0.652 8.0 0.810 10.0 0.976 12.0 1.124	Cd 0.0173 0.0208 0.0249 0.0306 0.0416 0.0732 0.1140 0.1658 0.2282 0.3398	0.0 11.2 13.8 14.9 13.6 8.9 7.2 5.9 4.9	0.000 011 017 024 032 040 060 082 106 148	0.00 0.97 0.97 0.96 0.81 0.47 0.43 0.40	0.0883 0.0379

# 1990 Light Attack Propulsion

### PHYSICAL ATTRIBUTES

ESF = 0.719 WEIGHT = 2077.642 LENGTH = 10.770 DIAM = 3.426

POWER	MACH	ALT (ft)	THRUST (1b)	SFC	FFLOW (lb/hr)	WAF (lb/sec)
100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.000 0.000 0.000 0.000 0.000 0.000	0.0 0.0 0.0 0.0 0.0 0.0	12749. 11156. 9562. 7968. 6375. 4781. 3187. 1594.	0.418 0.405 0.399 0.391 0.379 0.378 0.414 0.523	5329.2 4520.8 3819.3 3117.7 2416.2 1808.1 1320.6 833.2	326. 303. 276. 253. 233. 195. 148. 117.
100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.600 0.600 0.600 0.600 0.600 0.600 0.600	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	3154. 2760. 2366. 1971. 1577. 1183. 789. 394.	0.592 0.598 0.607 0.618 0.638 0.691 0.799 1.122	1867.3 1651.2 1435.1 1219.0 1005.4 817.8 630.2 442.6	328. 311. 296. 281. 266. 240. 218. 198.
100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.800 0.800 0.800 0.800 0.800 0.800 0.800	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	3466. 3033. 2600. 2166. 1733. 1300. 867. 433.	0.664 0.671 0.681 0.695 0.719 0.784 0.912 1.299	2301.7 2036.2 1770.8 1505.3 1246.4 1018.5 790.6 562.7	328. 312. 297. 283. 268. 247. 229.
100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.900 0.900 0.900 0.900 0.900 0.900 0.900	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	3591. 3142. 2693. 2244. 1795. 1347. 898. 449.	0.725 0.736 0.751 0.771 0.804 0.887 1.054 1.553	2604.5 2313.1 2021.7 1730.3 1443.6 1194.8 946.0 697.2	328. 313. 298. 285. 272. 252. 235. 220.

# 1990 Light Attack Weights

COMPONENT	POUNDS	KILOGRAMS	PERCENT
	7356. 2519. 2349. 587. 212. 589. 150. 951.		
	3248. 2433. 814.	1104.	13.11 9.82 3.29
(COMPONENTS BELOW DO NOT HYD. + PNEU. ELECTRICAL	208. 544.	CH FACTOR=0.85) 94. 247. 749. 43.	0.84 2.20
FUEL	5524.	2505.	22.29
PAYLOAD  FLIGHT CREW ( 1)  ARMAMENT  AMMUNITION  LASER GUIDED BOMBS  LGB PYLONS AND EJECTORS  SHORT RANGE MISSILES  SRM LAUNCHER  EXTERNAL TANKS	4559. 180. 612. 287. 2182. 700. 398. 200.	82. 278. 130. 990. 318. 181.	18.40 0.73 2.47 1.16 8.81 2.83 1.61 0.81
TOTAL WEIGHT	24777.	11239.	100.00

# 1990 Medium Attack Summary

# Standard English Units

GENERAL	FUSELAGE		WING	HTAIL	VTAIL
TOGW 33438. W/S 72.8 T/W Dry 0.52 CREW 1 N(Z) ULT 9.8	LENGTH 45.2 DIAMETER 4.5 VOLUME 670.5 WETTED AREA 610.9 FINENESS RATIO 10.0	AREA WETTED AREA SPAN L.E. SWEEP C/4 SWEEP ASPECT RATIO TAPER RATIO	459.6 794.4 48.1 23.5 18.2 5.02 0.31	114.3 160.7 20.2 35.0 30.0 3.57 0.39	72.5 145.3 8.6 47.8 30.0 1.02 0.30
ENGINE	WEIGHTS	T/C ROOT T/C TIP	0.09	0.09 0.07	0.08
NUMBER 1 LENGTH 12.6 DIAM. 4.0 WEIGHT 2896.4 TSLS 17495. SFCSLS 0.42	W % STRUCT. 10218. 30.6 PROPUL. 4527. 13.5 FIX. EQ. 4256. 12.7 FUEL 7596. 22.7 PAYLOAD 6841. 20.5	ROOT CHORD TIP CHORD M.A. CHORD LOC. OF L.E.	14.6 4.5 10.4 9.3	8.2 3.2 6.0 32.6	12.9 3.9 9.2 32.2

#### MISSION SUMMARY

PHASE	MACH	ALT	FUEL	TIME	DIST	L/D	THRUST	SFC	Q
======	====	=====	=====	=====	=====	=====	======	=====	=====
TAKEOFF	0.00	0.	179.	10.5					
CLIMB	0.79	36500.	659.	10.3	74.4	12.84	3476.9	0.650	201.6
CRUISE	0.80	36500.	1891.	65.4	500.0	12.33	2528.2	0.679	208.3
CRUISE	0.80	100.	649.	5.7	50.0	3.52	8635.0	0.795	944.6
COMBAT	0.85	100.	276.	2.0	18.7	5.85	10251.7	0.809	1066.4
CRUISE	0.80	100.	648.	5.7	50.0	3.41	8626.8	0.795	944.6
CLIMB	0.78	39500.	617.	10.6	76.5	12.97	3016.9	0.642	171.7
CRUISE	0.80	39500.	1637.	65.4	500.0	12.39	2201.8	0.674	180.4
LOITER	0.30	100.	536.	20.0	66.1	13.19	2038.3	0.788	132.8

BLOCK TIME = 3.086 HR BLOCK RANGE = 1335.9 NM

#### COMBAT PHASES

MACH	ALT	PS1G	NZS	CLS	CDS	ALS	NZI	PSI	CLI	CDI	ALI	CBE
0.85	100.	37.	3.3	0.122	0.0209	0.9	6.5	-118.	0.393	0.0301	3.0	4393.
0.20	100.	107.	1.5	1.314	0.1429	15.0	1.5	89.	1.314	0.1429	15.0	639.

#### 1990 Medium Attack Geometry

```
H.TAIL V.TAIL CANARD UNITS
                     WING
                     459.6
                                   72.5
PLAN AREA.....
                            114.3
                                            0.0 (SO.FT.)
                    794.4
                            160.7
SURFACE AREA.....
                                   145.3
                                             0.0 (SO.FT.)
                    238.1
                             39.9
                                            0.0 (CU.FT.)
VOLUME....
                                    34.8
20.215
                                   8.599
                                           0.000 (FT.)
L.E. SWEEP.....
                   23.450
                           35.042
                                  40.035
                                           0.000 (DEG.)
C/4 SWEEP.....
                           30.000
                   18.233
                                  30.000
                                          0.000 (DEG.)
T.E. SWEEP.....
                   0.936
                           11.612 -11.916
                                          0.000 (DEG.)
ASPECT RATIO .....
                   5.025
                           3.574
                                   1.020
                                          0.000
ROOT CHORD.....
                   14.579
                           8.162
                                  12.949
                                           0.000 (FT.)
ROOT THICKNESS.....
                   15.745
                            8.815
                                  12.276
                                           0.000 (IN.)
ROOT T/C .....
                    0.090
                            0.090
                                   0.079
                                           0.000
                   4.549
TIP CHORD.....
                                           0.000 (FT.)
                            3.150
                                   3.911
                   3.275
TIP THICKNESS.....
                           2.646
                                   3.050
                                           0.000 (IN.)
                  0.060
TIP T/C .....
                           0.070
                                   0.065
                                           0.000
TAPER RATIO .....
                   0.312
                           0.386
                                   0.302
                                           0.000
MEAN AERO CHORD....
                   10.440
                           6.026
                                   9.238
                                           0.000 (FT.)
LE ROOT AT....
                   9.280
                           32.646
                                  32.242
                                          0.000 (FT.)
C/4 ROOT AT.....
                   12.925
                           34.686
                                  35.479
                                          0.000 (FT.)
TE ROOT AT....
                   23.859
                          40.807
                                  45.191
                                          0.000 (FT.)
LE M.A.C. AT.....
                   13.580
                           35.667
                                  35.208
                                          0.000 (FT.)
C/4 M.A.C. AT.....
                   16.190
                           37.173
                                  37.518
                                          0.000 (FT.)
TE M.A.C. AT.....
                   24.021
                           41.693
                                  44.446
                                          0.000 (FT.)
Y M.A.C. AT.....
                   9.914
                           4.307
                                   3.531
                                          0.000
LE TIP AT.....
                   19.703
                           39.734
                                  39.466
                                          0.000 (FT.)
C/4 TIP AT....
                   20.840
                           40.522
                                  40.443
                                           0.000 (FT.)
TE TIP AT.....
                   24.251
                           42.885
                                  43.376
                                           0.000 (FT.)
ELEVATION....
                    0.000
                            0.000
                                   2.250
                                           0.000 (FT.)
VOLUME COEFF. ....
                            0.500
                                   0.070
                                           0.000
```

AIRCRAFT WEIGHT = 33438.113 Lbs. AIRCRAFT VOLUME = 983.340 Cu.Ft. AIRCRAFT DENSITY = 34.005 Lbs./Cu.Ft.

1990 Medium Attack Mission Performance

PHASE	M	H	CL	ALPHA	WFUEL	TIME	VEL
	SFC(I)	THRUST(I)	CD	GAMMA	W	WA	Q
	SFC(U)	THRUST(U)	CDINST	L/D	THR/THA	PR	X
CLIMB	0.79	36500.	0.3567	2.91	658.6	10.33	762.
	0.65	3477.	0.0278	1.59	32600.5	0.00	202.
	00.0	0.	0.0000	12.84	1.00	0.00	74.
CRUISE	0.80	36500.	0.3257	2.62	1891.0	65.38	774.
	0.68	2528.	0.0264	0.00	30709.5	0.00	208.
	0.00	6122.	0.0000	3.52	0.75	0.00	500.
CRUISE	0.80	100.	0.0700	0.55	649.0	5.67	893.
	0.79	8635.	0.0199	0.00	30060.6	0.00	945.
	0.00	23633.	0.0000	12.33	0.72	0.00	50.
COMBAT	0.85	100.	0.1223	0.91	276.5	2.00	949.
	0.81	10252.	0.0209	0.12	29784.1	0.00	1066.
	0.00	29148.	0.0000	3.52	0.93	0.00	19.
CRUISE	0.80	100.	0.0679	0.53	648.5	5.67	893.
	0.80	8627.	0.0199	0.00	29135.6	0.00	945.
	0.00	23621.	0.0000	3.41	0.75	0.00	50.
CLIMB	0.78	39500.	0.3663	3.01	616.7	10.62	756.
	0.64	3017.	0.0282	1.58	28518.9	0.00	172.
	0.00	0.	0.0000	12.97	1.00	0.00	76.
CRUISE	0.80	39500.	0.3291	2.64	1636.5	65.38	774.
	0.67	2202.	0.0266	0.00	26882.3	0.00	180.
	0.00	5283.	0.0000	12.39	0.72	0.00	500.
LOITER	0.30 0.79 0.00	100. 2038. 4502.	0.4403 0.0334 0.0000	4.64 0.00 13.19		20.00 0.00 0.00	335. 133. 66.

### FUEL SUMMARIES

MISSION FUEL = 7091.

RESERVE FUEL = 355.

TRAPPED FUEL = 150.

TOTAL FUEL = 7596.

# 1990 Medium Attack Maneuver Performance

	CONDITIONS	PS	NZ	TDOT	RADIUS	ALPHA	CL	CD
M= 0.85 H= 100.	1 G FLIGHT SUSTAINED MAX. INST. COMBAT ENERG	0.0 -117.6		0.00 6.12 12.48 +04	0. 8878. 4355.	0.45 0.91 2.98	0.061 0.122 0.393	0.0202 0.0209 0.0301
M= 0.20 H= 100.	1 G FLIGHT SUSTAINED MAX. INST. COMBAT ENERG	106.6 0.0 89.2	1.00 1.50 1.50 39383E	0.00 9.23 9.23	0. 1386. 1386.	10.83 15.00 15.00	0.971 1.314 1.314	0.0862 0.1429 0.1429

# 1990 Medium Attack Aerodynamics

Mach =	0.90	Altitud	de =	100.				
Parasite Drag Friction Body Wing Strakes H. Tail V. Tail Canard Pods Engine Cowl Boattail Interference Wave External Tanks	.0107 .0031 .0054 .0000 .0012 .0010 .0000 .0000 .0000 .0000 .0000 .011 .0106 .0100	2.0 0 3.0 0 4.0 0 5.0 0 6.0 0 8.0 0 10.0 1 12.0 1	C1 .000 .289 .431 .527 .617 .705 .875			027 038 049 060 086 090 120 170	e 0.00 1.00 0.79 0.52 0.49 0.46 0.42 0.32 0.30 0.26	0.0816
Bombs	.0050				Aipha 1^.5Al	pha		0.0401
Stores Extra	.0000 .0050							
Camber	.0000							
Cdmin	.0324							
Mach =	0.60	Altitu	.de =	35000.				
Parasite Drag Friction Body Wing Strakes H. Tail V. Tail Canard Pods Engine Cowl Boattail Interference	.0112 .0032 .0057 .0000 .0013 .0010 .0000 .0000 .0000 .0000	Induced Dr. Alpha  0.0 0 2.0 0 3.0 0 4.0 0 5.0 0 6.0 0 8.0 0 10.0 0 12.0 1		35000.  Cd 0.0199 0.0229 0.0266 0.0318 0.0394 0.0714 0.1098 0.1589 0.2184 0.3256	L/D 0.0 9.4 12.0 13.4 13.4 8.6 7.0 5.8 4.9 3.9	059 081	e 0.00 0.96 0.96 0.99 0.46 0.42 0.39 0.36 0.33	
Parasite Drag Friction Body Wing Strakes H. Tail V. Tail Canard Pods Engine Cowl Boattail	.0112 .0032 .0057 .0000 .0013 .0010 .0000 .0000 .0000	Induced Dr. Alpha  0.0 0 2.0 0 3.0 0 4.0 0 5.0 0 6.0 0 8.0 0 10.0 0 12.0 1	C1 .000 .216 .321 .424 .526 .613 .773 .926	Cd 0.0199 0.0229 0.0266 0.0318 0.0394 0.0714 0.1098 0.1589 0.2184 0.3256	0.0 9.4 12.0 13.4 13.4 8.6 7.0 5.8 4.9	0.000 011 017 024 032 040 059 081 106 148	0.00 0.96 0.96 0.96 0.90 0.46 0.42 0.39 0.36	0.0844 0.0369

# 1990 Medium Attack Propulsion

### PHYSICAL ATTRIBUTES

ESF = 0.987 WEIGHT = 2896.399 LENGTH = 12.616 DIAM = 4.013

POWER	MACH	ALT (ft)	THRUST (1b)	SFC	FFLOW (lb/hr)	WAF (lb/sec)
100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.0 0.0 0.0 0.0 0.0 0.0	17495. 15308. 13121. 10934. 8747. 6560. 4374. 2187.	0.418 0.405 0.399 0.391 0.379 0.378 0.414 0.523	7312.7 6203.5 5240.8 4278.1 3315.4 2481.1 1812.2 1143.2	447. 415. 379. 348. 320. 268. 204. 160.
100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.600 0.600 0.600 0.600 0.600 0.600 0.600	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	4328. 3787. 3246. 2705. 2164. 1623. 1082. 541.	0.592 0.598 0.607 0.618 0.638 0.691 0.799 1.122	2562.3 2265.8 1969.2 1672.7 1379.6 1122.1 864.7 607.3	450. 427. 406. 386. 366. 330. 299. 272.
100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.800 0.800 0.800 0.800 0.800 0.800 0.800	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	4756. 4162. 3567. 2973. 2378. 1784. 1189. 595.	0.664 0.671 0.681 0.695 0.719 0.784 0.912 1.299	3158.3 2794.1 2429.8 2065.6 1710.4 1397.6 1084.8 772.1	450. 428. 407. 388. 368. 339. 314. 291.
100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.900 0.900 0.900 0.900 0.900 0.900 0.900	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	4927. 4311. 3695. 3080. 2464. 1848. 1232. 616.	0.725 0.736 0.751 0.771 0.804 0.887 1.054 1.553	3573.8 3174.0 2774.2 2374.4 1980.9 1639.5 1298.1 956.7	450. 429. 409. 391. 373. 346. 323. 301.

# 1990 Medium Attack Weights

COMPONENT	POUNDS	KILOGRAMS	PERCENT
AIRFRAME STRUCTURE WING FUSELAGE HORIZONTAL TAIL VERTICAL TAIL ARMOR WING FOLD ALIGHTING GEAR	3776. 3094. 997. 329. 589. 150.	1713. 1403. 452	11.29 9.25 2.98 0.99 1.76 0.45
PROPULSION ENGINES (1) FUEL SYSTEM	4527. 3392. 1135.	2054. 1539. 515.	13.54 10.14 3.40
(COMPONENTS BELOW DO NOT HYD. + PNEU. ELECTRICAL	1NCLUDE TEX 281. 544. 1652. 94.	127. 247. 749	0.84 1.63
FUEL		3446.	22.72
	612. 287. 398. 200. 4364. 800.	91.	0.54 1.83 0.86 1.19
TOTAL WEIGHT	33438.	15168.	100.00

# 1990 Medium All Weather Attack Summary

# Standard English Units

GENERAL	FUSELAGE		WING	HTAIL	VTAIL
TOGW 37573. W/S 72.9	LENGTH 48.2 DIAMETER 4.5	AREA WETTED AREA	515.6 899.1	121.7 172.4	78.7 157.9
T/W Dry 0.51	VOLUME 740.0	SPAN	51.5	20.9	9.0
CREW 2 N(Z) ULT 9.8	WETTED AREA 663.1 FINENESS RATIO 10.6	L.E. SWEEP C/4 SWEEP	20.1 14.8	35.0 30.0	47.8 30.0
		ASPECT RATIO TAPER RATIO	5.14 0.31	3.57 0.39	1.02 0.30
ENGINE	WEIGHTS	T/C ROOT	0.09	0.09	0.08
NUMBER 1	W %	T/C TIP ROOT CHORD	0.06 15.3	0.07 8.4	0.06 13.5
LENGTH 13.2	STRUCT. 11423. 30.4	TIP CHORD	4.8	3.2	4.1
DIAM. 4.2 WEIGHT 3188.5	PROPUL. 4984. 13.3 FIX. EQ. 5930. 15.8	M.A. CHORD LOC. OF L.E.	10.9 10.0	6.2 35.1	9.6 34.7
TSLS 19171. SFCSLS 0.42	FUEL 8215. 21.9 PAYLOAD 7021. 18.7				

### MISSION SUMMARY

PHASE	MACH	ALT	FUEL	TIME	DIST	L/D	THRUST	SFC	Q
======	====	=====	=====	=====	======	=====	======	=====	=====
TAKEOFF	0.00	0.	196.	10.5					
CLIMB	0.80	36500.	725.	10.2	74.6	13.27	3830.9	0.655	208.1
CRUISE	0.80	36500.	2036.	65.4	500.0	12.93	2715.7	0.680	208.3
CRUISE	0.80	100.	696.	5.7	50.0	3.73	9191.8	0.800	944.6
COMBAT	0.85	100.	298.	2.0	18.7	6.14	11025.2	0.812	1066.4
CRUISE	0.80	100.	695.	5.7	50.0	3.62	9182.9	0.801	944.6
CLIMB	0.80	39500.	684.	10.6	77.4	13.41	3326.0	0.649	178.4
CRUISE	0.80	39500.	1767.	65.4	500.0	13.03	2372.7	0.676	180.4
LOITER	0.30	100.	584.	20.0	66.1	13.77	2213.8	0.792	132.8

BLOCK TIME = 3.084 HR BLOCK RANGE = 1337.0 NM

#### COMBAT PHASES

MACH	$\mathtt{ALT}$	PS1G	NZS	CLS	CDS	ALS	NZI	PSI	CLI	CDI	$\mathtt{ALI}$	CBE
0.85	100.	42.	3.5	0.123	0.0200	0.9	6.5	-106.	0.395	0.0289	2.9	4982.
0.20	100.	103.	1.5	1.333	0.1422	15.0	1.5	86.	1.333	0.1422	15.0	617.

# 1990 Medium All Weather Attack Geometry

	WING	H.TAIL	V.TAIL	CANARD	UNITS
PLAN AREA	515.6	121.7	78.7	0.0	(SQ.FT.)
SURFACE AREA	899.1	172.4	157.9	0.0	(SQ.FT.)
VOLUME	281.7	43.8	39.4	0.0	(CU.FT.)
SPAN	51.472	20.853	8.961	0.000	(FT.)
L.E. SWEEP	20.085	35.042	40.035	0.000	(DEG.)
C/4 SWEEP	14.767	30.000	30.000	0.000	(DEG.)
T.E. SWEEP	-2.438	11.612	-11.916	0.000	(DEG.)
ASPECT RATIO	5.138	3.574	1.020	0.000	
ROOT CHORD	15.271	8.419	13.496	0.000	(FT.)
ROOT THICKNESS	16.492	9.093	12.794	0.000	(IN.)
ROOT T/C	0.090	0.090	0.079	0.000	
TIP CHORD	4.764	3.250	4.076	0.000	(FT.)
TIP THICKNESS	3.430	2.730	3.179	0.000	(IN.)
TIP T/C	0.060	0.070	0.065	0.000	
TAPER RATIO	0.312	0.386	0.302	0.000	
MEAN AERO CHORD	10.936	6.216	9.627	0.000	(FT.)
LE ROOT AT	9.959	35.078	34.674	0.000	(FT.)
C/4 ROOT AT	13.777	37.183	38.0 <b>4</b> 8	0.000	(FT.)
TE ROOT AT	25.230	43.498	48.170	0.000	(FT.)
LE M.A.C. AT	13.842	38.194	37.766	0.000	(FT.)
C/4 M.A.C. AT	16.576	39.748	40.173	0.000	(FT.)
TE M.A.C. AT	24.778	44.411	47.393	0.000	(FT.)
Y M.A.C. AT	10.619	4.443	3.680	0.000	
LE TIP AT	19.369	42.390	42.203	0.000	(FT.)
C/4 TIP AT	20.561	43.203	43.222	0.000	(FT.)
TE TIP AT	24.134	45.640	46.279	0.000	(FT.)
ELEVATION	0.000	0.000	2.275	0.000	(FT.)
VOLUME COEFF		0.500	0.070	0.000	

AIRCRAFT WEIGHT = 37573.547 Lbs. AIRCRAFT VOLUME = 1104.919 Cu.Ft. AIRCRAFT DENSITY = 34.006 Lbs./Cu.Ft.

1990 Medium All Weather Attack Mission Performance

PHASE	M	H	CL	ALPHA	WFUEL	TIME	VEL
	SFC(I)	THRUST(I)	CD	GAMMA	W	WA	Q
	SFC(U)	THRUST(U)	CDINST	L/D	THR/THA	PR	X
CLIMB	0.80	36500.	0.3463	2.70	725.4	10.24	774.
	0.66	3831.	0.0261	1.61	36652.0	0.00	208.
	0.00	0.	0.0000	13.27	1.00	0.00	75.
CRUISE	0.80	36500.	0.3270	2.55	2035.8	65.38	774.
	0.68	2716.	0.0253	0.00	34616.2	0.00	208.
	0.00	6632.	0.0000	12.93	0.71	0.00	500.
CRUISE	0.80	100.	0.0704	0.54	695.5	5.67	893.
	0.80	9192.	0.0189	0.00	33920.7	0.00	945.
	0.00	25499.	0.0000	3.73	0.73	0.00	50.
COMBAT	0.85	100.	0.1231	0.88	298.4	2.00	949.
	0.81	11025.	0.0200	0.14	33622.3	0.00	1066.
	0.00	31942.	0.0000	6.14	0.91	0.00	19.
CRUISE	0.80	100.	0.0683	0.52	695.0	5.67	893.
	0.80	9183.	0.0189	0.00	32927.3	0.00	945.
	0.00	25486.	0.0000	3.62	0.73	0.00	50.
CLIMB	0.80	39500.	0.3553	2.79	684.0	10.59	770.
	0.65	3326.	0.0265	1.58	32243.3	0.00	178.
	0.00	0.	0.0000	13.41	1.00	0.00	77.
CRUISE	0.80	39500.	0.3324	2.59	1766.8	65.38	774.
	0.68	2373.	0.0255	0.00	30476.4	0.00	180.
	0.00	5734.	0.0000	13.03	0.71	0.00	500.
LOITER	0.30	100.	0.4449	4.62	584.1	20.00	335.
	0.79	2214.	0.0323	0.00	29892.3	0.00	133.
	0.00	4908.	0.0000	13.77	0.14	0.00	66.

### FUEL SUMMARIES

MISSION FUEL = 7681.
RESERVE FUEL = 384.
TRAPPED FUEL = 150.

TOTAL FUEL = 8215.

# 1990 Medium All Weather Attack Maneuver Performance

	CONDITIONS	PS	NZ	TDOT	RADIUS	ALPHA	CL	CD
M= 0.85 H= 100.	1 G FLIGHT SUSTAINED MAX. INST. COMBAT ENERG	0.0			0. 8262. 4355.	0.44 0.88 2.89	0.062 0.123 0.395	0.0193 0.0200 0.0289
M= 0.20 H= 100.	1 G FLIGHT SUSTAINED MAX. INST. COMBAT ENERG	102.8 0.0 85.6	1.00 1.50 1.50 16518E	0.00 9.23 9.23	0. 1386. 1386.	10.79 15.00 15.00	0.982 1.333 1.333	0.0849 0.1422 0.1422

# 1990 Medium All Weather Attack Aerodynamics

Mach	=	0.90	Altitude =	100.					
Parasite Friction Body Wing Strakes H. Tail V. Tail Canard Pods Engine Cowl Boattail Interfere		.0105 .0029 .0054 .0000 .0011 .0010 .0000 .0000 .0000 .0000 .0000	Induced Drag Alpha C. 0.0 0.000 2.0 0.300 3.0 0.450 4.0 0.540 5.0 0.630 6.0 0.720 8.0 0.900 10.0 1.010 12.0 1.100 15.0 1.22	0.0272 0.0328 0.0436 0.0627 0.0790 0.0985 0.1468 0.2299 0.2893	L/D 0.0 9.2 10.3 8.7 8.1 7.4 6.2 4.4 3.8 3.2		e 0.00 1.00 0.77 0.52 0.49 0.46 0.42 0.31 0.29 0.26		
External Tanks		.0044		Cl	e Fact Alpha				0.0818
Bombs Stores Extra Camber		.0000 .0000 .0044 .0000		Cd	ll^.5Al	pha		(	0.0401
Cdmin		.0272							
Mach	=	0.60	Altitude =	35000.					
Parasite Friction Body Wing Strakes H. Tail V. Tail Canard Pods Engine Cowl Boattail Interfere	Drag	.0110 .0031 .0057 .0000 .0012 .0010 .0000 .0000 .0000 .0000	Altitude =  Induced Drag Alpha C1 0.0 0.000 2.0 0.220 3.0 0.327 4.0 0.432 5.0 0.537 6.0 0.623 8.0 0.787 10.0 0.942 12.0 1.088 15.0 1.288	Cd 0.0158 0.0189 0.0227 0.0279 0.0374 0.0684 0.1075 0.1577	L/D 0.0 11.6 14.4 15.5 14.4 9.1 7.3 6.0 5.0 3.9	Cm 0.000 012 019 026 034 063 063 112 155	e 0.00 0.96 0.96 0.83 0.46 0.42 0.39 0.36 0.33		
Parasite Friction Body Wing Strakes H. Tail V. Tail Canard Pods Engine Cowl Boattail	Drag	.0110 .0031 .0057 .0000 .0012 .0010 .0000 .0000	Induced Drag Alpha C1 0.0 0.000 2.0 0.220 3.0 0.323 4.0 0.432 5.0 0.533 6.0 0.623 8.0 0.783 10.0 0.942 12.0 1.088	Cd 0.0158 0.0189 0.0227 0.0279 0.0374 0.0684 0.1075 0.1577 0.2184 0.3276	0.0 11.6 14.4 15.5 14.4 9.1 7.3 6.0 5.0	0.000 012 019 026 034 063 063 112 155	0.00 0.96 0.96 0.96 0.83 0.46 0.42 0.39		).0859 ).0372

# 1990 Medium All Weather Attack Propulsion

### PHYSICAL ATTRIBUTES

ESF = 1.081 WEIGHT = 3188.523 LENGTH = 13.207 DIAM = 4.201

POWER	MACH	ALT (ft)	THRUST (1b)	SFC	FFLOW (lb/hr)	WAF (lb/sec)
100.00 87.50 75.00 62.50 50.00 37.50 25.00	0.000 0.000 0.000 0.000 0.000 0.000	0.0 0.0 0.0 0.0 0.0 0.0	19171. 16775. 14378. 11982. 9586. 7189. 4793. 2396.	0.418 0.405 0.399 0.391 0.379 0.378 0.414 0.523	8013.5 6797.9 5743.0 4688.1 3633.2 2718.9 1985.8 1252.8	490. 455. 416. 381. 351. 294. 223. 175.
100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.600 0.600 0.600 0.600 0.600 0.600	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	4743. 4150. 3557. 2964. 2371. 1779. 1186. 593.	0.592 0.598 0.607 0.618 0.638 0.691 0.799 1.122	2807.9 2482.9 2158.0 1833.0 1511.8 1229.7 947.6 665.5	493. 468. 445. 423. 401. 361. 327. 298.
100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.800 0.800 0.800 0.800 0.800 0.800 0.800	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	5212. 4561. 3909. 3258. 2606. 1955. 1303. 652.	0.664 0.671 0.681 0.695 0.719 0.784 0.912 1.299	3461.0 3061.8 2662.7 2263.5 1874.3 1531.5 1188.8 846.1	493. 469. 446. 425. 403. 372. 344. 319.
100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.900 0.900 0.900 0.900 0.900 0.900 0.900	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	5400. 4725. 4050. 3375. 2700. 2025. 1350. 675.	0.725 0.736 0.751 0.771 0.804 0.887 1.054 1.553	3916.3 3478.2 3040.0 2601.9 2170.7 1796.6 1422.5 1048.3	493. 470. 449. 429. 409. 380. 354. 330.

# 1990 Medium All Weather Attack Weights

COMPONENT	POUNDS	KILOGRAMS	PERCENT
	11423. 4325. 3475. 1079. 364. 589. 150. 1442.	5182. 1962. 1576. 489. 165. 267. 68. 654.	30.40 11.51 9.25 2.87 0.97 1.57 0.40 3.84
PROPULSION ENGINES (1) FUEL SYSTEM	4984. 3734. 1250.	1694.	13.26 9.94 3.33
FIXED EQUIPMENT  (COMPONENTS BELOW DO NOT HYD. + PNEU. ELECTRICAL AVIONICS INSTRUMENTATION DE-ICE/AIR CONDITION AUXILIARY GEAR FURNISH. + EQPT. FLIGHT CONTROLS	5930. INCLUDE TE 315. 817. 2790. 219. 398. 200. 613. 1236.	CH FACTOR = 0.90 143. 370. 1266.	
FUEL	8215.	3727.	21.86
PAYLOAD  FLIGHT CREW ( 2)  ARMAMENT  AMMUNITION  SHORT RANGE MISSILES  SRM LAUNCHERS  LASER GUIDED BOMBS  LGB PYLONS AND EJECTORS  EXTERNAL TANKS	7021. 360. 612. 287. 398. 200. 4364. 800.	3185. 163. 278. 130. 181. 91. 1980. 363. 0.	18.69 0.96 1.63 0.76 1.06 0.53 11.61 2.13 0.00
TOTAL WEIGHT	37573.	17043.	100.00

# 1990 Medium Flying Wing Attack Summary

# Standard English Units

GENERAL	FUSELAGE		WING	HTAIL	VTAIL
TOGW 26392. W/S 31.8 T/W Dry 0.33	LENGTH 16.0 DIAMETER 4.5 VOLUME 188.9	AREA WETTED AREA SPAN	829.1 1402.1 53.9	0.0 0.0 0.2	0.0 0.0 0.1
CREW 2	WETTED AREA 192.5	L.E. SWEEP	47.7	35.0	47.8
N(Z) ULT 9.8	FINENESS RATIO 3.6	C/4 SWEEP ASPECT RATIO	39.1 3.50	30.0 3.57	30.0 1.02
		TAPER RATIO	0.00	0.39	0.30
ENGINE	WEIGHTS	T/C ROOT T/C TIP	0.15 0.00	0.09 0.07	0.08 0.06
NUMBER 1	W %	ROOT CHORD	30.8	0.1	0.1
LENGTH 8.9	STRUCT. 7733. 29.3	TIP CHORD	0.0	0.0	0.0
DIAM. 2.8 WEIGHT 1383.1	PROPUL. 2162. 8.2 FIX. EQ. 5630. 21.3	M.A. CHORD LOC. OF L.E.	20.5 -2.4	$\begin{smallmatrix}0.1\\14.4\end{smallmatrix}$	0.1 15.9
TSLS 8653. SFCSLS 0.42	FUEL 4446. 16.8 PAYLOAD 6421. 24.3				

#### MISSION SUMMARY

PHASE	MACH	ALT	FUEL	TIME	DIST	L/D	THRUST	SFC	Q
======	====	=====	=====	=====	=====	=====	======	=====	=====
TAKEOFF	0.00	0.	89.	10.5					
CLIMB	0.76	30463.	409.	10.8	74.8	17.85	2255.0	0.649	247.2
CRUISE	0.80	30463.	1131.	63.7	500.0	16.38	1528.9	0.692	276.2
CRUISE	0.80	100.	331.	5.7	50.0	5.54	4441.3	0.788	944.6
COMBAT	0.85	100.	140.	2.0	18.7	9.35	5222.3	0.805	1066.4
CRUISE	0.80	100.	331.	5.7	50.0	5.44	4438.7	0.788	944.6
CLIMB	0.78	39253.	533.	18.8	134.5	20.24	1510.5	0.643	174.2
CRUISE	0.80	39253.	854.	65.4	500.0	19.66	1158.9	0.671	182.5
LOITER	0.30	100.	274.	20.0	66.1	20.93	1078.4	0.763	132.8

BLOCK TIME = 3.204 HR BLOCK RANGE = 1394.3 NM

### COMBAT PHASES

MACH	ALT	PS1G	NZS	CLS	CDS	ALS	NZI	PSI	CLI	CDI	$\mathtt{ALI}$	CBE
0.85	100.	17.	2.8	0.055	0.0059	0.7	6.5	-81.	0.178	0.0085	2.3	2018.
0.20	100.	62.	2.0	0.882	0.0777	15.0	2.0	33.	0.882	0.0777	15.0	369.

# 1990 Medium Flying Wing Geometry

	WING	H.TAIL	V.TAIL	CANARD	UNITS
PLAN AREA	829.1	0.0	0.0	0.0	(SQ.FT.)
SURFACE AREA	1402.1	0.0	0.0	0.0	(SQ.FT.)
VOLUME	1130.7	0.0	0.0	0.0	(CU.FT.)
SPAN	53.868	0.172	0.092	0.000	(FT.)
L.E. SWEEP	47.667	35.042	40.035	0.000	(DEG.)
C/4 SWEEP	39.096	30.000	30.000	0.000	(DEG.)
T.E. SWEEP	-2.454	11.612	-11.916	0.000	(DEG.)
ASPECT RATIO	3.500	3.574	1.020	0.000	
ROOT CHORD	30.751	0.070	0.138	0.000	(FT.)
ROOT THICKNESS	55.352	0.075	0.131	0.000	(IN.)
ROOT T/C	0.150	0.090	0.079	0.000	
TIP CHORD	0.031	0.027	0.042	0.000	(FT.)
TIP THICKNESS	0.000	0.023	0.033	0.000	(IN.)
TIP T/C	0.001	0.070	0.065	0.000	
TAPER RATIO	0.001	0.386	0.302	0.000	
MEAN AERO CHORD	20.501	0.051	0.099	0.000	(FT.)
LE ROOT AT	-2.408	14.378	15.862	0.000	(FT.)
C/4 ROOT AT	5.280	14.396	15.896	0.000	(FT.)
TE ROOT AT	28.343	14.448	16.000	0.000	(FT.)
LE M.A.C. AT	7.457	14.404	15.893	0.000	(FT.)
C/4 M.A.C. AT	12.583	14.417	15.918	0.000	(FT.)
TE M.A.C. AT	27.958	14.456	15.992	0.000	(FT.)
Y M.A.C. AT	8.987	0.037	0.038	0.000	
LE TIP AT	27.158	14.439	15.939	0.000	(FT.)
C/4 TIP AT	27.166	14.446	15.949	0.000	(FT.)
TE TIP AT	27.189	14.466	15.981	0.000	(FT.)
ELEVATION	-0.450	0.000	2.250	0.000	(FT.)
VOLUME COEFF		0.000	0.000	0.000	

AIRCRAFT WEIGHT = 26392.357 Lbs. AIRCRAFT VOLUME = 1319.592 Cu.Ft. AIRCRAFT DENSITY = 20.000 Lbs./Cu.Ft.

1990 Medium Flying Wing Mission Performance

PHASE	M	H	CL	ALPHA	WFUEL	TIME	VEL
	SFC(I)	THRUST(I)	CD	GAMMA	W	WA	Q
	SFC(U)	THRUST(U)	CDINST	L/D	THR/THA	PR	X
CLIMB	0.76	30463.	0.1264	1.73	409.0	10.80	751.
	0.65	2255.	0.0071	1.78	25894.8	0.00	247.
	0.00	0.	0.0000	17.85	1.00	0.00	75.
CRUISE	0.80	30463.	0.1094	1.46	1130.7	63.75	794.
	0.69	1529.	0.0067	0.00	24764.0	0.00	276.
	0.00	3816.	0.0000	16.38	0.66	0.00	500.
CRUISE	0.80	100.	0.0314	0.42	330.8	5.67	893.
	0.79	4441.	0.0057	0.00	24433.3	0.00	945.
	0.00	11940.	0.0000	5.54	0.78	0.00	50.
COMBAT	0.85	100.	0.0552	0.71	140.1	2.00	949.
	0.80	5222.	0.0059	0.09	24293.1	0.00	1066.
	0.00	14418.	0.0000	9.35	0.95	0.00	19.
CRUISE	0.80	100.	0.0308	0.41	330.6	5.67	893.
	0.79	4439.	0.0057	0.00	23962.5	0.00	945.
	0.00	11936.	0.0000	5.44	0.78	0.00	50.
CLIMB	0.78	39253.	0.1618	2.20	532.8	18.85	757.
	0.64	1510.	0.0080	0.87	23429.7	0.00	174.
	0.00	0.	0.0000	20.24	1.00	0.00	134.
CRUISE LEWIS	0.80 0.67 0.00	39253. 1159. 2728.	0.1506 0.0077 0.0000	2.02 0.00 19.66	854.0 22575.7 0.76	65.38 0.00 0.00	774. 183. 500.
LOITER	0.30	100.	0.2050	3.21	274.4	20.00	335.
	0.76	1078.	0.0098	0.00	22301.3	0.00	133.
	0.00	2319.	0.0000	20.93	0.15	0.00	66.

#### FUEL SUMMARIES

MISSION FUEL = 4091. RESERVE FUEL = 205. TRAPPED FUEL = 150.

TOTAL FUEL = 4446.

# 1990 Medium Flying Wing Maneuver Peformance

	CONDITIONS	PS	NZ	TDOT	RADIUS	ALPHA	CL	CD
M= 0.85 H= 100.	1 G FLIGHT SUSTAINED MAX. INST. COMBAT ENERGY	0.0	6.50		0. 10540. 4355.	0.36 0.71 2.33	0.028 0.055 0.178	0.0057 0.0059 0.0085
M= 0.20 H= 100.	1 G FLIGHT SUSTAINED MAX. INST. COMBAT ENERGY	0.0	1.00 2.02 2.02 69247E	0.00 14.51 14.51 +03	0. 881. 881.	7.45 15.00 15.00	0.456 0.882 0.882	0.0251 0.0777 0.0777

# 1990 Medium Flying Wing Aerodynamics

Mach =	0.90	Altitude =	100.				
Parasite Drag Friction Body Wing Strakes H. Tail V. Tail Canard Pods Engine Cowl Boattail Interference Wave External	.0055 .0008 .0047 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000	Induced Drag Alpha Cl 0.0 0.000 2.0 0.158 3.0 0.235 4.0 0.311 5.0 0.385 6.0 0.459 8.0 0.570 10.0 0.671 12.0 0.753 15.0 0.819	0.2076 0.2752	L/D 0.0 11.2 14.0 15.1 15.2 14.3 7.0 5.7 3.6 3.0	Cm 0.000 0.003 0.004 0.005 0.007 0.008 0.010 0.012 0.033 0.035	e 0.00 1.00 1.00 1.00 0.94 0.42 0.39 0.26 0.23	
Tanks Bombs	.0000		Cl	Alpha ll^.5Al			0.0546 0.0342
Stores Extra Camber	.0000 .0000 .0000						
Cdmin	.0118	,					
Mach =	0.60	Altitude =	35000.				
Parasite Drag Friction Body Wing Strakes H. Tail V. Tail Canard Pods Engine Cowl Boattail Interference	.0057 .0009 .0049 .0000 .0000 .0000 .0000 .0000 .0000 .0000	Altitude =  Induced Drag Alpha Cl 0.0 0.000 2.0 0.137 3.0 0.205 4.0 0.271 5.0 0.336 6.0 0.400 8.0 0.525 10.0 0.648 12.0 0.743 15.0 0.858	Cd 0.0058 0.0075 0.0096 0.0125 0.0161 0.0204 0.0311 0.0443 0.1411	L/D 0.0 18.4 21.3 21.7 20.9 19.6 16.9 14.6 5.3 4.1	Cm 0.000 0.007 0.010 0.013 0.016 0.019 0.026 0.032 0.036 0.042	e 0.00 0.99 0.99 0.99 0.99 0.99 0.37 0.33	
Parasite Drag Friction Body Wing Strakes H. Tail V. Tail Canard Pods Engine Cowl	.0057 .0009 .0049 .0000 .0000 .0000 .0000 .0000 .0000	Induced Drag Alpha Cl 0.0 0.000 2.0 0.137 3.0 0.205 4.0 0.271 5.0 0.336 6.0 0.400 8.0 0.525 10.0 0.648 12.0 0.743	Cd 0.0058 0.0075 0.0096 0.0125 0.0161 0.0204 0.0311 0.0443 0.1411 0.2088	0.0 18.4 21.3 21.7 20.9 19.6 16.9 14.6 5.3	0.000 0.007 0.010 0.013 0.016 0.019 0.026 0.032 0.036 0.042	0.00 0.99 0.99 0.99 0.99 0.99 0.99	0.0572 0.0300

# 1990 Medium Flying Wing Propulsion

### PHYSICAL ATTRIBUTES

ESF = 0.488 WEIGHT = 1383.110 LENGTH = 8.873 DIAM = 2.823

POWER	MACH	ALT (ft)	THRUST (1b)	SFC	FFLOW (lb/hr)	WAF (lb/sec)
100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.0 0.0 0.0 0.0 0.0 0.0 0.0	8653. 7572. 6490. 5408. 4327. 3245. 2163. 1082.	0.418 0.405 0.399 0.391 0.379 0.378 0.414 0.523	3617.1 3068.4 2592.3 2116.1 1639.9 1227.2 896.4 565.5	221. 205. 188. 172. 158. 132. 101. 79.
100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.600 0.600 0.600 0.600 0.600 0.600	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	2141. 1873. 1606. 1338. 1070. 803. 535. 268.	0.592 0.598 0.607 0.618 0.638 0.691 0.799 1.122	1267.4 1120.7 974.1 827.4 682.4 555.1 427.7 300.4	223. 211. 201. 191. 181. 163. 148.
100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.800 0.800 0.800 0.800 0.800 0.800 0.800	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	2353. 2059. 1764. 1470. 1176. 882. 588. 294.	0.664 0.671 0.681 0.695 0.719 0.784 0.912 1.299	1562.2 1382.0 1201.9 1021.7 846.0 691.3 536.6 381.9	223. 212. 201. 192. 182. 168. 155. 144.
100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.500 0.500 0.500 0.500 0.500 0.500 0.500	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	2127. 1861. 1595. 1329. 1063. 798. 532. 266.	0.553 0.558 0.564 0.572 0.587 0.635 0.730 1.016	1176.5 1038.0 899.5 761.0 624.2 506.2 388.1 270.1	223. 210. 199. 189. 178. 158. 140. 126.

# 1990 Medium Flying Wing Weights

COMPONENT	POUNDS	KILOGRAMS	PERCENT
AIRFRAME STRUCTURE WING FUSELAGE HORIZONTAL TAIL VERTICAL TAIL ARMOR WING FOLD INTERNAL BAY STRUCTURE ALIGHTING GEAR	150.	3508. 1719. 450. 0. 0. 267. 68. 544. 459.	29.30 14.36 3.76 0.00 0.00 2.23 0.57 4.55 3.84
PROPULSION ENGINES (1) FUEL SYSTEM	2162. 1620. 542.	981. 735. 246.	8.19 6.14 2.05
(COMPONENTS BELOW DO NOT HYD. + PNEU. ELECTRICAL AVIONICS INSTRUMENTATION DE-ICE/AIR CONDITION AUXILIARY GEAR	221. 817. 2790. 219. 398. 200. 613.	H FACTOR = 0.90) 100. 370. 1266.	0.84 3.09
FUEL	4446.	2017.	16.84
PAYLOAD  FLIGHT CREW ( 2)  ARMAMENT  AMMUNITION  SHORT RANGE MISSILES  SRM LAUNCHERS  LASER GUIDED BOMBS  LGB PYLONS AND EJECTORS  EXTERNAL TANKS	200. 4364.	163. 278. 130.	24.33 1.36 2.32 1.09 1.51 0.76 16.54 0.76
TOTAL WEIGHT	26392.	11972.	100.00

# 1990 Medium Internal Attack Summary

# Standard English Units

GENERAL	FUSELAGE		WING	HTAIL	VTAIL
TOGW 34486. W/S 68.4 T/W Dry 0.45 CREW 2 N(Z) ULT 9.8	LENGTH 49.8 DIAMETER 4.6 VOLUME 767.5 WETTED AREA 685.9 FINENESS RATIO 10.8	AREA WETTED AREA SPAN L.E. SWEEP C/4 SWEEP ASPECT RATIO TAPER RATIO	504.0 874.1 50.5 18.9 13.4 5.05 0.31	111.5 154.2 20.0 35.0 30.0 3.57 0.39	69.7 139.8 8.4 47.8 30.0 1.02
ENGINE	WEIGHTS	T/C ROOT T/C TIP	0.09	0.09	0.08
NUMBER 1	W %	ROOT CHORD	15.2	8.1	12.7
LENGTH 11.9 DIAM. 3.8	STRUCT. 11960. 34.7 PROPUL. 3983. 11.6	TIP CHORD M.A. CHORD	4.8 10.9	3.1 6.0	3.8 9.1
WEIGHT 2548.2 TSLS 15486. SFCSLS 0.42	FIX. EQ. 5911. 17.1 FUEL 6211. 18.0 PAYLOAD 6421. 18.6	LOC. OF L.E.	10.4	36.9	37.1

# MISSION SUMMARY

PHASE	MACH	ALT	FUEL	TIME	DIST	L/D	THRUST	SFC	Q
======	====	=====	=====	=====	======	=====	======	=====	=====
TAKEOFF	0.00	0.	158.	10.5					
CLIMB	0.83	36500.	591.	9.5	75.1	16.44	3138.7	0.669	225.5
CRUISE	0.80	36500.	1488.	65.4	500.0	16.68	1955.5	0.691	208.3
CRUISE	0.80	100.	485.	5.7	50.0	5.26	6088.5	0.842	944.6
COMBAT	0.85	100.	206.	2.0	18.7	8.74	7256.0	0.852	1066.4
CRUISE	0.80	100.	484.	5.7	50.0	5.15	6082.7	0.842	944.6
CLIMB	0.84	39500.	580.	10.2	80.6	16.58	2731.5	0.675	200.2
CRUISE	0.80	39500.	1316.	65.4	500.0	16.89	1746.7	0.684	180.4
LOITER	0.30	100.	464.	20.0	66.1	16.83	1733.5	0.804	132.8

BLOCK TIME = 3.065 HR BLOCK RANGE = 1340.8 NM

### COMBAT PHASES

MACH	ALT	PS1G	NZS	CLS	CDS	ALS	NZI	PSI	CLI	CDI	ALI	CBE
0.85	100.	86.	5.0	0.118	0.0135	0.8	6.5	-57.	0.379	0.0217	2.7	10353.
0.20	100.	85.	1.5	1.333	0.1374	15.0	1.5	67.	1.333	0.1374	15.0	509.

# 1990 Medium Internal Attack Geometry

	WING	H.TAIL	V.TAIL	CANARD	UNITS
PLAN AREA	504.0	111.5	69.7	0.0	(SQ.FT.)
SURFACE AREA	874.1	154.2	139.8	0.0	(SQ.FT.)
VOLUME	273.4	38.4	32.8	0.0	(CU.FT.)
SPAN	50.463	19.963	8.433	0.000	(FT.)
L.E. SWEEP	18.858	35.042	40.035	0.000	(DEG.)
C/4 SWEEP	13.375	30.000	30.000	0.000	(DEG.)
T.E. SWEEP	-4.210	11.612	-11.916	0.000	(DEG.)
ASPECT RATIO	5.052	3.574	1.020	0.000	
ROOT CHORD	15.226	8.060	12.700	0.000	(FT.)
ROOT THICKNESS	16.444	8.705	12.040	0.000	(IN.)
ROOT T/C	0.090	0.090	0.079	0.000	
TIP CHORD	4.750	3.111	3, 836	0.000	(FT.)
TIP THICKNESS	3.420	2.613	2.992	0.000	(IN.)
TIP T/C	0.060	0.070	0.065	0.000	
TAPER RATIO	0.312	0.386	0.302	0.000	
MEAN AERO CHORD	10.904	5.951	9.060	0.000	(FT.)
LE ROOT AT	10.428	36.882	37.070	0.000	(FT.)
C/4 ROOT AT	14.234	38.897	40.245	0.000	(FT.)
TE ROOT AT	25.654	44.942	49.770	0.000	(FT.)
LE M.A.C. AT	13.984	39.865	39.979	0.000	(FT.)
C/4 M.A.C. AT	16.710	41.353	42.244	0.000	(FT.)
TE M.A.C. AT	24.887	45.816	49.039	0.000	(FT.)
Y M.A.C. AT	10.411	4.254	3.463	0.000	
LE TIP AT	19.046	43.882	44.155	0.000	(FT.)
C/4 TIP AT	20.234	44.660	45.114	0.000	(FT.)
TE TIP AT	23.796	46.993	47.990	0.000	(FT.)
ELEVATION	0.000	0.000	2.313	0.000	(FT.)
VOLUME COEFF		0.500	0.070	0.000	

AIRCRAFT WEIGHT = 34485.969 Lbs. AIRCRAFT VOLUME = 1112.232 Cu.Ft. AIRCRAFT DENSITY = 31.006 Lbs./Cu.Ft.

1990 Medium Internal Attack Mission Performance

PHASE	M	H	CL	ALPHA	WFUEL	TIME	VEL
	SFC(I)	THRUST(I)	CD	GAMMA	W	WA	Q
	SFC(U)	THRUST(U)	CDINST	L/D	THR/THA	PR	X
CLIMB	0.83	36500.	0.2955	2.17	591.3	9.49	806.
	0.67	3139.	0.0180	1.86	33736.2	0.00	225.
	0.00	0.	0.0000	16.44	1.00	0.00	75.
CRUISE	0.80	36500.	0.3107	2.39	1487.6	65.38	774.
	0.69	1956.	0.0186	0.00	32248.6	0.00	208.
	0.00	5023.	0.0000	16.68	0.63	0.00	500.
CRUISE	0.80	100.	0.0672	0.51	484.7	5.67	893.
	0.84	6088.	0.0128	0.00	31763.9	0.00	945.
	0.00	18630.	0.0000	5.26	0.60	0.00	50.
COMBAT	0.85	100.	0.1180	0.83	206.2	2.00	949.
	0.85	7256.	0.0135	0.42	31557.7	0.00	1066.
	0.00	25801.	0.0000	8.74	0.74	0.00	19.
CRUISE	0.80	100.	0.0658	0.50	484.4	5.67	893.
	0.84	6083.	0.0128	0.00	31073.3	0.00	945.
	0.00	18622.	0.0000	5.15	0.60	0.00	50.
CLIMB	0.84	39500.	0.3009	2.18	579.6	10.19	816.
	0.67	2732.	0.0182	1.69	30493.7	0.00	200.
	0.00	0.	0.0000	16.58	1.00	0.00	81.
CRUISE	0.80	39500.	0.3245	2.50	1316.1	65.38	774.
	0.68	1747.	0.0192	0.00	29177.7	0.00	180.
	0.00	4393.	0.0000	16.89	0.65	0.00	500.
LOITER	0.30	100.	0.4358	4.50	464.4	20.00	335.
	0.80	1734.	0.0259	0.00	28713.2	0.00	133.
	0.00	3893.	0.0000	16.83	0.14	0.00	66.

### FUEL SUMMARIES

MISSION FUEL = 5773. RESERVE FUEL = 289. TRAPPED FUEL = 150.

TOTAL FUEL = 6211.

# 1990 Medium Internal Attack Maneuver Performance

# ADDITIONAL COMBAT PARAMETERS

	CONDITIONS	PS	NZ	TDOT	RADIUS	ALPHA	CL	CD
M= 0.85 H= 100.	1 G FLIGHT SUSTAINED MAX. INST. COMBAT ENERGY	0.0 -56.5		0.00 9.60 12.48 +05	0. 5662. 4355.	0.42 0.83 2.73	0.059 0.118 0.379	0.0128 0.0135 0.0217
M= 0.20 H= 100.	1 G FLIGHT SUSTAINED MAX. INST. COMBAT ENERGY	0.0 67.4	1.00 1.50 1.50 508714E	0.00 9.24 9.24 +03	0. 1384. 1384.	10.57 15.00 15.00	0.965 1.333 1.333	0.0772 0.1374 0.1374

# 1990 Medium Internal Attack Aerodynamics

Mach =	0.90	Altitude =	100.				
Parasite Drag Friction Body Wing Strakes H. Tail V. Tail Canard Pods Engine Cowl Boattail Interference Wave External	.0104 .0031 .0054 .0000 .0010 .0009 .0000 .0000 .0000 .0000 .0011 .0112 .0000	Induced Drag Alpha Cl 0.0 0.000 2.0 0.308 3.0 0.459 4.0 0.555 5.0 0.647 6.0 0.737 8.0 0.911 10.0 1.013 12.0 1.103 15.0 1.223		L/D 0.0 10.8 11.5 9.4 8.5 7.7 6.3 4.5 3.9 3.2	Cm 0.000 019 029 041 053 065 092 099 131 183	e 0.00 1.01 0.76 0.53 0.50 0.47 0.43 0.32 0.29 0.26	
Tanks Bombs	.0000			Alpha 1^.5Al	pha		0.0815 0.0401
Stores Extra	.0000				<b>.</b>		******
Camber	.0000						
Cdmin	.0227						
Mach =	0.60	Altitude =	35000.				
Parasite Drag Friction Body Wing Strakes H. Tail V. Tail Canard Pods Engine Cowl Boattail Interference	.0110 .0032 .0057 .0000 .0011 .0009 .0000 .0000 .0000 .0000	Altitude =  Induced Drag Alpha Cl 0.0 0.000 2.0 0.221 3.0 0.329 4.0 0.435 5.0 0.540 6.0 0.626 8.0 0.789 10.0 0.944 12.0 1.090 15.0 1.288	35000.  Cd 0.0128 0.0160 0.0199 0.0252 0.0355 0.0661 0.1056 0.1561 0.2171 0.3266	L/D 0.0 13.8 16.6 17.3 15.2 9.5 7.5 6.1 5.0 3.9	Cm 0.000 012 019 027 035 044 065 088 114 158	e 0.00 0.97 0.97 0.96 0.81 0.46 0.42 0.39 0.37 0.33	
Parasite Drag Friction Body Wing Strakes H. Tail V. Tail Canard Pods Engine Cowl Boattail	.0110 .0032 .0057 .0000 .0011 .0009 .0000 .0000 .0000	Induced Drag Alpha C1 0.0 0.000 2.0 0.221 3.0 0.329 4.0 0.435 5.0 0.540 6.0 0.626 8.0 0.789 10.0 0.944 12.0 1.090	Cd 0.0128 0.0160 0.0199 0.0252 0.0355 0.0661 0.1056 0.1561 0.2171 0.3266	0.0 13.8 16.6 17.3 15.2 9.5 7.5 6.1 5.0	0.000 012 019 027 035 044 065 088 114 158	0.00 0.97 0.97 0.96 0.81 0.46 0.42 0.39 0.37	0.0859 0.0373

# 1990 Medium Internal Attack Propulsion

# PHYSICAL ATTRIBUTES

ESF = 0.874 WEIGHT = 2548.210 LENGTH = 11.870 DIAM = 3.776

POWER	MACH	ALT (ft)	THRUST (lb)	SFC	FFLOW (lb/hr)	WAF (lb/sec)
100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.000 0.000 0.000 0.000 0.000 0.000	0.0 0.0 0.0 0.0 0.0 0.0	15486. 13550. 11614. 9678. 7743. 5807. 3871. 1936.	0.418 0.405 0.399 0.391 0.379 0.378 0.414 0.523	6473.0 5491.1 4639.0 3786.8 2934.7 2196.2 1604.1 1012.0	396. 368. 336. 308. 283. 237. 180. 142.
100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.600 0.600 0.600 0.600 0.600 0.600	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	3831. 3352. 2873. 2394. 1916. 1437. 958. 479.	0.592 0.598 0.607 0.618 0.638 0.691 0.799 1.122	2268.1 2005.6 1743.1 1480.6 1221.2 993.3 765.4 537.5	398. 378. 359. 342. 324. 292. 264. 241.
100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.800 0.800 0.800 0.800 0.800 0.800 0.800	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	4210. 3684. 3158. 2631. 2105. 1579. 1053. 526.	0.664 0.671 0.681 0.695 0.719 0.784 0.912 1.299	2795.7 2473.2 2150.8 1828.4 1514.0 1237.1 960.3 683.4	398. 379. 360. 343. 325. 300. 278. 258.
100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.900 0.900 0.900 0.900 0.900 0.900 0.900	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	4362. 3816. 3271. 2726. 2181. 1636. 1090. 545.	0.725 0.736 0.751 0.771 0.804 0.887 1.054 1.553	3163.4 2809.5 2455.6 2101.7 1753.4 1451.2 1149.0 846.8	398. 380. 362. 346. 330. 307. 286. 267.

# 1990 Medium Internal Attack Weights

COMPONENT	POUNDS	KILOGRAMS	PERCENT
AIRFRAME STRUCTURE WING FUSELAGE HORIZONTAL TAIL VERTICAL TAIL ARMOR WING FOLD INTERNAL BAY STRUCTURE ALIGHTING GEAR	11960. 3974. 3488. 920. 314. 589. 150. 1200. 1323.		
PROPULSION ENGINES (1) FUEL SYSTEM	3983. 2984. 999.	1807. 1354. 453.	11.55 8.65 2.90
FIXED EQUIPMENT (COMPONENTS BELOW DO NOT HYD. + PNEU. ELECTRICAL AVIONICS INSTRUMENTATION DE-ICE/AIR CONDITION AUXILIARY GEAR FURNISH. + EQPT. FLIGHT CONTROLS	289. 817. 2790. 219.	FACTOR = 0.90) 131. 370. 1266.	17.14 0.84 2.37 8.09 0.63 1.15 0.58 1.78 3.60
FUEL	6211.	2818.	18.01
PAYLOAD  FLIGHT CREW ( 2)  ARMAMENT  AMMUNITION  SHORT RANGE MISSILES  SRM LAUNCHERS  LASER GUIDED BOMBS  LGB PYLONS AND EJECTORS  EXTERNAL TANKS	398. 200. 4364.	2913. 163. 278. 130. 181. 91. 1980. 91. 0.	18.62 1.04 1.77 0.83 1.15 0.58 12.65 0.58 0.00
TOTAL WEIGHT	34486.	15643.	100.00

### 1990 MRF Summary

# Standard English Units

GENERAL	FUSELAGE		WING	HTAIL	VTAIL
TOGW 53072.	LENGTH 58.5	AREA	580.0	221.3	88.0
W/S 91.5 T/W DRY 0.59	DIAMETER 5.9 VOLUME 1179.4	WETTED AREA SPAN	883.0 38.1	306.8 25.8	176.2 10.5
T/W WET 0.90	WETTED AREA 897.8	L.E. SWEEP	45.0	47.4	45.9
CREW 1	FINENESS RATIO 10.0	C/4 SWEEP	36.3	43.0	34.0
N(Z) ULT 11.3		ASPECT RATIO	2.50	3.00	1.25
		TAPER RATIO	0.20	0.36	0.38
ENGINE	WEIGHTS	T/C ROOT	0.05	0.05	0.05
		T/C TIP	0.04	0.04	0.04
NUMBER 1	W %	ROOT CHORD	25.4	12.6	12.1
LENGTH 16.1	STRUCT. 12600. 23.7	TIP CHORD	5.1	4.6	4.6
DIAM. 3.6	PROPUL. 5947. 11.2	M.A. CHORD	17.5	9.2	8.9
WEIGHT 3700.0	FIX. EQ. 5330. 10.0	LOC. OF L.E.	22.9	45.9	43.5
TSLS 31341.	FUEL 24244. 45.7				
SFCSLS 0.80	PAYLOAD 4951. 9.3				

# MISSION SUMMARY

PHASE	MACH	ALT	FUEL	TIME	DIST	L/D	THRUST	SFC	Q
======	====	======	=====	=====	=====	=====	======	=====	=====
TAKEOFF	0.00	0.	649.	10.5					
CRUISE	0.85	100.	6332.	26.7	250.0	4.61	10458.0	1.357	1066.4
CLIMB	0.91	36000.	857.	3.1	27.6	8.50	9669.2	0.963	276.2
LOITER	0.80	37282.	4670.	60.0	459.0	8.29	5166.6	0.875	201.9
CLIMB	0.89	50000.	1215.	3.5	26.4	6.32	9033.2	1.896	135.7
ACCEL	1.50	50000.	1163.	3.0	35.1	3.51	15115.1	2.100	383.7
CRUISE	1.50	50000.	3232.	10.5	150.0	3.36	10705.9	1.699	383.7
COMBAT	1.50	50000.	1057.	2.0	28.7	4.51	15109.2	2.099	383.7
CRUISE	0.91	44000.	2655.	46.0	400.0	8.76	3640.3	0.918	188.2
LOITER	0.30	100.	1113.	20.0	66.1	9.18	3403.5	0.981	132.8

BLOCK TIME = 2.922 HR BLOCK RANGE = 1447.7 NM

### COMBAT PHASES

MACH	ALT	PS1G	NZS	CLS	CDS	ALS	NZI	PSI	CLI	CDI	ALI	CBE
1.50	50000.	-128.	1.0	0.172	0.0491	2.9	5.4	-2125.	0.909	0.2839	15.0	-767.
1.50	50000.	187.	2.0	0.305	0.0676	5.1	5.9	-2019.	0.909	0.2839	15.0	22479.
0.20	100.	287.	1.5	0.933	0.2472	15.0	1.5	266.	0.933	0.2472	15.0	1720.
0.90	30000.	371.	3.0	0.613	0.1060	8.6	4.8	-741.	0.972	0.2800	15.0	7791.

# 1990 MRF Geometry

	WING	H.TAIL	V.TAIL	CANARD	UNITS
PLAN AREA	580.0	221.3	88.0	0.0	(SQ.FT.)
SURFACE AREA	883.0	306.8	176.2	0.0	(SQ.FT.)
VOLUME	263.0	66.3	25.6	0.0	(CU.FT.)
SPAN	38.079	25.768	10.504	0.000	(FT.)
L.E. SWEEP	45.000	47.412	40.486	0.000	(DEG.)
C/4 SWEEP	36.254	43.000	34.000	0.000	(DEG.)
T.E. SWEEP	-3.814	24.997	7.806	0.000	(DEG.)
ASPECT RATIO	2.500	3.000	1.254	0.000	
ROOT CHORD	25.386	12.594	12.140	0.000	(FT.)
ROOT THICKNESS	15.232	7.557	7.284	0.000	(IN.)
ROOT T/C	0.050	0.050	0.050	0.000	
TIP CHORD	5.077	4.584	4.613	0.000	(FT.)
TIP THICKNESS	2.437	2.200	2.214	0.000	(IN.)
TIP T/C	0.040	0.040	0.040	0.000	
TAPER RATIO	0.200	0.364	0.380	0.000	
MEAN AERO CHORD	17.488	9.212	8.940	0.000	(FT.)
LE ROOT AT	22.922	45.942	43.469	0.000	(FT.)
C/4 ROOT AT	29.268	49.090	46.504	0.000	(FT.)
TE ROOT AT	48.307	58.536	55.609	0.000	(FT.)
LE M.A.C. AT	30.326	51.861	47.281	0.000	(FT.)
C/4 M.A.C. AT	34.698	54.164	49.516	0.000	(FT.)
TE M.A.C. AT	47.814	61.073	56.221	0.000	(FT.)
Y M.A.C. AT	7.404	5.441	4.465	0.000	
LE TIP AT	41.961	59.959	52.436	0.000	(FT.)
C/4 TIP AT	43.230	61.105	53.589	0.000	(FT.)
TE TIP AT	47.038	64.543	57.049	0.000	(FT.)
ELEVATION	0.263	-0.293	2.927	0.000	(FT.)
VOLUME COEFF		0.425	0.059	0.000	

AIRCRAFT WEIGHT = 53068.680 Lbs. AIRCRAFT VOLUME = 1559.816 Cu.Ft. AIRCRAFT DENSITY = 34.022 Lbs./Cu.Ft.

1990 MRF Mission Performance

PHASE	M	H	CL	ALPHA	WFUEL	TIME	VEL
	SFC(I)	THRUST(I)	CD	GAMMA	W	WA	Q
	SFC(U)	THRUST(U)	CDINST	L/D	THR/THA	PR	X
CRUISE	0.85	100.	0.0779	0.87	6332.1	26.69	949.
	1.36	10458.	0.0169	0.00	46088.1	0.00	1066.
	0.00	24654.	0.0000	4.61	0.38	0.00	250.
CLIMB	0.91	36000.	0.3334	4.19	857.4	3.12	882.
	0.96	9669.	0.0392	4.29	45230.7	0.00	276.
	0.00	0.	0.0000	8.50	1.00	0.00	28.
LOITER	0.80	37282.	0.3656	4.82	4669.7	60.00	774.
	0.88	5167.	0.0441	0.00	40561.0	0.00	202.
	0.00	7705.	0.0000	8.29	0.63	0.00	459.
CLIMB	0.89	50000.	0.5535	7.67	1215.0	3.54	863.
	1.90	9033.	0.0876	3.10	39345.9	0.00	136.
	0.00	0.	0.0000	6.32	1.85	0.00	26.
ACCEL	1.50	50000.	0.1723	2.93	1163.2	3.00	1452.
	2.10	15115.	0.0491	0.00	38182.8	0.00	384.
	0.00	21784.	0.0000	3.51	2.00	0.00	35.
CRUISE	1.50	50000.	0.1618	2.76	3231.8	10.46	1452.
	1.70	10706.	0.0481	0.00	34950.7	0.00	384.
	0.00	17376.	0.0000	3.36	1.42	0.00	150.
COMBAT	1.50	50000.	0.3052	5.12	1057.3	2.00	1452.
	2.10	15109.	0.0676	0.43	33893.4	0.00	384.
	0.00	21784.	0.0000	4.51	2.00	0.00	29.
CRUISE	0.91	44000.	0.2921	3.57	2655.2	45.98	881.
	0.92	3640.	0.0334	0.00	31238.2	0.00	188.
	0.00	5821.	0.0000	8.76	0.55	0.00	400.
LOIŤER	0.30 0.98 0.00	100. 3403. 4998.	0.4054 0.0442 0.0000	5.69 0.00 9.18		20.00 0.00 0.00	335. 133. 66.

#### FUEL SUMMARIES

MISSION FUEL = 22946. RESERVE FUEL = 1147. TRAPPED FUEL = 150.

TOTAL FUEL = 24244.

### 1990 MRF Maneuver Performance

	CONDITIONS	PS	NZ	TDOT	RADIUS	ALPHA	CL	CD
M= 1.50 H=50000.	1 G FLIGHT SUSTAINED MAX. INST COMBAT ENERG	0.0 2125.5	1.00 5.35	6.67	0. 465095. 12469.	0.00	0.172 0.000 0.909	0.0491 0.0000 0.2839
M= 1.50 H=50000.			1.98 5.90		0. 38308. 11269.		0.157 0.305 0.909	0.0477 0.0676 0.2839
M= 0.20 H= 100.	1 G FLIGHT SUSTAINED MAX. INST. COMBAT ENERG	266.4	1.46 1.46	8.73	0. 1465. 1465.		0.880 0.933 0.933	0.2134 0.2472 0.2472
M= 0.90 H=30000.	1 G FLIGHT SUSTAINED MAX. INST. COMBAT ENERG	371.0 0.0 -741.4 SY = 0.7	3.04 4.77	0.00 5.91 9.61	0. 8682. 5341.	2.30 8.61 15.00	0.210 0.613 0.972	0.0234 0.1060 0.2800

## 1990 MRF Aerodynamics

Mach	=	0.90	Altit	tude =	100.				-	
Parasite Friction Body Wing Strakes H. Tail V. Tail Canard Pods Engine Cowl Boattail Interfere Wave	1	.0110 .0035 .0041 .0000 .0016 .0018 .0000 .0000 .0000 .0000	Induced I Alpha 0.0 2.0 3.0 4.0 5.0 6.0 8.0 10.0 12.0 15.0	C1 0.000 0.184 0.254 0.320 0.385 0.449 0.575 0.695 0.810 0.972	Cd 0.0152 0.0205 0.0274 0.0359 0.0466 0.0597 0.0929 0.1353 0.1865 0.2789	L/D 0.0 9.0 9.3 8.9 8.3 7.5 6.2 5.1 4.3 3.5		e 0.00 0.81 0.67 0.63 0.60 0.58 0.54 0.51 0.49		
External Tanks Bombs Stores Extra Camber		.0026 .0000 .0000 .0000 .0026			Cl	e Fact Alpha 11^.5Al				0.0648 0.0342
Cdmin		.0152								
Mach	=	0.60	Alti	tude =	35000.					
Parasite Friction Body Wing Strakes H. Tail V. Tail Canard Pods Engine Cowl Boattai Interfere Wave External Tanks Bombs Stores Extra Camber	l ence	.0115 .0036 .0043 .0000 .0017 .0019 .0000 .0000 .0000 .0000 .0015 .0000 .0018 .0000 .0000	Induced Alpha 0.0 2.0 3.0 4.0 5.0 6.0 8.0 10.0 12.0 15.0	C1 0.000 0.158 0.234 0.309 0.368 0.429 0.549 0.664 0.775 0.930	cl	L/D 0.0 8.5 10.0 10.0 8.6 7.9 6.5 5.4 4.6 3.6 e Fact Alpha 11^.5Al	095 ors	e 0.00 0.84 0.81 0.75 0.62 0.59 0.55 0.52 0.49		0.0620 0.0327
Cdmin Detailed	Aero	.0149 odynamics	output							

### 1990 MRF Propulsion

#### PHYSICAL ATTRIBUTES

ESF = 1.150 WEIGHT = 3700.016 LENGTH = 16.086 DIAM = 3.635

POWER	MACH	ALT (ft)	THRUST (1b)	SFC	FFLOW (lb/hr)	WAF (lb/sec)
100.00 100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.0 0.0 0.0 0.0 0.0 0.0 0.0	47584. 31341. 27423. 23506. 19588. 15670. 11753. 7835. 3918.	1.747 0.796 0.766 0.743 0.711 0.688 0.684 0.677	83128.5 24946.5 20999.8 17460.9 13921.9 10778.9 8043.2 5307.4 2902.6	362. 362. 335. 307. 282. 248. 211. 182. 121.
100.00 100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.600 0.600 0.600 0.600 0.600 0.600 0.600	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	18002. 10007. 8756. 7505. 6254. 5004. 3753. 2502. 1251.	1.897 0.873 0.854 0.829 0.818 0.821 0.826 0.866 1.016	34150.0 8736.4 7479.8 6223.0 5117.7 4108.3 3098.9 2166.6 1270.7	362. 362. 338. 316. 285. 252. 225. 187. 153.
100.00 100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.800 0.800 0.800 0.800 0.800 0.800 0.800 0.800	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	21018. 11584. 10136. 8688. 7240. 5792. 4344. 2896. 1448.	1.894 0.932 0.921 0.906 0.908 0.932 0.971 1.072 1.419	39809.1 10796.2 9332.9 7869.7 6575.6 5396.8 4218.0 3104.1 2055.3	362. 362. 340. 320. 292. 261. 235. 202. 169.
100.00 100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.900 0.900 0.900 0.900 0.900 0.900 0.900	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	22822. 12438. 10883. 9329. 7774. 6219. 4664. 3110. 1555.	1.913 0.988 0.978 0.964 0.968 0.997 1.045 1.161 1.559	43662.5 12288.4 10639.0 8989.6 7526.7 6200.6 4874.4 3610.5 2423.3	362. 362. 341. 321. 293. 263. 237. 206. 172.

## 1990 MRF Weights

COMPONENT	POUNDS	KILOGRAMS	PERCENT
AIRFRAME STRUCTURE WING FUSELAGE HORIZONTAL TAIL VERTICAL TAIL REACTION CONTROL SYSTEM WING FOLD INTERNAL BAY STRUCTURE ALIGHTING GEAR	12600. 4693. 4137. 946. 715. 0. 150. 0.	5715. 2129. 1877. 429. 324. 0. 68. 0. 888.	23.74 8.84 7.80 1.78 1.35 0.00 0.28 0.00 3.69
PROPULSION ENGINES (1) FUEL SYSTEM	5947. 4292. 1655.	2697. 1947. 751.	11.20 8.09 3.12
FIXED EQUIPMENT (COMPONENTS BELOW DO NOT HYD. + PNEU. ELECTRICAL	771. 544. 1652. 94. 610.	FACTOR=0.85) 350. 247. 749.	10.04 1.45 1.03 3.11 0.18 1.15 0.38 0.71 3.16
FUEL	24244.	10997.	45.68
PAYLOAD  FLIGHT CREW ( 1)  ARMAMENT  AMMUNITION  LONG RANGE MISSILES  LRM PYLONS & LAUNCHERS  SHORT RANGE MISSILES  SRM LAUNCHERS  EXTERNAL TANKS	4951. 180. 612. 287. 1974. 1300. 398. 200. 0.	2246. 82. 278. 130. 895. 590. 181. 91. 0.	9.33 0.34 1.15 0.54 3.72 2.45 0.75 0.38 0.00
TOTAL WEIGHT	53072.	24073.	100.00

#### 1990 NFA Summary

### Standard English Units

GENERAL	FUSELAGE		WING	HTAIL	VTAIL
TOGW 64315.	LENGTH 59.9	AREA	791.1	301.9	120.0
W/S 81.3	DIAMETER 6.0	WETTED AREA	1248.7	439.9	240.3
T/W DRY 0.57	VOLUME 1272.9	SPAN	44.5	30.1	12.3
T/W WET 0.87	WETTED AREA 943.9	L.E. SWEEP	45.0	47.4	45.9
CREW 1	FINENESS RATIO 10.0	C/4 SWEEP	36.3	43.0	34.0
N(Z) ULT 11.3		ASPECT RATIO	2.50	3.00	1.25
		TAPER RATIO	0.20	0.36	0.38
ENGINE	WEIGHTS	T/C ROOT	0.05	0.05	0.05
		T/C TIP	0.04	0.04	0.04
NUMBER 1	W %	ROOT CHORD	29.6	14.7	14.2
LENGTH 17.4	STRUCT. 18006. 28.0	TIP CHORD	5.9	5.4	5.4
DIAM. 3.9	PROPUL. 7037. 10.9	M.A. CHORD	20.4	10.8	10.4
WEIGHT 4378.5	FIX. EQ. 5797. 9.0	LOC. OF L.E.	. 22.5	45.2	42.7
TSLS 36792.	FUEL 28523. 44.3				
SFCSLS 0.80	PAYLOAD 4951. 7.7				

#### MISSION SUMMARY

PHASE	MACH	ALT	FUEL	TIME	DIST	L/D	THRUST	SFC	Q
======	====	=====	======	=====	=====	=====	======	=====	=====
TAKEOFF	0.00	0.	761.	10.5					
CRUISE	0.85	100.	7553.	26.7	250.0	4.65	12583.1	1.346	1066.4
CLIMB	0.95	36000.	1040.	3.2	27.0	7.90	11800.6	0.976	301.8
LOITER	0.80	37192.	5297.	60.0	459.0	8.92	5855.4	0.878	202.7
CLIMB	0.89	50000.	1354.	3.3	24.9	6.89	10604.2	1.896	135.7
ACCEL	1.50	50000.	1450.	3.2	37.2	3.58	17743.8	2.100	383.7
CRUISE	1.50	50000.	3956.	10.5	150.0	3.43	12879.5	1.732	383.7
COMBAT	1.50	50000.	1240.	2.0	28.7	4.71	17723.4	2.099	383.7
CRUISE	0.91	44000.	3075.	46.0	400.0	9.30	4228.1	0.918	188.2
LOITER	0.30	100.	1296.	20.0	66.1	9.78	3946.4	0.985	132.8

BLOCK TIME = 2.923 HR BLOCK RANGE = 1447.7 NM

### COMBAT PHASES

MACH	ALT	PS1G	NZS	CLS	CDS	ALS	NZI	PSI	CLI	CDI	ALI	CBE
1.50	50000.	-132.	1.0	0.154	0.0432	2.6	5.9	-2358.	0.906	0.2790	15.0	-789.
1.50	50000.	168.	2.0	0.274	0.0582	4.6	6.5	-2286.	0.906	0.2790	15.0	20204.
0.20	100.	281.	1.5	0.911	0.2388	15.0	1.5	245.	0.911	0.2388	15.0	1688.
0.90	30000.	357.	3.1	0.550	0.0866	7.8	5.2	-861.	0.950	0.2717	15.0	7500.

### 1990 NFA Geometry

PLAN AREA	WING 791.1	H.TAIL 301.9	V.TAIL 120.0	CANARD 0.0	UNITS (SQ.FT.)
SURFACE AREA	1248.7	439.9	240.3	0.0	(SQ.FT.)
VOLUME	432.1	105.6	40.7	0.0	(CU.FT.)
SPAN	44.471	30.094	12.267	0.000	(FT.)
L.E. SWEEP	45.000	47.412	40.486	0.000	(DEG.)
C/4 SWEEP	36.254	43.000	34.000	0.000	(DEG.)
T.E. SWEEP	-3.814	24.997	7.806	0.000	(DEG.)
ASPECT RATIO	2.500	3.000	1.254	0.000	
ROOT CHORD	29.647	14.708	14.178	0.000	(FT.)
ROOT THICKNESS	17.788	8.825	8.507	0.000	(IN.)
ROOT T/C	0.050	0.050	0.050	0.000	
TIP CHORD	5.929	5.354	5.388	0.000	(FT.)
TIP THICKNESS	2.846	2.570	2.586	0.000	(IN.)
TIP T/C	0.040	0.040	0.040	0.000	
TAPER RATIO	0.200	0.364	0.380	0.000	
MEAN AERO CHORD	20.424	10.758	10.441	0.000	(FT.)
LE ROOT AT	22.538	45.192	42.727	0.000	(FT.)
C/4 ROOT AT	29.950	48.869	46.272	0.000	(FT.)
TE ROOT AT	52.186	59.900	56.905	0.000	(FT.)
LE M.A.C. AT	31.185	52.104	47.179	0.000	(FT.)
C/4 M.A.C. AT	36.291	54.794	49.789	0.000	(FT.)
TE M.A.C. AT	51.609	62.863	57.620	0.000	(FT.)
Y M.A.C. AT	8.647	6.354	5.215	0.000	(DD)
LE TIP AT	44.774	61.562	53.199	0.000	(FT.)
C/4 TIP AT	46.256	62.900	54.546	0.000	(FT.)
TE TIP AT	50.703	66.915	58.587	0.000	(FT.)
ELEVATIONVOLUME COEFF	0.270	-0.299	2.995	0.000	(FT.)
VOLUME COEFF		0.346	0.046	0.000	

AIRCRAFT WEIGHT = 64314.387 Lbs. AIRCRAFT VOLUME = 1892.013 Cu.Ft. AIRCRAFT DENSITY = 33.993 Lbs./Cu.Ft.

## 1990 NFA Mission Performance

PHASE	M	H	CL	ALPHA	WFUEL	TIME	VEL
	SFC(I)	THRUST(I)	CD	GAMMA	W	WA	Q
	SFC(U)	THRUST(U)	CDINST	L/D	THR/THA	PR	X
CRUISE	0.85	100.	0.0694	0.81	7553.4	26.69	949.
	1.35	12583.	0.0149	0.00	55999.7	0.00	1066.
	0.00	29336.	0.0000	4.65	0.39	0.00	250.
CLIMB	0.95	36000.	0.2264	2.48	1040.2	3.18	922.
	0.98	11801.	0.0287	5.17	54959.5	0.00	302.
	0.00	0.	0.0000	7.90	1.00	0.00	27.
LOITER	0.80	37192.	0.3257	4.37	5296.9	60.00	774.
	0.88	5855.	0.0365	0.00	49662.6	0.00	203.
	0.00	8800.	0.0000	8.92	0.60	0.00	459.
CLIMB	0.89	50000.	0.4986	7.02	1354.1	3.35	863.
	1.90	10604.	0.0723	3.36	48308.5	0.00	136.
	0.00	0.	0.0000	6.89	1.85	0.00	25.
ACCEL	1.50	50000.	0.1550	2.64	1449.7	3.16	1452.
	2.10	17744.	0.0433	0.00	46858.8	0.00	384.
	0.00	25573.	0.0000	3.58	2.00	0.00	37.
CRUISE	1.50	50000.	0.1456	2.49	3956.1	10.46	1452.
	1.73	12879.	0.0424	0.00	42902.4	0.00	384.
	0.00	20709.	0.0000	3.43	1.45	0.00	37.
COMBAT	1.50	50000.	0.2742	4.61	1239.8	2.00	1452.
	2.10	17723.	0.0582	0.39	41662.6	0.00	384.
	0.00	25573.	0.0000	4.71	2.00	0.00	150.
CRUISE	0.91	44000.	0.2642	3.29	3074.7	45.98	881.
	0.92	4228.	0.0284	0.00	38587.9	0.00	188.
	0.00	6775.	0.0000	9.30	0.54	0.00	400.
LOITER	0.30	100.	0.3672	5.31	1295.5	20.00	335.
	0.98	3946.	0.0376	0.00	37292.4	0.00	133.
	0.00	5809.	0.000	9.78	0.12	0.00	66.

#### FUEL SUMMARIES

MISSION FUEL = 27022. RESERVE FUEL = 1351. TRAPPED FUEL = 150.

TOTAL FUEL = 28523.

## 1990 NFA Maneuver Performance

	CONDITIONS	PS	NZ	TDOT	RADIUS	ALPHA	CL	CD
M= 1.50 H=50000.	1 G FLIGHT SUSTAINED MAX. INST. COMBAT ENERG	0.0 -2358.4	1.00 5.92	7.41	465095.		0.154 0.000 0.906	0.0432 0.0000 0.2790
M= 1.50 H=50000.	1 G FLIGHT SUSTAINED MAX. INST. COMBAT ENERG		1.97 6.52	0.00 2.16 8.18 +05	0. 38533. 10174.	2.41 4.61 15.00	0.141 0.274 0.906	0.0421 0.0582 0.2790
M= 0.20 H= 100.	1 G FLIGHT SUSTAINED MAX. INST. COMBAT ENERG	281.4 0.0 $245.4$ GY = 0.1	1.52 1.52	0.00 9.40 9.40 +04	0. 1360. 1360.	12.12 15.00 15.00	0.798 0.911 0.911	0.1494 0.2388 0.2388
M= 0.90 H=30000.	1 G FLIGHT SUSTAINED MAX. INST. COMBAT ENERG	357.2 0.0 -861.2 GY = 0.7	3.13 5.21	0.00 6.11 10.52 +04	0. 8398. 4877.	2.13 7.84 15.00	0.187 0.550 0.950	0.0202 0.0866 0.2717

### 1990 NFA Aerodynamics

Mach =	0.80	Altitude = 40000.	
Parasite Dra Friction Body Wing Strakes H. Tail V. Tail Canard Pods Engine Cowl Boattail	.0104 .0027 .0042 .0000 .0016 .0018 .0000 .0000 .0000 .0000	Induced Drag  Alpha Cl Cd L/D Cm e  0.0 0.000 0.0131 0.0 0.000 0.00  2.0 0.165 0.0173 9.5005 0.83  3.0 0.245 0.0228 10.7009 0.79  4.0 0.302 0.0319 9.5013 0.62  5.0 0.365 0.0418 8.7017 0.59  6.0 0.427 0.0540 7.9022 0.57  8.0 0.548 0.0850 6.4033 0.53  10.0 0.665 0.1249 5.3045 0.50  12.0 0.777 0.1734 4.5059 0.48  15.0 0.934 0.2615 3.6083 0.45	
Wave External Tanks Bombs Stores Extra Camber	.0000 .0013 .0000 .0000 .0000 .0013 .0000	Slope Factors ClAlpha Cdl^.5Alpha	0.0622 0.0332
Cdmin	.0131		
Mach =	1.50	Altitude = 50000.	
Parasite Dra Friction Body Wing Strakes H. Tail V. Tail Canard Pods Engine Cowl Boattail Interference	.0089 .0023 .0036 .0000 .0014 .0016 .0000 .0000 .0000 .0000	Induced Drag Alpha Cl Cd L/D Cm e 0.0 0.000 0.0341 0.0 0.000 0.00 2.0 0.117 0.0382 3.1026 0.43 3.0 0.176 0.0434 4.1039 0.43 4.0 0.237 0.0507 4.7052 0.43 5.0 0.298 0.0602 5.0066 0.43 6.0 0.360 0.0719 5.0080 0.44 8.0 0.483 0.1020 4.7108 0.44 10.0 0.607 0.1411 4.3137 0.44 12.0 0.728 0.1889 3.9166 0.44 15.0 0.906 0.2770 3.3208 0.43	
Wave External Tanks Bombs Stores Extra Camber	.0225 .0023 .0000 .0000 .0000 .0023	Slope Factors ClAlpha Cdl^.5Alpha	0.0604 0.0329
	.0000		

## 1990 NFA Propulsion

#### PHYSICAL ATTRIBUTES

ESF = 1.350 WEIGHT = 4378.459 LENGTH = 17.428 DIAM = 3.939

POWER	MACH	ALT (ft)	THRUST (lb)	SFC	FFLOW (lb/hr)	WAF (lb/sec)
100.00 100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.0 0.0 0.0 0.0 0.0 0.0 0.0	55859. 36792. 32193. 27594. 22995. 18396. 13797. 9198. 4599.	1.747 0.796 0.766 0.743 0.711 0.688 0.684 0.677	97585.6 29285.0 24652.0 20497.5 16343.1 12653.5 9442.0 6230.4 3407.4	425. 425. 394. 360. 331. 291. 248. 213. 142.
100.00 100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.600 0.600 0.600 0.600 0.600 0.600 0.600	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	21133. 11748. 10279. 8811. 7342. 5874. 4405. 2937. 1468.	1.897 0.873 0.854 0.829 0.818 0.821 0.826 0.866 1.016	40089.1 10255.7 8780.6 7305.2 6007.8 4822.8 3637.8 2543.4 1491.7	425. 425. 397. 371. 335. 296. 264. 220. 180.
100.00 100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.900 0.900 0.900 0.900 0.900 0.900 0.900	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	26791. 14601. 12776. 10951. 9126. 7301. 5475. 3650. 1825.	1.913 0.988 0.978 0.964 0.968 0.997 1.045 1.161 1.559	51255.9 14425.6 12489.3 10553.0 8835.7 7278.9 5722.2 4238.5 2844.8	425. 425. 400. 377. 344. 309. 278. 241. 201.
100.00 100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	1.500 1.500 1.500 1.500 1.500 1.500 1.500 1.500	50000.0 50000.0 50000.0 50000.0 50000.0 50000.0 50000.0 50000.0	17744. 8870. 7761. 6653. 5544. 4435. 3326. 2218. 1109.	2.100 1.126 1.113 1.112 1.111 1.138 1.212 1.360 1.896	37256.7 9987.7 8638.4 7397.9 6157.4 5048.8 4032.4 3016.1 2102.7	421. 421. 399. 373. 349. 318. 285. 258. 217.

## 1990 NFA Weights

COMPONENT	POUNDS	KILOGRAMS	PERCENT
	6526. 5885. 1322. 1038. 0. 150.	2960. 2670. 600. 471. 0. 68.	10.15 9.15 2.06 1.61 0.00 0.23 0.00
PROPULSION ENGINES (1) FUEL SYSTEM	7037. 5079. 1958.	3193. 2304. 888.	10.94 7.90 3.05
FIXED EQUIPMENT (COMPONENTS BELOW DO NOT HYD. + PNEU. ELECTRICAL AVIONICS INSTRUMENTATION DE-ICE/AIR CONDITION AUXILIARY GEAR FURNISH. + EQPT. FLIGHT CONTROLS	TNOTITION MOOI	2630. H FACTOR=0.9) 424. 247. 749. 43. 277. 91. 170. 922.	
	28523.		44.35
PAYLOAD  FLIGHT CREW ( 1)  ARMAMENT  AMMUNITION  LONG RANGE MISSILES  LRM PYLONS & LAUNCHERS  SHORT RANGE MISSILES  SRM LAUNCHERS  EXTERNAL TANKS	180. 612. 287. 1974.	278. 130. 895. 318. 181. 91.	0.28 0.95 0.45 3.07 0.49
TOTAL WEIGHT	64315.	29173.	100.00

### 1990 STOVL Summary

### Standard English Units

GENERAL	FUSELAGE		WING	HTAIL	VTAIL
TOGW 80510. W/S 90.0 T/W DRY 0.78 T/W WET 1.18 CREW 1 N(Z) ULT 11.3	LENGTH 64.0 DIAMETER 7.1 VOLUME 1871.1 WETTED AREA 1179.5 FINENESS RATIO 9.0	AREA WETTED AREA SPAN L.E. SWEEP C/4 SWEEP ASPECT RATIO TAPER RATIO	894.6 1369.7 47.3 50.0 42.8 2.50 0.20	477.7 2 32.0 47.4 43.0 3.00	35.7 71.7 13.0 45.9 34.0 1.25 0.38
ENGINE	WEIGHTS	T/C ROOT T/C TIP	0.20 0.05 0.04	0.05	0.38 0.05 0.04
NUMBER 1 LENGTH 22.7 DIAM. 5.1 WEIGHT 11262. TSLS 62682. SFCSLS 0.80	W % STRUCT. 20602. 25.6 PROPUL. 15831. 19.7 FIX. EQ. 6469. 8.0 FUEL 32656. 40.6 PAYLOAD 4951. 6.1	ROOT CHORD TIP CHORD M.A. CHORD LOC. OF L.E.	31.5 6.3 21.7 24.1	5.7 11.4	15.1 5.7 11.1 45.7

#### MISSION SUMMARY

PHASE	MACH	ALT	FUEL	TIME	DIST	L/D	THRUST	SFC	Q
======	====	=====	=====	=====	=====	=====	======	=====	======
TAKEOFF	0.00	0.	1297.	10.5					
CRUISE	0.85	100.	9970.	26.7	250.0	5.11	14185.8	1.575	1066.4
CLIMB	0.92	35000.	1032.	1.8	15.3	8.70	20537.0	0.968	298.0
LOITER	0.79	36433.	7086.	60.0	454.3	8.45	7634.9	0.896	206.4
CLIMB	0.89	50000.	1202.	1.7	12.6	6.23	18066.5	1.896	135.7
ACCEL	1.50	50000.	1117.	1.5	16.9	4.06	30230.2	2.100	383.7
CRUISE	1.50	50000.	2811.	10.5	150.0	3.97	14349.4	1.116	383.7
COMBAT	1.50	50000.	1197.	2.0	28.7	5.21	21261.7	1.689	383.7
CRUISE	0.91	41000.	4274.	46.0	400.0	9.17	5621.1	0.959	217.2
LOITER	0.30	100.	970.	10.0	33.1	9.13	5534.2	1.052	132.8

BLOCK TIME = 2.672 HR BLOCK RANGE = 1363.1 NM

### COMBAT PHASES

MACH	ALT	PS1G	NZS	CLS	CDS	ALS	NZI	PSI	CLI	CDI	ALI	CBE
1.50	50000.	15.	1.1	0.190	0.0440	2.2	5.3	-1994.	0.903	0.2778	15.0	90.
0.90	30000.	513.	3.4	0.616	0.1130	9.8	4.3	-451.	0.882	0.2446	15.0	3081.
1.50	50000.	414.	2.8	0.322	0.0618	4.2	5.7	-1716.	0.903	0.2778	15.0	49656.

## 1990 STOVL Geometry

PLAN AREASURFACE AREAVOLUME	WING 894.6 1369.7 506.3	H.TAIL 341.4 477.7 127.0	V.TAIL 135.7 271.7 48.9	CANARD 0.0 0.0 0.0	UNITS (SQ.FT.) (SQ.FT.) (CU.FT.)
SPAN	47.291	32.002	13.045	0.000	(FT.)
L.E. SWEEP	50.000	47.412	40.486	0.000	(DEG.)
C/4 SWEEP	42.772 7.130	43.000 24.997	34.000 7.806	0.000	(DEG.)
ASPECT RATIO	2.500	3.000	1.254	0.000	(DEG.)
ROOT CHORD	31.527	15.641	15.077	0.000	(FT.)
ROOT THICKNESS	18.916	9.385	9.046	0.000	(IN.)
ROOT T/C	0.050	0.050	0.050	0.000	,,
TIP CHORD	6.305	5.693	5.729	0.000	(FT.)
TIP THICKNESS	3.027	2.733	2.750	0.000	(IN.)
TIP T/C	0.040	0.040	0.040	0.000	
TAPER RATIO	0.200	0.364	0.380	0.000	(DT)
MEAN AERO CHORD LE ROOT AT	21.719 24.118	11.440 48.359	11.103 45.723	0.000	(FT.)
C/4 ROOT AT	32.000	52.269	49.493	0.000	(FT.) (FT.)
TE ROOT AT	55.645	64.000	60.800	0.000	(FT.)
LE M.A.C. AT	35.077	55.710	50.458	0.000	(FT.)
C/4 M.A.C. AT	40.507	58.570	53.233	0.000	(FT.)
TE M.A.C. AT	56.796	67.150	61.560	0.000	(FT.)
Y M.A.C. AT	9.195	6.757	5.546	0.000	
LE TIP AT	52.298	65.767	56.859	0.000	(FT.)
C/4 TIP AT	53.874	67.190	58.292	0.000	(FT.)
TE TIP AT	58.603 .0.000	71.460 -0.355	62.588	0.000	(FT.)
VOLUME COEFF	.0.000	0.317	3.550 0.041	0.000 0.000	(FT.)

AIRCRAFT WEIGHT = 80510.859 Lbs. AIRCRAFT VOLUME = 2602.273 Cu.Ft. AIRCRAFT DENSITY = 30.939 Lbs./Cu.Ft.

# 1990 STOVL Mission Performance

PHASE	M	H	CL	ALPHA	WFUEL	TIME	VEL
	SFC(I)	THRUST(I)	CD	GAMMA	W	WA	Q
	SFC(U)	THRUST(U)	CDINST	L/D	THR/THA	PR	X
CRUISE	0.85	100.	0.0761	0.98	9970.1	26.69	949.
	1.57	14186.	0.0149	0.00	69243.8	0.00	1066.
	0.00	40648.	0.0000	5.11	0.26	0.00	250.
CLIMB	0.92	35000.	0.2921	4.12	1032.2	1.77	898.
	0.97	20537.	0.0336	9.77	68211.5	0.00	298.
	0.00	0.	0.0000	8.70	1.00	0.00	15.
LOITER	0.79	36433.	0.3495	5.21	7086.4	60.00	765.
	0.90	7635.	0.0413	0.00	61125.1	0.00	206.
	0.00	12186.	0.0000	8.45	0.45	0.00	454.
CLIMB	0.89	50000.	0.5345	8.36	1202.0	1.73	863.
	1.90	18066.	0.0858	7.32	59923.2	0.00	136.
	0.00	0.	0.0000	6.23	1.85	0.00	13.
ACCEL	1.50	50000.	0.1717	1.96	1116.8	1.46	1452.
	2.10	30230.	0.0423	0.00	58806.4	0.00	384.
	0.00	43569.	0.0000	4.06	2.00	0.00	17.
CRUISE	1.50	50000.	0.1659	1.87	2810.8	10.46	1452.
	1.12	14349.	0.0418	0.00	55995.0	0.00	384.
	0.00	27489.	0.0000	3.97	0.95	0.00	150.
COMBAT	1.50	50000.	0.3217	4.23	1197.1	2.00	1452.
	1.69	21262.	0.0618	1.12	54797.9	0.00	384.
	0.00	43569.	0.0000	5.21	1.41	0.00	29.
CRUISE	0.91	41000.	0.2653	3.68	4274.4	45.98	881.
	0.96	5621.	0.0289	0.00	50523.5	0.00	217.
	0.00	10098.	0.0000	9.17	0.37	0.00	400.
LOITER	0.30	100.	0.4252	6.60	970.3	10.00	335.
	1.05	5534.	0.0466	0.00	49553.2	0.00	133.
	0.00	8505.	0.0000	9.13	0.10	0.00	33.

### FUEL SUMMARIES

MISSION FUEL = 30958.
RESERVE FUEL = 1548.
TRAPPED FUEL = 150.

TOTAL FUEL = 32656.

## 1990 STOVL Maneuver Performance

	CONDITIONS	PS	NZ	TDOT	RADIUS	ALPHA	CL	CD
M= 1.50 H=50000.	1 G FLIGHT SUSTAINED MAX. INST COMBAT ENERG		1.00 1.12 5.34 97338E-	6.66	0. 130096. 12498.	1.95 2.24 15.00	0.171 0.190 0.903	0.0423 0.0440 0.2778
M= 0.90 H=30000.	1 G FLIGHT SUSTAINED MAX. INST. COMBAT ENERG	513.4 0.0 -450.6 SY = 0.3	1.00 3.36 4.34 08067E-	0.00 6.60 8.70 +04	0. 7769. 5898.	2.72 9.81 15.00	0.212 0.616 0.882	0.0215 0.1130 0.2446
M= 1.50 H=50000.	1 G FLIGHT SUSTAINED MAX. INST	413.8 0.0 1715.7 Y = 0.4	1.00 2.77 5.68	0.00 3.28 7.09	0. 25343. 11729.	1.82 4.23 15.00	0.163 0.322 0.903	0.0416 0.0618 0.2778

## 1990 STOVL Aerodynamics

Mach =	0.80	Altitude = 40000.	
Parasite Drag Friction Body Wing Strakes H. Tail V. Tail Canard Pods Engine Cowl Boattail Interference Wave	.0104 .0030 .0041 .0000 .0016 .0018 .0000 .0000 .0000 .0000 .0000	Induced Drag Alpha Cl Cd L/D Cm e 0.0 0.000 0.0121 0.0 0.000 0.00 2.0 0.151 0.0157 9.6004 0.82 3.0 0.223 0.0207 10.8006 0.74 4.0 0.280 0.0286 9.8009 0.61 5.0 0.338 0.0374 9.0012 0.58 6.0 0.396 0.0482 8.2016 0.55 8.0 0.508 0.0758 6.7024 0.52 10.0 0.617 0.1116 5.5033 0.49 12.0 0.722 0.1555 4.6044 0.46 15.0 0.870 0.2359 3.7064 0.43	
External Tanks Bombs	.0002	Slope Factors ClAlpha Cdl^.5Alpha	0.0580 0.0315
Stores Extra Camber	.0000 .0002 .0000		
Cdmin	.0121		
Mach =	1.50	Altitude = 50000.	
Parasite Drag Friction Body Wing Strakes H. Tail V. Tail Canard Pods Engine Cowl Boattail Interference	.0089 .0026 .0035 .0000 .0013 .0015 .0000 .0000 .0000	Altitude = 50000.  Induced Drag Alpha Cl Cd L/D Cm e 0.0 0.000 0.0324 0.0 0.000 0.00 2.0 0.175 0.0391 4.5028 0.57 3.0 0.240 0.0461 5.2041 0.53 4.0 0.306 0.0557 5.5055 0.51 5.0 0.372 0.0680 5.5069 0.49 6.0 0.438 0.0830 5.3084 0.48 8.0 0.569 0.1211 4.7116 0.46 10.0 0.699 0.1703 4.1149 0.45 12.0 0.826 0.2304 3.6184 0.44 15.0 0.903 0.2744 3.3201 0.43	
Parasite Drag Friction Body Wing Strakes H. Tail V. Tail Canard Pods Engine Cowl Boattail	.0089 .0026 .0035 .0000 .0013 .0015 .0000 .0000	Induced Drag Alpha Cl Cd L/D Cm e 0.0 0.000 0.0324 0.0 0.000 0.00 2.0 0.175 0.0391 4.5028 0.57 3.0 0.240 0.0461 5.2041 0.53 4.0 0.306 0.0557 5.5055 0.51 5.0 0.372 0.0680 5.5069 0.49 6.0 0.438 0.0830 5.3084 0.48 8.0 0.569 0.1211 4.7116 0.46 10.0 0.699 0.1703 4.1149 0.45 12.0 0.826 0.2304 3.6184 0.44	0.0602 0.0328

## 1990 STOVL Propulsion

PHYSICAL ATT	RIBUTES	НО	VER PERFORI DR		WET	
ESF = WEIGHT = 112			T = 59 $T/W = 5$	381. .272	59381. 5.272	lb
LENGTH = DIAM =	22.749 5.141		SFC = 0	795. .803 .000	795. 0.803 0.000	
POWER	MACH	ALT (ft)	THRUST (lb)	SFC	FFLOW (lb/hr)	WAF (lb/sec)
100.00 100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.0 0.0 0.0 0.0 0.0 0.0	95167. 62682. 54847. 47011. 39176. 31341. 23506. 15670. 7835.	1.747 0.796 0.766 0.743 0.711 0.688 0.684 0.677		725. 725. 671. 614. 564. 497. 422. 364. 241.
100.00 100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.600 0.600 0.600 0.600 0.600 0.600 0.600	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	36004. 20014. 17513. 15011. 12509. 10007. 7505. 5004. 2502.	1.897 0.873 0.854 0.829 0.818 0.821 0.826 0.866 1.016	17472.7 14959.5 12446.0 10235.4 8216.6 6197.8	725. 725. 676. 632. 570. 505. 450. 375.
100.00 100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.900 0.900 0.900 0.900 0.900 0.900 0.900	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	45644. 24876. 21767. 18657. 15548. 12438. 9329. 6219. 3110.	1.913 0.988 0.978 0.964 0.968 0.997 1.045 1.161 1.559	87324.9 24576.9 21278.0 17979.2 15053.4 12401.1 9748.9 7221.1 4846.7	725. 725. 682. 643. 587. 526. 474. 411. 343.
100.00 100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	1.500 1.500 1.500 1.500 1.500 1.500 1.500	50000.0 50000.0 50000.0 50000.0 50000.0 50000.0 50000.0 50000.0	30230. 15112. 13223. 11334. 9445. 7556. 5667. 3778. 1889.	2.100 1.126 1.113 1.112 1.111 1.138 1.212 1.360 1.896	63474.3 17016.1 14717.3 12603.9 10490.4 8601.6 6870.1 5138.6 3582.4	718. 718. 679. 635. 595. 542. 486. 439. 369.

## 1990 STOVL Weights

COMPONENT	POUNDS	KILOGRAMS	PERCENT
AIRFRAME STRUCTURE WING FUSELAGE HORIZONTAL TAIL VERTICAL TAIL REACTION CONTROL SYSTEM WING FOLD INTERNAL BAY STRUCTURE ALIGHTING GEAR	20602. 8991. 5584. 1533. 1202. 171. 150. 0. 2971.	9620. 4078. 2533. 695. 545. 78. 68. 0. 1348.	25.59 11.17 6.94 1.90 1.49 0.21 0.19 0.00 3.69
PROPULSION ENGINES (1) FUEL SYSTEM	15831. 12411. 3420.	7183. 5630. 1551.	19.66 15.42 4.25
FIXED EQUIPMENT  (COMPONENTS BELOW DO NOT HYD. + PNEU. ELECTRICAL AVIONICS INSTRUMENTATION DE-ICE/AIR CONDITION AUXILIARY GEAR FURNISH. + EQPT. FLIGHT CONTROLS	1170. 544. 1652. 94.	FACTOR=0.9) 531. 247. 749. 43.	1.45 0.68
FUEL	32656.	14813.	40.56
PAYLOAD  FLIGHT CREW ( 1)  ARMAMENT  AMMUNITION  LONG RANGE MISSILES  LRM PYLONS & LAUNCHERS  SHORT RANGE MISSILES  SRM LAUNCHERS  EXTERNAL TANKS	4951. 180. 612. 287. 1974. 1300. 398. 200. 0.	1974. 82. 278. 130. 895. 318. 181. 91. 0.	6.15 0.22 0.76 0.36 2.45 0.87 0.49 0.25 0.00
TOTAL WEIGHT	80510.	36519.	100.00

### 1995 Fighter Summary

### Standard English Units

GENERAL	FUSELAGE		WING	HTAIL	VTAIL
TOGW 53356.	LENGTH 49.0	AREA	794.0	297.8	82.9
W/S 67.2	DIAMETER 4.9	WETTED AREA	1481.5	436.6	166.0
T/W DRY 0.58	VOLUME 702.3	SPAN	73.4	28.9	9.9
T/W A/B 0.88	WETTED AREA 634.0	L.E. SWEEP	20.0	51.0	57.1
CREW 2	FINENESS RATIO 10.0	C/4 SWEEP	15.8	44.6	48.0
N(Z) ULT 13.5		ASPECT RATIO	6.79	2.81	1.17
		TAPER RATIO	0.29	0.18	0.32
ENGINE	WEIGHTS	T/C ROOT	0.12	0.05	0.05
	•	T/C TIP	0.09	0.04	0.04
NUMBER 1	W %	ROOT CHORD	16.7	17.5	12.7
LENGTH 15.3	STRUCT. 18718. 35.1	TIP CHORD	4.9	3.1	4.1
DIAM. 3.5	PROPUL. 4382. 8.2	M.A. CHORD	11.9	12.0	9.1
WEIGHT 2768.9	FIX. EQ. 6926. 13.0	LOC. OF L.E.	17.6	31.5	36.2
TSLS 30930.	FUEL 14746. 27.6				
SFCSLS 0.80	PAYLOAD 8583. 16.1				

### MISSION SUMMARY

PHASE	MACH	ALT	FUEL	TIME	DIST	L/D	THRUST	SFC	Q
======	====	=====	=====	=====	======	=====	======	=====	=====
TAKEOFF	0.00	0.	649.	10.5					
CLIMB	0.88	50000.	1633.	9.8	82.0	15.28	4745.0	0.945	131.9
CRUISE	0.85	50000.	2288.	49.2	400.0	15.86	3110.6	0.881	123.2
LOITER	0.55	35644.	2362.	60.0	316.7	16.13	2949.6	0.790	103.1
CLIMB	0.89	50000.	674.	2.0	14.5	14.44	8800.8	1.878	135.7
ACCEL	1.50	50000.	885.	2.3	27.4	5.17	16149.5	1.934	383.7
CRUISE	1.50	50000.	1151.	7.0	100.0	5.10	8649.8	1.141	383.7
COMBAT	1.60	35000.	1402.	3.0	46.1	4.39	19814.2	1.415	894.8
CRUISE	0.80	50000.	1940.	52.3	400.0	16.11	2535.5	0.864	109.1
LOITER	0.30	100.	918.	20.0	66.1	14.43	2797.9	0.984	132.8

BLOCK TIME = 3.432 HR BLOCK RANGE = 1455.4 NM

### COMBAT PHASES

MACH	ALT	PS1G	NZS	CLS	CDS	ALS	NZI	PSI	CLI	CDI	ALI	CBE
1.50	50000.	1.	1.0	0.149	0.0286	1.2	5.3	-2340.	0.768	0.2649	15.0	6.
1.60	35000.	549.	4.8	0.123	0.0279	1.0	9.0	-1845.	0.541	0.1200	10.5	98837.
0.20	100.	244.	2.0	1.399	0.1275	15.0	2.0	217.	1.399	0.1275	15.0	1465.
0.90	30000.	305.	3.9	0.580	0.0638	5.6	7.2	-1466.	1.180	0.3501	15.0	1832.

#### 1995 Fighter Geometry

	WING	H.TAIL	V.TAIL	CANARD	UNITS
PLAN AREA	794.0	297.8	82.9	0.0	(SQ.FT.)
SURFACE AREA	1481.5	436.6	166.0	0.0	(SQ.FT.)
VOLUME	700.4	117.3	24.7	0.0	(CU.FT.)
SPAN	73.425	28.925	9.863	0.000	(FT.)
L.E. SWEEP	20.000	51.000	53.025	0.000	(DEG.)
C/4 SWEEP	15.834	44.598	48.000	0.000	(DEG.)
T.E. SWEEP	2.437	13.471	24.594	0.000	(DEG.)
ASPECT RATIO	6.790	2.810	1.173	0.000	
ROOT CHORD	16.714	17.491	12.701	0.000	(FT.)
ROOT THICKNESS	24.870	10.495	7.621	0.000	(IN.)
ROOT T/C	0.124	0.050	0.050	0.000	
TIP CHORD	4.914	3.096	4.115	0.000	(FT.)
TIP THICKNESS	5.307	1.486	1.975	0.000	(IN.)
TIP T/C	0.090	0.040	0.040	0.000	
TAPER RATIO	0.294	0.177	0.324	0.000	
MEAN AERO CHORD	11.887	11.971	9.139	0.000	(FT.)
LE ROOT AT	17.634	31.459	36.249	0.000	(FT.)
C/4 ROOT AT	21.812	35.831	39.424	0.000	(FT.)
TE ROOT AT	34.347	48.950	48.950	0.000	(FT.)
LE M.A.C. AT	23.100	38.307	41.684	0.000	(FT.)
C/4 M.A.C. AT	26.071	41.300	43.969	0.000	(FT.)
TE M.A.C. AT	34.987	50.278	50.823	0.000	(FT.)
Y M.A.C. AT	15.018	5.546	4.092	0.000	
LE TIP AT	30.996	49.318	49.349	0.000	(FT.)
C/4 TIP AT	32.224	50.092	50.378	0.000	(FT.)
TE TIP AT	35.910	52.414	53.464	0.000	(FT.)
ELEVATION	1.713	0.000	2.447	0.000	(FT.)
VOLUME COEFF		0.480	0.025	0.000	

AIRCRAFT WEIGHT = 53354.504 Lbs. AIRCRAFT VOLUME = 1569.422 Cu.Ft. AIRCRAFT DENSITY = 33.996 Lbs./Cu.Ft.

1995 Fighter Mission Performance

PHASE	M	H	CL	ALPHA	WFUEL	TIME	VEL
	SFC(I)	THRUST(I)	CD	GAMMA	W	WA	Q
	SFC(U)	THRUST(U)	CDINST	L/D	THR/THA	PR	X
CLIMB	0.88	50000.	0.4909	4.41	1632.8	9.80	851.
	0.94	4745.	0.0321	1.55	51072.3	0.00	132.
	0.00	0.	0.0000	15.28	1.00	0.00	82.
CRUISE	0.85	50000.	0.5045	4.36	2287.9	49.23	823.
	0.88	3111.	0.0318	0.00	48784.4	0.00	123.
	0.00	4550.	0.0000	15.86	0.67	0.00	400.
LOITER	0.55	35644.	0.5811	5.40	2361.6	60.00	534.
	0.79	2950.	0.0360	0.00	46422.7	0.00	103.
	0.00	4062.	0.0000	16.13	0.40	0.00	317.
CLIMB	0.89	50000.	0.4218	3.83	674.0	1.99	863.
	1.88	8801.	0.0292	7.09	45748.7	0.00	136.
	0.00	0.	0.0000	14.44	1.83	0.00	14.
ACCEL	1.50	50000.	0.1476	1.15	884.8	2.34	1452.
	1.93	16150.	0.0286	0.00	44863.9	0.00	384.
	0.00	22403.	0.0000	5.17	1.85	0.00	27.
CRUISE	1.50	50000.	0.1447	1.09	1151.0	6.97	1452.
	1.14	8650.	0.0284	0.00	43712.6	0.00	384.
	0.00	14884.	0.0000	5.10	0.99	0.00	100.
COMBAT	1.60	35000.	0.1225	1.04	1401.6	3.00	1557.
	1.41	19814.	0.0279	0.83	42311.0	0.00	895.
	0.00	49750.	0.0000	4.39	1.14	0.00	46.
CRUISE	0.80	50000.	0.4714	3.80	1939.7	52.30	774.
	0.86	2536.	0.0293	0.00	40371.3	0.00	109.
	0.00	3689.	0.0000	16.11	0.57	0.00	400.
LOITER	0.30	100.	0.3828	3.82	917.9	20.00	335.
	0.98	2798.	0.0265	0.00	39453.5	0.00	133.
	0.00	4060.	0.0000	14.43	0.09	0.00	66.

FUEL SUMMARIES

MISSION FUEL = 13901. RESERVE FUEL = 695. TRAPPED FUEL = 150.

TOTAL FUEL = 14746.

### 1995 Fighter Maneuver Performance

	CONDITIONS	PS	NZ	TDOT	RADIUS	ALPHA	CL	CD
M= 1.50 H=50000.	1 G FLIGHT SUSTAINED MAX. INST COMBAT ENERG			6.56	0. 368643. 12677.	1.15 1.18 15.00	0.147 0.149 0.768	0.0285 0.0286 0.2649
M= 1.60 H=35000.	1 G FLIGHT SUSTAINED MAX. INST COMBAT ENERG		9.00		0. 16048. 8424.	0.34 1.04 10.49	0.062 0.123 0.541	0.0262 0.0279 0.1200
M= 0.20 H= 100.	1 G FLIGHT SUSTAINED MAX. INST. COMBAT ENERG	244.1 0.0 216.6 SY = 0.1	1.96	0.00 13.95 13.95 +04	0. 917. 917.	8.78 15.00 15.00	0.842 1.399 1.399	0.0571 0.1275 0.1275
M= 0.90 H=30000.	1 G FLIGHT SUSTAINED MAX. INST COMBAT ENERG	305.3 0.0 -1465.6 SY = 0.1	1.00 3.93 7.16 83170E	0.00 7.83 14.61 +04	0. 6554. 3512.	1.52 5.57 15.00	0.168 0.580 1.180	0.0213 0.0638 0.3501

## 1995 Fighter Aerodynamics

Mach	=	0.80	Altitude	= 400	00.				
Parasite	Drac	r	Induced	Drag					
Friction		.0110	Alpha	Cl	Cd	L/D	Cm	е	
Body		.0019	0.0	0.000	0.0141	0.0	0.000	0.00	
Wing		.0063	2.0	0.252	0.0173	14.6	008	0.95	
Strakes		.0000	3.0	0.375	0.0211	17.7	013	0.94	
H. Tail		.0016	4.0	0.496	0.0264	18.8	019	0.94	
V. Tail		.0013	5.0	0.618	0.0402	15.4	025	0.69	
Canard		.0000	6.0	0.708	0.0737	9.6	029	0.40	
Pods		.0000	8.0	0.883	0.1165	7.6		0.36	
Engine		.0000	10.0	1.049	0.1710			0.33	
Cowl	_	.0000	12.0		0.2369			0.31	
_Boattai		.0000	15.0	1.369	0.3932	3.5	070	0.23	
Interfer	ence	.0025							
Wave		.0001							
External		.0005			-	e Fact	ors		0 0010
Tanks		.0000				Alpha	1		0.0912
Bombs		.0000			Ca	l1^.5Al	pna		0.0410
Stores		.0000							
Extra Camber		.0005							
Caliber		.0000							
Cdmin		.0141							
yawe	sweep d asp aero		2 io 6 1 0.	0.41 .747 1.92 1179 3.19					

### 1995 Fighter Aerodynamics

Mach =	1.50	Altitude	= 500	00.				
Parasite Drag	q	Induced	Drag					
Friction	.0085	Alpha	Cl	Cđ	L/D	Cm	е	
Body	.0016	0.0	0.000	0.0189	0.0	0.000	0.00	
Wing	.0045	2.0	0.187	0.0247	7.6	051	0.55	
Strakes	.0000	3.0	0.234		7.9		0.47	
H. Tail	.0014	4.0	0.281		7.8		0.42	
V. Tail	.0011	5.0	0.328		7.5		0.39	
Canard	.0000	6.0	0.376	0.0537	7.0	122	0.37	
_Pods	.0000	8.0		0.0788	6.0		0.34	
Engine	.0000	10.0		0.1117			0.32	
Cowl	.0000			0.1842			0.24	
Boattail	.0000	15.0	0.768	0.2582	3.0	220	0.22	
Interference	.0002 .0093							
Wave External	.0093			Slone	e Fact	ore		
Tanks	.0000				Alpha	OLS		0.0512
Bombs	.0000				1^.5A1	nha		0.0326
Stores	.0000			- Cu				0.0520
Extra	.0009					•		
Camber	.0000							
Cdmin	.0189							
For a variable c/4 sweet yawed as mean aere t/c span	p pect rati	.0 3 .0 1	0.05 .488 6.58 0868 62.63					

### 1995 Fighter Propulsion

#### PHYSICAL ATTRIBUTES

ESF = 1.070 WEIGHT = 2768.881 LENGTH = 15.309 DIAM = 3.486

POWER	MACH	ALT (ft)	THRUST (1b)	SFC	FFLOW (lb/hr)	WAF (lb/sec)
100.00 100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.0 0.0 0.0 0.0 0.0 0.0 0.0	46818. 30930. 27064. 23198. 19332. 15465. 11599. 7733. 3866.	1.714 0.803 0.778 0.745 0.702 0.695 0.685 0.664 0.723	80245.8 24836.3 21060.2 17283.3 13565.0 10755.7 7946.4 5137.1 2795.7	337. 337. 310. 286. 263. 222. 189. 164. 106.
100.00 100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.600 0.600 0.600 0.600 0.600 0.600 0.600	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	17568. 9799. 8574. 7349. 6124. 4899. 3675. 2450. 1225.	1.875 0.868 0.847 0.820 0.808 0.809 0.810 0.843 0.965	32940.6 8505.6 7266.2 6026.7 4950.7 3964.4 2978.0 2064.0 1182.1	337. 337. 314. 294. 262. 231. 204. 167. 135.
100.00 100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.900 0.900 0.900 0.900 0.900 0.900 0.900	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	22238. 12205. 10679. 9154. 7628. 6102. 4577. 3051. 1526.	1.893 0.981 0.968 0.951 0.953 0.979 1.022 1.127 1.490	42101.2 11977.4 10342.3 8707.2 7271.4 5973.5 4675.6 3438.9 2272.6	337. 337. 316. 297. 270. 241. 216. 185. 152.
100.00 100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	1.500 1.500 1.500 1.500 1.500 1.500 1.500 1.500	50000.0 50000.0 50000.0 50000.0 50000.0 50000.0 50000.0	16150. 8728. 7637. 6546. 5455. 4364. 3273. 2182. 1091.	1.934 1.143 1.123 1.112 1.095 1.112 1.164 1.269 1.671	31238.7 9977.1 8579.6 7277.1 5974.5 4853.8 3811.2 2768.5 1823.5	337. 337. 317. 294. 274. 244. 215. 191. 154.

## 1995 Fighter Weights

COMPONENT	POUNDS	KILOGRAMS	PERCENT
AIRFRAME STRUCTURE WING FUSELAGE HORIZONTAL TAIL VERTICAL TAIL REACTION CONTROL SYSTEM WING FOLD INTERNAL BAY STRUCTURE ALIGHTING GEAR	0.	4804. 1732. 554. 305. 0. 0.	19.85 7.16
PROPULSION ENGINES (1) FUEL SYSTEM	4382. 3212. 1170.	1988. 1457. 531.	8.21 6.02 2.19
FIXED EQUIPMENT  (COMPONENTS BELOW DO NOT HYD. + PNEU. ELECTRICAL AVIONICS INSTRUMENTATION DE-ICE/AIR CONDITION AUXILIARY GEAR FURNISH. + EQPT. FLIGHT CONTROLS	6926. INCLUDE TECH 775. 784. 3006. 169. 995. 200. 534. 1685.	EXCMOD O OC	
FUEL		6689.	
PAYLOAD  FLIGHT CREW ( 2)  ARMAMENT  AMMUNITION  LONG RANGE MISSILES  LRM PYLONS & LAUNCHERS  SHORT RANGE MISSILES  SRM LAUNCHERS  EXTERNAL TANKS	612. 287. 3948.	3893. 163. 278. 130. 1791. 853. 361. 318. 0.	16.09 0.67 1.15 0.54 7.40 3.52 1.49 1.31 0.00
TOTAL WEIGHT	53356.	24202.	100.00

### 1995 Light Attack Summary

### Standard English Units

GENERAL	FUSELAGE		WING	HTAIL	VTAIL
TOGW 21046. W/S 73.6 T/W 0.51 CREW 1 N(Z) ULT 9.8	LENGTH 35.0 DIAMETER 4.5 VOLUME 464.1 WETTED AREA 444.3 FINENESS RATIO 7.8	AREA WETTED AREA SPAN L.E. SWEEP C/4 SWEEP ASPECT RATIO TAPER RATIO	285.9 468.2 35.9 22.5 16.6 4.51 0.31	75.5 96.5 16.4 35.0 30.0 3.57 0.39	42.5 85.2 6.6 47.8 30.0 1.02 0.30
ENGINE	WEIGHTS	T/C ROOT T/C TIP	0.09	0.09	0.08
NUMBER 1 LENGTH 8.7	W % STRUCT. 5980. 28.4	ROOT CHORD TIP CHORD	12.1	6.6 2.6	9.9
DIAM. 2.9 WEIGHT 1144.9	PROPUL. 1765. 8.4 FIX. EQ. 3802. 18.1	M.A. CHORD LOC. OF L.E.	8.7 7.0	4.9 25.0	7.1 25.1
TSLS 10826. SFCSLS 0.45	FUEL 4940. 23.5 PAYLOAD 4559. 21.7				

### MISSION SUMMARY

PHASE	MACH	ALT	FUEL	TIME	DIST	L/D	THRUST	SFC	Q
======	====	=====	=====	====	=====	=====	======	=====	=====
TAKEOFF	0.00	0.	120.	10.5					
CLIMB	0.82	36500.	431.	10.1	75.0	11.59	2316.4	0.665	220.5
CRUISE	0.80	36500.	1230.	65.4	500.0	11.66	1677.8	0.664	208.3
CRUISE	0.80	100.	411.	5.7	50.0	3.37	5647.9	0.769	944.6
COMBAT	0.85	100.	173.	2.0	18.7	5.72	6569.9	0.791	1066.4
CRUISE	0.80	100.	410.	5.7	50.0	3.27	5642.2	0.769	944.6
CLIMB	0.82	39500.	400.	10.3	76.1	11.65	2006.9	0.663	189.9
CRUISE	0.80	39500.	1064.	65.4	500.0	11.70	1458.8	0.660	180.4
LOITER	0.30	100.	321.	20.0	66.1	12.37	1358.2	0.710	132.8

BLOCK TIME = 3.077 HR BLOCK RANGE = 1336.1 NM

#### COMBAT PHASES

MACH	ALT	PS1G	NZS	CLS	CDS	ALS	NZI	PSI	CLI	CDI	ALI	CBE
0.85	100.	60.	4.0	0.123	0.0215	0.9	6.5	-105.	0.396	0.0315	2.9	7195.
0.20	100.	107.	1.5	1.324	0.1572	15.0	1.5	88.	1.324	0.1572	15.0	640.

### 1995 Light Attack Geometry

	WING	H.TAIL	V.TAIL	CANARD	UNITS
PLAN AREA	285.9	75.5	42.5	0.0	(SQ.FT.)
SURFACE AREA	468.2	96.5	85.2	0.0	(SQ.FT.)
VOLUME	118.1	21.4	15.6	0.0	(CU.FT.)
SPAN	35.916	16.428	6.582	0.000	(FT.)
L.E. SWEEP	22.483	35.042	40.035	0.000	(DEG.)
C/4 SWEEP	16.576	30.000	30.000	0.000	(DEG.)
T.E. SWEEP	-2.917	11.612	-11.916	0.000	(DEG.)
ASPECT RATIO	4.513	3.574	1.020	0.000	
ROOT CHORD	12.133	6.633	9.912	0.000	(FT.)
ROOT THICKNESS	13.103	7.163	9.396	0.000	(IN.)
ROOT T/C	0.090	0.090	0.079	0.000	
TIP CHORD	3.785	2.560	2.993	0.000	(FT.)
TIP THICKNESS	2.726	2.151	2.335	0.000	(IN.)
TIP T/C	0.060	0.070	0.065	0.000	
TAPER RATIO	0.312	0.386	0.302	0.000	
MEAN AERO CHORD	8.689	4.897	7.071	0.000	(FT.)
LE ROOT AT	6.982	24.988	25.105	0.000	(FT.)
C/4 ROOT AT	10.015	26.646	27.583	0.000	(FT.)
TE ROOT AT	19.114	31.620	35.017	0.000	(FT.)
LE M.A.C. AT	10.048	27.443	27.376	0.000	(FT.)
C/4 M.A.C. AT	12.220	28.667	29.144	0.000	(FT.)
TE M.A.C. AT	18.737	32.340	34.447	0.000	(FT.)
Y M.A.C. AT	7.410	3.500	2.703	0.000	
LE TIP AT	14.414	30.748	30.635	0.000	(FT.)
C/4 TIP AT	15.360	31.388	31.383	0.000	(FT.)
TE TIP AT	18.199	33.308	33.628	0.000	(FT.)
ELEVATION	0.000	0.000	2.258	0.000	(FT.)
VOLUME COEFF		0.500	0.070	0.000	

AIRCRAFT WEIGHT = 21046.086 Lbs. AIRCRAFT VOLUME = 619.233 Cu.Ft. AIRCRAFT DENSITY = 33.987 Lbs./Cu.Ft.

1995 Light Attack Mission Performance

PHASE	M	H	CL	ALPHA	WFUEL	TIME	VEL
	SFC(I)	THRUST(I)	CD	GAMMA	W	WA	Q
	SFC(U)	THRUST(U)	CDINST	L/D	THR/THA	PR	X
CLIMB	0.82	36500.	0.3225	2.41	431.5	10.09	797.
	0.67	2316.	0.0278	1.57	20494.3	0.00	220.
	0.00	0.	0.0000	11.59	1.00	0.00	75.
CRUISE	0.80	36500.	0.3287	2.53	1230.1	65.38	774.
	0.66	1678.	0.0282	0.00	19264.2	0.00	208.
	0.00	3575.	0.0000	11.66	0.73	0.00	500.
CRUISE	0.80	100.	0.0706	0.53	410.8	5.67	893.
	0.77	5648.	0.0209	0.00	18853.4	0.00	945.
	0.00	13422.	0.0000	3.37	0.73	0.00	50.
COMBAT	0.85	100.	0.1234	0.87	173.2	2.00	949.
	0.79	6570.	0.0215	0.19	18680.2	0.00	1066.
	0.00	17106.	0.0000	5.72	0.87	0.00	19.
CRUISE	0.80	100.	0.0684	0.51	410.4	5.67	893.
	0.77	5642.	0.0209	0.00	18269.8	0.00	945.
	0.00	13414.	0.0000	3.27	0.73	0.00	50.
CLIMB	0.82	39500.	0.3263	2.44	400.4	10.30	795.
	0.66	2007.	0.0280	1.56	17869.4	0.00	190.
	0.00	0.	0.0000	11.65	1.00	0.00	76.
CRUISE	0.80	39500.	0.3310	2.55	1063.6	65.38	774.
	0.66	1459.	0.0283	0.00	16805.8	0.00	180.
	0.00	3085.	0.0000	11.70	0.73	0.00	500.
LOITER	0.30	100.	0.4426	4.52	321.3	20.00	335.
	0.71	1358.	0.0358	0.00	16484.5	0.00	133.
	0.00	2637.	0.0000	12.37	0.15	0.00	66.

### FUEL SUMMARIES

MISSION FUEL = 4562. RESERVE FUEL = 228. TRAPPED FUEL = 150.

TOTAL FUEL = 4940.

## 1995 Light Attack Maneuver Performance

	CONDITIONS	PS	NZ	TDOT	RADIUS	ALPHA	CL	CD
M= 0.85 H= 100.	1 G FLIGHT SUSTAINED MAX. INST. COMBAT ENERG	60.0 0.0 -104.6 GY = 0.7		0.00 7.46 12.48 4-04	0. 7291. 4355.	0.43 0.87 2.87	0.062 0.123 0.396	0.0208 0.0215 0.0315
M= 0.20 H= 100.	1 G FLIGHT SUSTAINED MAX. INST. COMBAT ENERG	106.7 0.0 87.9 GY = 0.6	1.00 1.50 1.50 40381E	0.00 9.28 9.28 3+03	0. 1379. 1379.	10.72 15.00 15.00	0.977 1.324 1.324	0.0939 0.1572 0.1572

## 1995 Light Attack Aerodynamics

Mach =	0.90	Altitude =	100.				
Parasite Dra Friction Body Wing Strakes H. Tail V. Tail Canard Pods Engine Cowl Boattail Interference Wave	.0113 .0038 .0053 .0000 .0012 .0010 .0000 .0000 .0000	Induced Drag Alpha Cl 0.0 0.000 2.0 0.305 3.0 0.453 4.0 0.549 5.0 0.638 6.0 0.726 8.0 0.896 10.0 1.024 12.0 1.113 15.0 1.232	Cd 0.0292 0.0357 0.0471 0.0669 0.0836 0.1035 0.1525 0.2389 0.2989 0.3993	L/D 0.0 8.5 9.6 8.2 7.6 7.0 5.9 4.3 3.7 3.1		e 0.00 1.02 0.81 0.56 0.53 0.50 0.46 0.35 0.32 0.29	
External	.0105		Slop	e Fact	ors		
Tanks Bombs Stores Extra Camber	.0000 .0000 .0000 .0059		Cl.	Alpha 1^.5Al			0.0821 0.0406
Cdmin	.0292						
)/a -1-		22.11	25000				
Mach =	0.60	Altitude =	35000.				
Parasite Dra Friction Body Wing Strakes H. Tail V. Tail Canard Pods Engine Cowl Boattail Interference Wave External	.0119 .0040 .0056 .0000 .0013 .0010 .0000 .0000 .0000 .0000 .0000 .0000 .0000 .0000	Induced Drag Alpha Cl 0.0 0.000 2.0 0.224 3.0 0.332 4.0 0.438 5.0 0.543 6.0 0.629 8.0 0.788 10.0 0.938 12.0 1.080 15.0 1.272	Cd 0.0182 0.0218 0.0261 0.0320 0.0416 0.0740 0.1141 0.1649 0.2258 0.3347	L/D 0.0 10.3 12.7 13.7 13.1 8.5 6.9 5.7 4.8 3.8	092 131	e 0.00 0.98 0.98 0.99 0.50 0.46 0.42 0.40 0.36	
Parasite Dra Friction Body Wing Strakes H. Tail V. Tail Canard Pods Engine Cowl Boattail Interference Wave	.0119 .0040 .0056 .0000 .0013 .0010 .0000 .0000 .0000 .0000	Induced Drag Alpha Cl 0.0 0.000 2.0 0.224 3.0 0.332 4.0 0.438 5.0 0.543 6.0 0.629 8.0 0.788 10.0 0.938 12.0 1.080	Cd 0.0182 0.0218 0.0261 0.0320 0.0416 0.0740 0.1141 0.1649 0.2258 0.3347	0.0 10.3 12.7 13.7 13.1 8.5 6.9 5.7 4.8 3.8	0.000 008 013 018 025 032 049 069 092 131	0.00 0.98 0.98 0.98 0.89 0.50 0.46 0.42 0.40	0.0848 0.0375

### 1995 Light Attack Propulsion

#### PHYSICAL ATTRIBUTES

ESF = 0.484 WEIGHT = 1144.911 LENGTH = 8.693 DIAM = 2.914

POWER	MACH	ALT (ft)	THRUST (lb)	SFC	FFLOW (lb/hr)	WAF (lb/sec)
100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.0 0.0 0.0 0.0 0.0 0.0	10826. 9473. 8120. 6766. 5413. 4060. 2707. 1353.	0.449 0.434 0.425 0.413 0.395 0.387 0.412 0.487	4860.9 4108.9 3452.6 2796.4 2140.1 1573.0 1116.0 659.0	239. 222. 203. 186. 172. 144. 109. 86.
100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.600 0.600 0.600 0.600 0.600 0.600 0.600	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	2808. 2457. 2106. 1755. 1404. 1053. 702. 351.	0.598 0.599 0.601 0.603 0.610 0.651 0.733 0.979	1679.4 1472.1 1264.9 1057.7 856.7 685.7 514.7 343.7	240. 226. 213. 201. 188. 168. 151.
100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.800 0.800 0.800 0.800 0.800 0.800 0.800	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	3110. 2721. 2332. 1944. 1555. 1166. 777. 389.	0.668 0.670 0.672 0.676 0.687 0.733 0.826 1.102	2077.5 1822.7 1567.9 1313.0 1068.5 855.4 642.3 428.4	240. 226. 214. 202. 190. 172. 157.
100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.900 0.900 0.900 0.900 0.900 0.900 0.900	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	3254. 2847. 2440. 2034. 1627. 1220. 813. 407.	0.723 0.728 0.734 0.742 0.760 0.820 0.941 1.302	2352.7 2071.4 1790.2 1508.9 1236.3 1000.7 765.1 529.6	240. 227. 215. 204. 192. 175. 161.

## 1995 Light Attack Weights

COMPONENT	POUNDS	KILOGRAMS	PERCENT
AIRFRAME STRUCTURE WING FUSELAGE HORIZONTAL TAIL VERTICAL TAIL ARMOR WING FOLD ALIGHTING GEAR	5980. 1900. 1867. 538. 173. 589. 150. 763.	2713. 862. 847. 244. 79. 267. 68. 346.	28.42 9.03 8.87 2.56 0.82 2.80 0.71 3.62
PROPULSION ENGINES (1) FUEL SYSTEM	1765. 1341. 424.		8.38 6.37 2.01
(COMPONENTS BELOW DO NOT HYD. + PNEU. ELECTRICAL	177. 544. 1652. 94.	FACTOR=0.85) 80. 247. 749. 43.	18.07 0.84 2.58 7.85 0.45 1.89 0.95 1.78 4.91
FUEL	4940.	2241.	23.47
PAYLOAD  FLIGHT CREW ( 1)  ARMAMENT  AMMUNITION  LASER GUIDED BOMBS  LGB PYLONS AND EJECTOR  SHORT RANGE MISSILES  SRM LAUNCHERS  EXTERNAL TANKS	4559. 180. 612. 287. 2182. 700. 398. 200. 0.	2068. 82. 278. 130. 990. 318. 181. 91.	21.66 0.86 2.91 1.36 10.37 3.33 1.89 0.95 0.00
TOTAL WEIGHT	21046.	9547.	100.00

#### 1995 Medium Attack Summary

#### Standard English Units

GENERAL	FUSELAGE		WING	HTAIL	VTAIL
TOGW 27728.	LENGTH 40.3	AREA	380.1	103.1	56.3
W/S 72.9	DIAMETER 4.5	WETTED AREA	638.6	141.6	113.0
T/W Dry 0.53	VOLUME 569.7	SPAN	40.9	19.2	7.6
CREW 1	WETTED AREA 530.0	L.E. SWEEP	23.6	35.0	47.8
N(Z) ULT 9.8	FINENESS RATIO 8.9	C/4 SWEEP	17.7	30.0	30.0
,		ASPECT RATIO	4.40	3.57	1.02
		TAPER RATIO	0.31	0.39	0.30
ENGINE	WEIGHTS	T/C ROOT	0.09	0.09	0.08
		T/C TIP	0.06	0.07	0.06
NUMBER 1	W %	ROOT CHORD	14.2	7.8	11.4
LENGTH 10.1	STRUCT. 7883. 28.4	TIP CHORD	4.4	3.0	3.4
DIAM. 3.4	PROPUL. 2409. 8.7	M.A. CHORD	10.2	5.7	8.1
WEIGHT 1562.6	FIX. EO. 3923. 14.1	LOC. OF L.E.	8.0	28.6	28.9
TSLS 14559.	FUEL 6672. 24.1				
SFCSLS 0.45	PAYLOAD 6841. 24.7				

#### MISSION SUMMARY

PHASE	MACH	ALT	FUEL	TIME	DIST	L/D	THRUST	SFC	Q
======	====	=====	=====	=====	=====	=====	======	=====	=====
TAKEOFF	0.00	0.	162.	10.5					
CLIMB	0.79	36500.	578.	10.3	74.4	11.70	3058.5	0.651	201.0
CRUISE	0.80	36500.	1683.	65.4	500.0	11.20	2296.5	0.663	208.3
CRUISE	0.80	100.	565.	5.7	50.0	3.21	7793.1	0.767	944.6
COMBAT	0.85	100.	243.	2.0	18.7	5.33	9256.3	0.787	1066.4
CRUISE	0.80	100.	564.	5.7	50.0	3.11	7785.1	0.767	944.6
CLIMB	0.78	39500.	533.	10.4	75.4	11.76	2650.1	0.645	171.7
CRUISE	0.80	39500.	1451.	65.4	500.0	11.21	1990.5	0.660	180.4
LOITER	0.30	100.	433.	20.0	66.1	11.96	1835.3	0.708	132.8

BLOCK TIME = 3.082 HR BLOCK RANGE = 1334.9 NM

#### COMBAT PHASES

MACH	ALT	PS1G	NZS	CLS	CDS	ALS	NZI	PSI	CLI	CDI	ALI	CBE
0.85	100.	45.	3.5	0.122	0.0228	0.9	6.5	-127.	0.390	0.0331	3.0	5421.
0.20	100.	110	1 5	1.291	0.1544	15.0	1.5	92.	1.291	0.1544	15.0	661.

#### 1995 Medium Attack Geometry

```
WING H.TAIL V.TAIL CANARD UNITS
                    380.1
                            103.1
                                   56.3
PLAN AREA.....
                                             0.0 (SO.FT.)
                    638.6
                            141.6
                                    113.0
                                             0.0 (SQ.FT.)
SURFACE AREA.....
                                             0.0 (CU.FT.)
VOLUME.....
                    187.2
                            34.2
                                    23.9
SPAN....
                   40.879
                           19.196
                                   7.581
                                           0.000 (FT.)
                   23.637
                           35.042
                                  40.035
                                           0.000 (DEG.)
L.E. SWEEP.....
C/4 SWEEP.....
                   17.661
                           30.000
                                  30.000
                                           0.000 (DEG.)
T.E. SWEEP.....
                   -2.259
                           11.612 -11.916
                                           0.000 (DEG.)
ASPECT RATIO .....
                   4.396
                            3.574
                                   1.020
                                           0.000
                   14.174
                                  11.417
ROOT CHORD.....
                            7.750
                                           0.000 (FT.)
ROOT THICKNESS.....
                   15.308
                            8.370
                                   10.823
                                           0.000 (IN.)
                   0.090
ROOT T/C .....
                            0.090
                                    0.079
                                           0.000
                   4.422
                                           0.000 (FT.)
TIP CHORD.....
                            2.992
                                    3.448
TIP THICKNESS.....
                  3.184
                           2.513
                                   2.689
                                           0.000 (IN.)
TIP T/C .....
                  0.060
                           0.070
                                   0.065
                                           0.000
                   0.312
                           0.386
                                   0.302
                                           0.000
TAPER RATIO .....
MEAN AERO CHORD....
                   10.151
                           5.722
                                   8.144
                                           0.000 (FT.)
LE ROOT AT.....
                    7.974
                           28.616
                                  28.856
                                           0.000 (FT.)
                                           0.000 (FT.)
                   11.518
                           30.554
                                   31.710
C/4 ROOT AT....
TE ROOT AT.....
                    22.149
                           36.367
                                  40.273
                                           0.000 (FT.)
LE M.A.C. AT.....
                    11.666
                           31.485
                                   31.472
                                           0.000 (FT.)
C/4 M.A.C. AT.....
                   14.203
                           32.915
                                   33.508
                                           0.000 (FT.)
TE M.A.C. AT.....
                   21.816
                           37.207
                                   39.616
                                           0.000 (FT.)
                   8.433
                           4.090
                                   3.113
                                           0.000
Y M.A.C. AT.....
LE TIP AT....
                   16.920
                           35.347
                                   35.225
                                           0.000 (FT.)
C/4 TIP AT....
                   18.026
                           36.095
                                   36.087
                                           0.000 (FT.)
                    21.343
                           38.339
                                   38.673
                                           0.000 (FT.)
TE TIP AT....
ELEVATION.....
                    0.000
                           0.000
                                    2.263
                                           0.000 (FT.)
VOLUME COEFF. ....
                            0.500
                                    0.070
                                           0.000
```

AIRCRAFT WEIGHT = 27726.607 Lbs. AIRCRAFT VOLUME = 814.984 Cu.Ft. AIRCRAFT DENSITY = 34.021 Lbs./Cu.Ft.

1995 Medium Attack Mission Performance

PHASE	M	H	CL	ALPHA	WFUEL	TIME	VEL
	SFC(I)	THRUST(I)	CD	GAMMA	W	WA	Q
	SFC(U)	THRUST(U)	CDINST	L/D	THR/THA	PR	X
CLIMB	0.79	36500.	0.3590	2.95	577.7	10.29	761.
	0.65	3059.	0.0307	1.51	26987.1	0.00	201.
	0.00	0.	0.0000	11.70	1.00	0.00	74.
CRUISE	0.80	36500.	0.3249	2.62	1683.0	65.38	774.
	0.66	2296.	0.0290	0.00	25304.1	0.00	208.
	0.00	4862.	0.0000	11.20	0.75	0.00	500.
CRUISE	0.80	100.	0.0697	0.55	564.8	5.67	893.
	0.77	7793.	0.0217	0.00	24739.3	0.00	945.
	0.00	18333.	0.0000	3.21	0.75	0.00	50.
COMBAT	0.85	100.	0.1217	0.91	242.7	2.00	949.
	0.79	9256.	0.0228	0.13	24496.6	0.00	1066.
	0.00	23003.	0.0000	5.33	0.92	0.00	19.
CRUISE	0.80	100.	0.0674	0.53	564.3	5.67	893.
	0.77	7785.	0.0217	0.00	23932.3	0.00	945.
	0.00	18322.	0.0000	3.11	0.74	0.00	50.
CLIMB	0.78	39500.	0.3642	3.01	533.2	10.42	756.
	0.64	2650.	0.0310	1.54	23399.1	0.00	172.
	0.00	0.	0.0000	11.76	1.00	0.00	75.
CRUISE	0.80	39500.	0.3253	2.62	1450.7	65.38	774.
	0.66	1991.	0.0290	0.00	21948.4	0.00	180.
	0.00	4189.	0.0000	11.21	0.74	0.00	500.
LOITER	0.30	100.	0.4347	4.62	433.3	20.00	335.
	0.71	1835.	0.0363	0.00	21515.0	0.00	133.
	0.00	3557.	0.0000	11.96	0.15	0.00	66.

### FUEL SUMMARIES

MISSION FUEL = .6212. RESERVE FUEL = .311. TRAPPED FUEL = .150.

TOTAL FUEL = 6672.

## 1995 Medium Attack Maneuver Performance

	CONDITIONS	PS	NŽ	TDOT	RADIUS	ALPHA	CL	CD
M= 0.85 H= 100.	1 G FLIGHT SUSTAINED MAX. INST. COMBAT ENERG	-126.7	3.45 6.50		0. 8462. 4355.	0.45 0.91 2.97	0.061 0.122 0.390	0.0220 0.0228 0.0331
	COMBAT ENERC	3Y = 0.5	4211/6	+04				
M = 0.20 H = 100.	1 G FLIGHT SUSTAINED	110.2	1.00 1.50	0.00 9.23	0. 1386.	10.85 15.00	0.959 1.291	0.0938 0.1544
11- 100:	MAX. INST.		1.50	9.23	1386.	15.00	1.291	0.1544
	COMBAT ENERO	3Y = 0.6	61418E	+03				

# 1995 Medium Attack Aerodynamics

Mach =	0.90	Altit	ude =	100.				
Parasite Drag Friction Body Wing Strakes H. Tail V. Tail Canard Pods Engine Cowl Boattail Interference Wave	.0109 .0033 .0053 .0000 .0013 .0010 .0000 .0000 .0000 .0000 .0000	2.0 3.0 4.0 5.0 6.0 8.0 10.0	C1 0.000 0.289 0.430 0.524 0.612 0.698 0.864 1.005	Cd 0.0329 0.0388 0.0494 0.0684 0.0845 0.1037 0.1512 0.2404 0.2996 0.3990	L/D 0.0 7.4 8.7 7.7 7.2 6.7 5.7 4.2 3.6 3.0		e 0.00 1.01 0.81 0.56 0.52 0.50 0.46 0.35 0.32 0.29	
External	.0121				e Fact Alpha	ors		0.0808
Tanks Bombs Stores Extra Camber	.0000 .0061 .0000 .0060				l^.5Al	pha		0.0403
Cdmin	.0329							
Mach =	0.60	Altit	ude =	35000.				
Parasite Drag Friction Body Wing Strakes H. Tail V. Tail Canard Pods Engine Cowl Boattail Interference	.0114 .0035 .0056 .0000 .0013 .0010 .0000 .0000 .0000 .0000	Induced D. Alpha 0.0 2.0 3.0 4.0 5.0 6.0 8.0 10.0 12.0		35000.  Cd 0.0216 0.0250 0.0291 0.0348 0.0433 0.0752 0.1142 0.1638 0.2235 0.3306	L/D 0.0 8.6 10.9 12.1 12.0 8.1 6.7 5.6 4.7 3.8	Cm 0.000 008 013 019 026 033 051 071 094 135	e 0.00 0.98 0.98 0.99 0.50 0.45 0.42 0.40 0.36	
Parasite Drag Friction Body Wing Strakes H. Tail V. Tail Canard Pods Engine Cowl Boattail	.0114 .0035 .0056 .0000 .0013 .0010 .0000 .0000 .0000	Induced D. Alpha 0.0 2.0 3.0 4.0 5.0 6.0 8.0 10.0 12.0	0.000 0.214 0.319 0.421 0.522 0.606 0.762 0.911 1.050	Cd 0.0216 0.0250 0.0291 0.0348 0.0433 0.0752 0.1142 0.1638 0.2235 0.3306	0.0 8.6 10.9 12.1 12.0 8.1 6.7 5.6 4.7	0.000 008 013 019 026 033 051 071 094 135	0.00 0.98 0.98 0.99 0.91 0.50 0.45 0.42 0.40	0.0828 0.0371

## 1995 Medium Attack Propulsion

### PHYSICAL ATTRIBUTES

ESF = 0.650 WEIGHT = 1562.604 LENGTH = 10.080 DIAM = 3.379

POWER	MACH	ALT (ft)	THRUST (lb)	SFC	FFLOW (lb/hr)	WAF (lb/sec)
100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.0 0.0 0.0 0.0 0.0 0.0	14559. 12739. 10919. 9099. 7279. 5459. 3640. 1820.	0.449 0.434 0.425 0.413 0.395 0.387 0.412 0.487	6536.8 5525.5 4643.0 3760.5 2878.0 2115.3 1500.7 886.2	322. 298. 273. 251. 231. 193. 147. 115.
100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.600 0.600 0.600 0.600 0.600 0.600	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	3776. 3304. 2832. 2360. 1888. 1416. 944. 472.	0.598 0.599 0.601 0.603 0.610 0.651 0.733 0.979	2258.4 1979.7 1701.0 1422.3 1152.0 922.1 692.2 462.1	323. 304. 286. 270. 253. 226. 202. 181.
100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.800 0.800 0.800 0.800 0.800 0.800 0.800	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	4182. 3659. 3137. 2614. 2091. 1568. 1046. 523.	0.668 0.670 0.672 0.676 0.687 0.733 0.826 1.102	2793.8 2451.1 2108.4 1765.7 1436.8 1150.3 863.7 576.1	323. 304. 288. 272. 255. 232. 212. 179.
100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.900 0.900 0.900 0.900 0.900 0.900 0.900	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	4375. 3828. 3282. 2735. 2188. 1641. 1094. 547.	0.723 0.728 0.734 0.742 0.760 0.820 0.941 1.302	3163.8 2785.6 2407.4 2029.2 1662.5 1345.7 1028.9 712.1	323. 305. 289. 274. 258. 236. 216. 199.

## 1995 Medium Attack Weights

COMPONENT	POUNDS	KILOGRAMS	PERCENT
FUSELAGE HORIZONTAL TAIL VERTICAL TAIL ARMOR WING FOLD	2667.	1210. 1093. 371.	9.62 8.69
	2409. 1830. 579.	1093. 830. 262.	6.60
FIXED EQUIPMENT  (COMPONENTS BELOW DO NOT  HYD. + PNEU.  ELECTRICAL  AVIONICS  INSTRUMENTATION  DE-ICE/AIR CONDITION  AUXILIARY GEAR  FURNISH. + EQPT.  FLIGHT CONTROLS	233. 544	106. 247. 749. 43. 181.	0.84 1.96 5.96 0.34 1.44
FUEL	6672.	3027.	24.06
PAYLOAD  FLIGHT CREW ( 1)  ARMAMENT  AMMUNITION  SHORT RANGE MISSILES  SRM LAUNCHERS  LASER GUIDED BOMBS  LGB PYLONS AND EJECTORS  EXTERNAL TANKS	287. 398. 200. 4364.	82. 278. 130. 181. 91. 1980.	24.67 0.65 2.21 1.04 1.44 0.72 15.74 2.89 0.00
TOTAL WEIGHT	27728.	12577.	100.00

## 1995 Medium All Weather Attack Summary

## Standard English Units

GENERAL	FUSELAGE		WING	HTAIL	VTAIL
TOGW 31072. W/S 73.8	LENGTH 44.3 DIAMETER 4.6	AREA WETTED AREA	420.8 720.5	97.2 131.1	61.2 122.7
T/W 0.50 CREW 2	VOLUME 650.7 WETTED AREA 594.7	SPAN L.E. SWEEP	$\frac{46.1}{19.5}$	18.6 35.0	7.9 47.8
N(Z) ULT 9.8	FINENESS RATIO 9.7	C/4 SWEEP	14.1	30.0	30.0
		ASPECT RATIO	5.05	3.57	1.02
ENGINE	WEIGHTS	TAPER RATIO T/C ROOT T/C TIP	0.31 0.09 0.06	0.39 0.09 0.07	0.30 0.08 0.06
NUMBER 1	W %	ROOT CHORD	13.9	7.5	11.9
LENGTH 10.4	STRUCT. 8906. 28.7	TIP CHORD	4.3	2.9	3.6
DIAM. 3.5	PROPUL. 2588. 8.3	M.A. CHORD	10.0	5.6	8.5
WEIGHT 1679.2 TSLS 15591. SFCSLS 0.45	FIX. EQ. 5521. 17.8 FUEL 7036. 22.6 PAYLOAD 7021. 22.6	LOC. OF L.E.	9.2	32.5	32.4

### MISSION SUMMARY

PHASE	MACH	ALT	FUEL	TIME	DIST	L/D	THRUST	SFC	Q
======	====	=====	=====	=====	=====	=====	======	=====	=====
TAKEOFF	0.00	0.	173.	10.5					
CLIMB	0.79	36500.	627.	10.2	75.1	12.58	3284.5	0.653	203.8
CRUISE	0.80	36500.	1750.	65.4	500.0	12.12	2389.0	0.664	208.3
CRUISE	0.80	100.	595.	5.7	50.0	3.44	8195.9	0.769	944.6
COMBAT	0.85	100.	257.	2.0	18.7	5.69	9795.7	0.787	1066.4
CRUISE	0.80	100.	595.	5.7	50.0	3.34	8188.3	0.769	944.6
CLIMB	0.79	39500.	586.	10.5	76.7	12.61	2855.5	0.650	177.4
CRUISE	0.80	39500.	1516.	65.4	500.0	12.18	2080.6	0.660	180.4
LOITER	0.30	100.	457.	20.0	66.1	13.01	1919.3	0.715	132.8

BLOCK TIME = 3.083 HR BLOCK RANGE = 1336.9 NM

### COMBAT PHASES

MACH	ALT	PS1G	NZS	CLS	CDS	ALS	NZI	PSI	CLI	CDI	ALI	CBE
0.85	100.	46.	3.7	0.124	0.0218	0.9	6.5	-104.	0.398	0.0309	2.9	5542.
0.20	100.	104.	1.5	1.341	0.1471	15.0	1.5	87.	1.341	0.1471	15.0	625.

#### 1995 Medium All Weather Attack Geometry

```
WING H.TAIL V.TAIL CANARD UNITS
                            97.2
                                            0.0 (SQ.FT.)
PLAN AREA.....
                    420.8
                                   61.2
                    720.5
                           131.1
                                   122.7
SURFACE AREA....
                                            0.0 (SO.FT.)
                  206.6
VOLUME....
                           31.3
                                   27.0
                                            0.0 (CU.FT.)
18.635
                                   7.899
                                          0.000 (FT.)
L.E. SWEEP..... 19.532
                          35.042
                                 40.035
                                          0.000 (DEG.)
C/4 SWEEP.....
                  14.080
                          30.000
                                 30.000
                                          0.000 (DEG.)
                  -3.491
                          11.612 -11.916
T.E. SWEEP.....
                                          0.000 (DEG.)
                   5.045
ASPECT RATIO .....
                           3.574
                                  1.020
                                          0.000
                   13.921
                           7.524
                                          0.000 (FT.)
ROOT CHORD.....
                                  11.896
ROOT THICKNESS..... 15.035
                                  11.278
                                          0.000 (IN.)
                           8.126
ROOT T/C ..... 0.090
                          0.090
                                  0.079
                                          0.000
                  4.343
                           2.904
                                   3.593
                                          0.000 (FT.)
TIP CHORD.....
TIP THICKNESS.....
                                   2.802
                  3.127
                           2.440
                                          0.000 (IN.)
TIP T/C .....
                  0.060
                          0.070
                                   0.065
                                          0.000
TAPER RATIO .....
                           0.386
                  0.312
                                   0.302
                                          0.000
MEAN AERO CHORD....
                  9.969
                           5.555
                                  8.486
                                          0.000 (FT.)
                  9.183
LE ROOT AT.....
                          32.459
                                  32.382
                                          0.000 (FT.)
C/4 ROOT AT.....
                   12.664
                          34.340
                                  35.356
                                          0.000 (FT.)
TE ROOT AT..... 23.104
                          39.983
                                 44.278
                                          0.000 (FT.)
LE M.A.C. AT..... 12.555
                          35.244
                                  35.107
                                          0.000 (FT.)
C/4 M.A.C. AT.....
                  15.047
                          36.633
                                 37.229
                                          0.000 (FT.)
TE M.A.C. AT..... 22.524
                          40.799
                                 43.593
                                          0.000 (FT.)
Y M.A.C. AT....
                   9.505
                          3.971
                                  3.244
                                          0.000
LE TIP AT.....
                   17.356
                          38.994
                                  39.018
                                          0.000 (FT.)
C/4 TIP AT.....
                  18.441
                          39.720
                                  39.916
                                          0.000 (FT.)
TE TIP AT.....
                   21.699
                          41.898
                                  42.611
                                          0.000 (FT.)
ELEVATION.....
                   0.000
                           0.000
                                   2.288
                                          0.000 (FT.)
VOLUME COEFF. ....
                           0.500
                                   0.070
                                          0.000
```

AIRCRAFT WEIGHT = 31072.084 Lbs. AIRCRAFT VOLUME = 915.601 Cu.Ft. AIRCRAFT DENSITY = 33.936 Lbs./Cu.Ft.

1995 Medium All Weather Attack Mission Performance

PHASE	M	H	CL	ALPHA	WFUEL	TIME	VEL
	SFC(I)	THRUST(I)	CD	GAMMA	W	WA	Q
	SFC(U)	THRUST(U)	CDINST	L/D	THR/THA	PR	X
CLIMB	0.79	36500.	0.3585	2.77	627.5	10.25	766.
	0.65	3284.	0.0285	1.59	30271.3	0.00	204.
	0.00	0.	0.0000	12.58	1.00	0.00	75.
CRUISE	0.80	36500.	0.3304	2.52	1750.5	65.38	774.
	0.66	2389.	0.0273	0.00	28520.8	0.00	208.
	0.00	5111.	0.0000	12.12	0.72	0.00	500.
CRUISE	0.80	100.	0.0710	0.53	595.5	5.67	893.
	0.77	8196.	0.0206	0.00	27925.3	0.00	945.
	0.00	19419.	0.0000	3.44	0.73	0.00	50.
COMBAT	0.85 0.79 0.00		0.1241 0.0218 0.0000	0.87 0.14 5.69	257.1 27668.3 0.90	2.00 0.00 0.00	949. 1066. 19.
CRUISE	0.80	100.	0.0689	0.52	595.0	5.67	893.
	0.77	8188.	0.0206	0.00	27073.3	0.00	945.
	0.00	19408.	0.0000	3.34	0.73	0.00	50.
CLIMB	0.79	39500.	0.3603	2.78	585.7	10.52	768.
	0.65	2855.	0.0286	1.56	26487.6	0.00	177.
	0.00	0.	0.0000	12.61	1.00	0.00	77.
CRUISE	0.80	39500.	0.3340	2.55	1515.9	65.38	774.
	0.66	2081.	0.0274	0.00	24971.6	0.00	180.
	0.00	4416.	0.0000	12.18	0.73	0.00	500.
LOITER	0.30	100.	0.4468	4.57	457.5	20.00	335.
	0.72	1919.	0.0343	0.00	24514.2	0.00	133.
	0.00	3751.	0.0000	13.01	0.15	0.00	66.

### FUEL SUMMARIES

MISSION FUEL = 6558.
RESERVE FUEL = 328.
TRAPPED FUEL = 150.

TOTAL FUEL = 7036.

## 1995 Medium All Weather Attack Maneuver Performance

	CONDITIONS	PS	NZ	TDOT	RADIUS	ALPHA	CL	CD
M= 0.85 H= 100.	1 G FLIGHT SUSTAINED MAX. INST. COMBAT ENERG	0.0 -103.7			0. 7923. 4355.	0.43 0.87 2.85	0.062 0.124 0.398	0.0211 0.0218 0.0309
M= 0.20 H= 100.	1 G FLIGHT SUSTAINED MAX. INST. COMBAT ENERG	104.2 0.0 86.6 GY = 0.6	1.50	0.00 9.27 9.27 403	0. 1380. 1380.	10.74 15.00 15.00	0.987 1.341 1.341	0.0882 0.1471 0.1471

# 1995 Medium All Weather Attack Aerodynamics

Mach =	0.90	Altitude :	100.				
Parasite Dra Friction Body Wing Strakes H. Tail V. Tail Canard Pods Engine Cowl Boattail Interference Wave External	.0107 .0033 .0054 .0000 .0011 .0009 .0000 .0000 .0000	Induced Drag Alpha C. 0.0 0.000 2.0 0.310 3.0 0.460 4.0 0.550 5.0 0.650 6.0 0.74 8.0 0.91 10.0 1.020 12.0 1.11 15.0 1.230	0.0291 0.0351 0.0465 0.0659 0.0826 0.1025 0.1517 0.2336 0.2933 0.3936	4.4 3.8	126 177	e 0.00 1.01 0.77 0.53 0.50 0.47 0.43 0.32 0.29 0.26	
Tanks	.0000		C]	LAlpha 11^.5Al			0.0821 0.0403
Bombs Stores Extra Camber	.0000 .0000 .0054 .0000			II .SAI	.pna		0.0403
Cdmin	.0291						
Mach =	0.60	Altitude	35000.				
Parasite Dra Friction Body Wing Strakes H. Tail V. Tail Canard Pods Engine Cowl Boattail Interference	.0113 .0035 .0057 .0000 .0011 .0010 .0000 .0000 .0000 .0000	Altitude  Induced Drag Alpha C 0.0 0.00 2.0 0.22 3.0 0.33 4.0 0.43 5.0 0.54 6.0 0.63 8.0 0.79 10.0 0.95 12.0 1.09 15.0 1.29	Cd 0.0169 0.0201 0.0221 0.0295 0.0396 0.0708 0.1106 0.1613 0.2224	0.0 11.1 13.8 14.9 13.8 8.9 7.2 5.9 4.9		e 0.00 0.97 0.96 0.82 0.47 0.43 0.39 0.37	
Parasite Dra Friction Body Wing Strakes H. Tail V. Tail Canard Pods Engine Cowl Boattail	.0113 .0035 .0057 .0000 .0011 .0010 .0000 .0000	Induced Drag Alpha C 0.0 0.00 2.0 0.22 3.0 0.33 4.0 0.43 5.0 0.54 6.0 0.63 8.0 0.79 10.0 0.95 12.0 1.09	Cd 0.0169 0.0201 0.0241 0.0295 0.0396 0.0708 0.1106 0.1613 0.2224 0.3322	0.0 11.1 13.8 14.9 13.8 8.9 7.2 5.9 4.9	0.000 011 018 025 033 042 062 084 109 152	0.00 0.97 0.97 0.96 0.82 0.47 0.43 0.39	0.0863

## 1995 Medium All Weather Attack Propulsion

### PHYSICAL ATTRIBUTES

ESF = 0.696 WEIGHT = 1679.187 LENGTH = 10.432 DIAM = 3.497

POWER	MACH	ALT (ft)	THRUST (lb)	SFC	FFLOW (lb/hr)	WAF (lb/sec)
100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.000 0.000 0.000 0.000 0.000 0.000	0.0 0.0 0.0 0.0 0.0 0.0	15591. 13642. 11693. 9744. 7796. 5847. 3898. 1949.	0.449 0.434 0.425 0.413 0.395 0.387 0.412 0.487	7000.4 5917.4 4972.3 4027.2 3082.1 2265.3 1607.2 949.0	345. 319. 292. 268. 247. 207. 157. 123.
100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.600 0.600 0.600 0.600 0.600 0.600	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	4044. 3539. 3033. 2528. 2022. 1517. 1011. 506.	0.598 0.599 0.601 0.603 0.610 0.651 0.733 0.979	2418.6 2120.1 1821.6 1523.2 1233.8 987.5 741.3 494.9	345. 325. 307. 290. 271. 242. 217. 194.
100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.800 0.800 0.800 0.800 0.800 0.800 0.800	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	4479. 3919. 3359. 2799. 2239. 1680. 1120. 560.	0.668 0.670 0.672 0.676 0.687 0.733 0.826 1.102	2992.0 2625.0 2258.0 1890.9 1538.8 1231.9 925.0 616.9	345. 326. 308. 292. 273. 248. 227. 191.
100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.900 0.900 0.900 0.900 0.900 0.900 0.900	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	4686. 4100. 3514. 2929. 2343. 1757. 1171. 586.	0.723 0.728 0.734 0.742 0.760 0.820 0.941 1.302	3388.2 2983.2 2578.1 2173.1 1780.5 1441.2 1101.9 762.7	345. 327. 309. 293. 276. 253. 232. 213.

1995 Medium All Weather Attack Weights

COMPONENT	POUNDS	KILOGRAMS	PERCENT
AIRFRAME STRUCTURE WING FUSELAGE HORIZONTAL TAIL VERTICAL TAIL ARMOR WING FOLD ALIGHTING GEAR	8906. 3228. 2788. 757. 269. 589. 150.	4040. 1464. 1265. 343. 122. 267. 68. 511.	10.39
PROPULSION ENGINES (1) FUEL SYSTEM	2588. 1966. 622.		8.33 6.33 2.00
FIXED EQUIPMENT  (COMPONENTS BELOW DO NOT HYD. + PNEU. ELECTRICAL AVIONICS INSTRUMENTATION DE-ICE/AIR CONDITION AUXILIARY GEAR FURNISH. + EQPT. FLIGHT CONTROLS	261. 817. 2790. 219.	118. 370. 1266. 99.	0.84 2.63 8.98 0.70
FUEL	7036.	3191.	22.64
PAYLOAD  FLIGHT CREW ( 2)  ARMAMENT  AMMUNITION  LASER GUIDED BOMBS  LGB PYLONS AND EJECTORS  SHORT RANGE MISSILES  SRM LAUNCHERS  EXTERNAL TANKS	612. 287. 4364. 800.	3185. 163. 278. 130. 1980. 363. 181. 91. 0.	
TOTAL WEIGHT	31072.	14094.	100.00

## 1995 Medium Flying Wing Attack Summary

### Standard English Units

GENE	RAL	FUS	ELAGE			WING	HTAIL	VTAIL
TOGW W/S T/W Dry CREW N(Z) UL	2	LENGTH DIAMETER VOLUME WETTED AR FINENESS		22.5 4.5 289.1 282.4 5.0	AREA WETTED AREA SPAN L.E. SWEEP C/4 SWEEP ASPECT RATIO TAPER RATIO	751.6 1259.6 51.3 47.7 39.1 3.50	0.0 0.0 0.2 35.0 30.0 3.57	0.0 0.0 0.1 47.8 30.0 1.02 0.30
ENGI	NE	WEI	GHTS		T/C ROOT T/C TIP	0.15	0.09	0.08
NUMBER LENGTH DIAM. WEIGHT TSLS SFCSLS	1 7.9 2.7 940.7 8978. 0.45	STRUCT. PROPUL. FIX. EQ. FUEL PAYLOAD	W 7720. 1450. 5359. 4127. 6421.	5.8 21.4 16.5	ROOT CHORD TIP CHORD M.A. CHORD LOC. OF L.E.	29.3 0.0 19.5 0.1	0.1 0.0 0.0 20.2	0.1 0.0 0.1 22.3

#### MISSION SUMMARY

PHASE	MACH	ALT	FUEL	TIME	DIST	L/D	THRUST	SFC	Q
======	====	=====	=====	=====	=====	=====	======	=====	=====
TAKEOFF	0.00	0.	100.	10.5					
CLIMB	0.84	33112.	409.	9.6	74.9	16.92	2271.9	0.683	271.5
CRUISE	0.80	33112.	991.	64.5	500.0	17.55	1357.3	0.675	244.5
CRUISE	0.80	100.	312.	5.7	50.0	5.55	4221.6	0.781	944.6
COMBAT	0.85	100.	133.	2.0	18.7	9.35	4973.1	0.802	1066.4
CRUISE	0.80	100.	312.	5.7	50.0	5.45	4219.0	0.781	944.6
CLIMB	0.84	39425.	465.	13.3	104.9	18.98	1685.9	0.674	200.4
CRUISE	0.80	39425.	812.	65.4	500.0	19.52	1114.0	0.663	181.0
LOITER	0.30	100.	255.	20.0	66.1	20.54	1048.8	0.730	132.8

BLOCK TIME = 3.103 HR BLOCK RANGE = 1364.9 NM

### COMBAT PHASES

MACH	ALT	PS1G	NZS	CLS	CDS	ALS	NZI	PSI	CLI	CDI	ALI	CBE
0.85	100.	59.	4.9	0.058	0.0062	0.7	6.5	-43.	0.187	0.0091	2.4	7080.
0.20	100.	70.	1.9	0.885	0.0786	15.0	1.9	43.	0.885	0.0786	15.0	417.

### 1995 Medium Flying Wing Geometry

	WING	H.TAIL	V.TAIL	CANARD	UNITS
PLAN AREA	751.6	0.0	0.0	0.0	(SQ.FT.)
SURFACE AREA	1259.6	0.0	0.0	0.0	(SQ.FT.)
VOLUME	967.1	0.0	0.0	0.0	(CU.FT.)
SPAN	51.288	0.164	0.088	0.000	(FT.)
L.E. SWEEP	47.667	35.042	40.035	0.000	(DEG.)
C/4 SWEEP	39.096	30.000	30.000	0.000	(DEG.)
T.E. SWEEP	-2.454	11.612	-11.916	0.000	(DEG.)
ASPECT RATIO	3.500	3.574	1.020	0.000	
ROOT CHORD	29.278	0.066	0.132	0.000	(FT.)
ROOT THICKNESS	52.701	0.071	0.125	0.000	(IN.)
ROOT T/C	0.150	0.090	0.079	0.000	
TIP CHORD	0.029	0.026	0.040	0.000	(FT.)
TIP THICKNESS	0.000	0.021	0.031	0.000	(IN.)
TIP T/C	0.001	0.070	0.065	0.000	
TAPER RATIO	0.001	0.386	0.302	0.000	
MEAN AERO CHORD	19.519	0.049	0.094	0.000	(FT.)
LE ROOT AT	0.093	20.218	22.331	0.000	(FT.)
C/4 ROOT AT	7.413	20.234	22.364	0.000	(FT.)
TE ROOT AT	29.371	20.284	22.463	0.000	(FT.)
LE M.A.C. AT	9.486	20.242	22.361	0.000	(FT.)
C/4 M.A.C. AT	14.366	20.255	22.385	0.000	(FT.)
TE M.A.C. AT	29.005	20.291	22.455	0.000	(FT.)
Y M.A.C. AT	8.557	0.035	0.036	0.000	
LE TIP AT	28.243	20.275	22.405	0.000	(FT.)
C/4 TIP AT	28.250	20.282	22.415	0.000	(FT.)
TE TIP AT	28.272	20.301	22.445	0.000	(FT.)
ELEVATION	-0.450	0.000	2.250	0.000	(FT.)
VOLUME COEFF		0.000	0.000	0.000	

AIRCRAFT WEIGHT = 25078.863 Lbs. AIRCRAFT VOLUME = 1256.204 Cu.Ft. AIRCRAFT DENSITY = 19.964 Lbs./Cu.Ft.

1995 Medium Flying Wing Mission Performance

PHASE	M	H	CL	ALPHA	WFUEL	TIME	VEL
	SFC(I)	THRUST(I)	CD	GAMMA	W	WA	Q
	SFC(U)	THRUST(U)	CDINST	L/D	THR/THA	PR	X
CLIMB	0.84	33112.	0.1207	1.56	409.0	9.59	827.
	0.68	2272.	0.0071	1.90	24570.1	0.00	272.
	0.00	0.	0.0000	16.92	1.00	0.00	75.
CRUISE	0.80	33112.	0.1297	1.72	991.1	64.49	785.
	0.67	1357.	0.0074	0.00	23579.0	0.00	244.
	0.00	3103.	0.0000	17.55	0.61	0.00	500.
CRUISE	0.80	100.	0.0330	0.43	311.7	5.67	893.
	0.78	4222.	0.0059	0.00	23267.3	0.00	945.
	0.00	10469.	0.0000	5.55	0.65	0.00	50.
COMBAT	0.85	100.	0.0580	0.74	132.9	2.00	949.
	0.80	4973.	0.0062	0.30	23134.4	0.00	1066.
	0.00	14186.	0.0000	9.35	0.80	0.00	19.
CRUISE	0.80	100.	0.0324	0.42	311.5	5.67	893.
	0.78	4219.	0.0059	0.00	22822.9	0.00	945.
	0.00	10465.	0.0000	5.45	0.65	0.00	50.
CLIMB	0.84	39425.	0.1483	1.93	465.1	13.29	815.
	0.67	1686.	0.0078	1.30	22357.8	0.00	200.
	0.00	0.	0.0000	18.98	1.00	0.00	105.
CRUISE	0.80	39425.	0.1598	2.13	811.6	65.38	774.
	0.66	1114.	0.0082	0.00	21546.2	0.00	181.
	0.00	2432.	0.0000	19.52	0.67	0.00	500.
LOITER	0.30	100.	0.2158	3.36	255.4	20.00	335.
	0.73	1049.	0.0105	0.00	21290.9	0.00	133.
	0.00	2088.	0.0000	20.54	0.14	0.00	66.

## FUEL SUMMARIES

MISSION FUEL = 3788. RESERVE FUEL = 189. TRAPPED FUEL = 150.

TOTAL FUEL = 4127.

## 1995 Medium Flying Wing Maneuver Performance

	CONDITIONS	PS	NZ	TDOT	RADIUS	ALPHA	CL	CD
M= 0.85 H= 100.	1 G FLIGHT SUSTAINED MAX. INST. COMBAT ENERGY	59.0 0.0 -43.0 Y = 0.7		0.00 9.42 12.48 +04	0. 5770. 4355.	0.37 0.74 2.43	0.029 0.058 0.187	0.0060 0.0062 0.0091
M= 0.20 H= 100.	1 G FLIGHT SUSTAINED MAX. INST. COMBAT ENERGY	0.0 42.9	1.00 1.94 1.94 17195E	0.00 13.74 13.74 +03	0. 931. 931.	7.81 15.00 15.00	0.480 0.885 0.885	0.0275 0.0786 0.0786

# 1995 Medium Flying Wing Aerodynamics

Mach =	0.90	Altitude =	100.				
Parasite Drag Friction Body Wing Strakes H. Tail V. Tail Canard Pods Engine Cowl Boattail Interference Wave	.0057 .0011 .0046 .0000 .0000 .0000 .0000 .0000 .0000 .0000	Induced Drag Alpha Cl 0.0 0.000 2.0 0.159 3.0 0.237 4.0 0.313 5.0 0.388 6.0 0.462 8.0 0.573 10.0 0.674 12.0 0.755 15.0 0.821	0.0147 0.0175 0.0213 0.0261 0.0330 0.0828 0.1187 0.2086 0.2762	3.6 3.0	Cm 0.000 0.003 0.004 0.006 0.007 0.009 0.011 0.013 0.034 0.037	e 0.00 1.00 1.00 1.00 0.94 0.42 0.39 0.26 0.23	
External Tanks	.0000		Cl	e Fact Alpha			0.0547
Bombs Stores	.0000		Cc	l1^.5A1	pha		0.0342
Extra Camber	.0000			•			
Cdmin	.0124						
Mach =	0.60	Altitude =	35000.				
Parasite Drag Friction Body Wing Strakes H. Tail V. Tail Canard Pods Engine Cowl Boattail Interference	.0060 .0011 .0049 .0000 .0000 .0000 .0000 .0000 .0000 .0000	Altitude =  Induced Drag Alpha Cl 0.0 0.000 2.0 0.139 3.0 0.206 4.0 0.272 5.0 0.338 6.0 0.402 8.0 0.528 10.0 0.651 12.0 0.746 15.0 0.861	Cd 0.0060 0.0078 0.0099 0.0128 0.0165 0.0209 0.0317 0.0450 0.1422	L/D 0.0 17.8 20.8 21.2 20.5 19.3 16.7 14.5 5.2 4.1	Cm 0.000 0.007 0.010 0.013 0.017 0.020 0.027 0.033 0.037 0.044	e 0.00 0.99 0.99 0.99 0.99 0.99 0.37 0.33	
Parasite Drag Friction Body Wing Strakes H. Tail V. Tail Canard Pods Engine Cowl Boattail	.0060 .0011 .0049 .0000 .0000 .0000 .0000 .0000	Induced Drag Alpha Cl 0.0 0.000 2.0 0.139 3.0 0.206 4.0 0.272 5.0 0.338 6.0 0.402 8.0 0.528 10.0 0.651 12.0 0.746	Cd 0.0060 0.0078 0.0099 0.0128 0.0165 0.0209 0.0317 0.0450 0.1422 0.2100	0.0 17.8 20.8 21.2 20.5 19.3 16.7 14.5 5.2	0.000 0.007 0.010 0.013 0.017 0.020 0.027 0.033 0.037 0.044	0.00 0.99 0.99 0.99 0.99 0.99 0.99	0.0574 0.0301

## 1995 Medium Flying Wing Propulsion

### PHYSICAL ATTRIBUTES

ESF = 0.401 WEIGHT = 940.660 LENGTH = 7.916

POWER	MACH	ALT (ft)	THRUST (lb)	SFC	FFLOW (lb/hr)	WAF (lb/sec)
100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.0 0.0 0.0 0.0 0.0 0.0	8978. 7856. 6734. 5611. 4489. 3367. 2245. 1122.	0.449 0.434 0.425 0.413 0.395 0.387 0.412 0.487	4031.3 3407.6 2863.4 2319.1 1774.9 1304.5 925.5 546.5	199. 184. 168. 155. 142. 119. 90. 71.
100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.600 0.600 0.600 0.600 0.600 0.600 0.600	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	2329. 2038. 1747. 1456. 1164. 873. 582. 291.	0.598 0.599 0.601 0.603 0.610 0.651 0.733 0.979	1392.8 1220.9 1049.0 877.2 710.5 568.7 426.9 285.0	199. 187. 177. 167. 156. 139. 125.
100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.800 0.800 0.800 0.800 0.800 0.800 0.800	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	2579. 2257. 1934. 1612. 1290. 967. 645. 322.	0.668 0.670 0.672 0.676 0.687 0.733 0.826 1.102	1723.0 1511.6 1300.3 1088.9 886.1 709.4 532.7 355.3	199. 188. 177. 168. 157. 143. 131.
100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.900 0.900 0.900 0.900 0.900 0.900 0.900	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	2698. 2361. 2024. 1686. 1349. 1012. 675. 337.	0.723 0.728 0.734 0.742 0.760 0.820 0.941 1.302	1951.1 1717.9 1484.6 1251.4 1025.3 829.9 634.6 439.2	199. 188. 178. 169. 159. 145. 133.

# 1995 Medium Flying Wing Weights

COMPONENT	POUNDS	KILOGRAMS	PERCENT
	150.	3502. 1589. 621. 0. 0. 267. 68. 544. 412.	30.78 13.97 5.46 0.00 0.00 2.35 0.60 4.78 3.62
PROPULSION ENGINES (1) FUEL SYSTEM	1450. 1102. 348.	658. 500. 158.	5.78 4.39 1.39
(COMPONENTS BELOW DO NOT HYD. + PNEU. ELECTRICAL AVIONICS	210. 817. 2790. 219. 398.	FACTOR = 0.85) 95. 370. 1266. 99.	0.84 3.26 11.13
FUEL	4127.	1872.	16.46
PAYLOAD  FLIGHT CREW ( 2)  ARMAMENT  AMMUNITION  SHORT RANGE MISSILES  SRM LAUNCHERS  LASER GUIDED BOMBS  LGB PYLONS AND EJECTORS  EXTERNAL TANKS	398. 200. 4364.	2912. 163. 278. 130. 181. 91. 1980. 91. 0.	
TOTAL WEIGHT	25078.	11375.	100.00

## 1995 Medium Internal Attack Summary

## Standard English Units

GENERAL	FUSELAGE		WING	HTAIL	VTAIL
TOGW 29095. W/S 67.3 T/W Dry 0.43 CREW 2 N(Z) ULT 9.8	LENGTH 45.4 DIAMETER 4.6 VOLUME 658.2 WETTED AREA 604.9 FINENESS RATIO 9.9	AREA WETTED AREA SPAN L.E. SWEEP C/4 SWEEP ASPECT RATIO	432.4 736.3 44.7 20.4 14.5 4.63	102.9 140.3 19.2 35.0 30.0	58.5 117.3 7.7 47.8 30.0
ENGINE	WEIGHTS	TAPER RATIO T/C ROOT T/C TIP	0.31 0.09 0.06	0.39 0.09 0.07	0.30 0.08 0.06
NUMBER 1 LENGTH 9.4 DIAM. 3.1 WEIGHT 1347.8 TSLS 12646. SFCSLS 0.45	W % STRUCT. 9801. 33.7 PROPUL. 2077. 7.1 FIX. EQ. 5505. 18.9 FUEL 5290. 18.2 PAYLOAD 6421. 22.1	ROOT CHORD TIP CHORD M.A. CHORD LOC. OF L.E.	14.7 4.6 10.6 9.3	7.7 3.0 5.7 33.3	11.6 3.5 8.3 33.8

#### MISSION SUMMARY

PHASE	MACH	ALT	FUEL	TIME	DIST	L/D	THRUST	SFC	Q
======	====	=====	=====	=====	=====	=====	======	=====	=====
TAKEOFF	0.00	0.	141.	10.5					
CLIMB	0.84	36500.	512.	9.4	75.1	15.59	2729.3	0.673	230.1
CRUISE	0.80	36500.	1272.	65.4	500.0	15.92	1726.9	0.668	208.3
CRUISE	0.80	100.	401.	5.7	50.0	5.05	5337.7	0.795	944.6
COMBAT	0.85	100.	171.	2.0	18.7	8.52	6275.4	0.816	1066.4
CRUISE	0.80	100.	401.	5.7	50.0	4.95	5332.6	0.795	944.6
CLIMB	0.85	39500.	502.	10.1	80.7	15.72	2377.2	0.679	204.5
CRUISE	0.80	39500.	1129.	65.4	500.0	16.11	1542.6	0.663	180.4
LOITER	0.30	100.	368.	20.0	66.1	16.03	1532.3	0.720	132.8

BLOCK TIME = 3.061 HR BLOCK RANGE = 1340.9 NM

### COMBAT PHASES

MACH	ALT	PS1G	NZS	CLS	CDS	ALS	NZI	PSI	CLI	CDI	ALI	CBE
0.85	100.	100.	5.3	0.116	0.0136	0.8	6.5	-52.	0.372	0.0222	2.7	12013.
0.20	100.	83.	1.5	1.311	0.1431	15.0	1.5	65.	1.311	0.1431	15.0	499.

### 1995 Medium Internal Attack Geometry

	WING	H.TAIL	V.TAIL	CANARD	UNITS
PLAN AREA	432.4	102.9	58.5	0.0	(SQ.FT.)
SURFACE AREA	736.3	140.3	117.3	0.0	(SQ.FT.)
VOLUME	223.8	34.1	25.3	0.0	(CU.FT.)
SPAN	44.724	19.177	7.726	0.000	(FT.)
L.E. SWEEP	20.421	35.042	40.035	0.000	(DEG.)
C/4 SWEEP	14.518	30.000	30.000	0.000	(DEG.)
T.E. SWEEP	-4.637	11.612	-11.916	0.000	(DEG.)
ASPECT RATIO	4.626	3.574	1.020	0.000	
ROOT CHORD	14.738	7.743	11.635	0.000	(FT.)
ROOT THICKNESS	15.917	8.362	11.030	0.000	(IN.)
ROOT T/C	0.090	0.090	0.079	0.000	
TIP CHORD	4.598	2.989	3.514	0.000	(FT.)
TIP THICKNESS	3.311	2.510	2.741	0.000	(IN.)
TIP T/C	0.060	0.070	0.065	0.000	
TAPER RATIO	0.312	0.386	0.302	0.000	
MEAN AERO CHORD	10.554	5.717	8.300	0.000	(FT.)
LE ROOT AT	9.300	33.255	33.766	0.000	(FT.)
C/4 ROOT AT	12.985	35.190	36.675	0.000	(FT.)
TE ROOT AT	24.038	40.997	45.401	0.000	(FT.)
LE M.A.C. AT	12.735	36.120	36.431	0.000	(FT.)
C/4 M.A.C. AT	15.374	37.549	38.506	0.000	(FT.)
TE M.A.C. AT	23.289	41.837	44.731	0.000	(FT.)
Y M.A.C. AT	9.227	4.086	3.173	0.000	
LE TIP AT	17.626	39.979	40.257	0.000	(FT.)
C/4 TIP AT	18.775	40.726	41.135	0.000	(FT.)
TE TIP AT	22.224	42.967	43.771	0.000	(FT.)
ELEVATION	0.000	0.000	2.296	0.000	(FT.)
VOLUME COEFF		0.500	0.070	0.000	

AIRCRAFT WEIGHT = 29094.568 Lbs. AIRCRAFT VOLUME = 941.282 Cu.Ft. AIRCRAFT DENSITY = 30.910 Lbs./Cu.Ft.

1995 Medium Internal Attack Mission Performance

PHASE	M	H	CL	ALPHA	WFUEL	TIME	VEL
	SFC(I)	THRUST(I)	CD	GAMMA	W	WA	Q
	SFC(U)	THRUST(U)	CDINST	L/D	THR/THA	PR	X
CLIMB	0.84	36500.	0.2847	2.10	512.4	9.37	814.
	0.67	2729.	0.0183	1.84	28441.6	0.00	230.
	0.00	0.	0.0000	15.59	1.00	0.00	75.
CRUISE	0.80	36500.	0.3052	2.38	1272.0	65.38	774.
	0.67	1727.	0.0192	0.00	27169.6	0.00	208.
	0.00	3856.	0.0000	15.92	0.65	0.00	500.
CRUISE	0.80	100.	0.0660	0.51	400.9	5.67	893.
	0.79	5338.	0.0131	0.00	26768.7	0.00	945.
	0.00	13874.	0.0000	5.05	0.59	0.00	50.
COMBAT	0.85	100.	0.1159	0.83	170.7	2.00	949.
	0.82	6275.	0.0136	0.47	26598.0	0.00	1066.
	0.00	19981.	0.0000	8.52	0.71	0.00	19.
CRUISE	0.80	100.	0.0646	0.50	400.6	5.67	893.
	0.79	5333.	0.0131	0.00	26197.4	0.00	9 <b>4</b> 5.
	0.00	13867.	0.0000	4.95	0.59	0.00	50.
CLIMB	0.85	39500.	0.2896	2.10	502.3	10.08	825.
	0.68	2377.	0.0184	1.67	25695.1	0.00	204.
	0.00	0.	0.0000	15.72	1.00	0.00	81.
CRUISE	0.80	39500.	0.3185	2.49	1128.6	65.38	774.
	0.66	1543.	0.0198	0.00	24566.5	0.00	180.
	0.00	3383.	0.0000	16.11	0.66	0.00	500.
LOITER	0.30	100.	0.4277	4.47	367.5	20.00	335.
	0.72	1532.	0.0267	0.00	24199.0	0.00	133.
	0.00	3011.	0.0000	16.03	0.14	0.00	66.

### FUEL SUMMARIES

MISSION FUEL = 4896. RESERVE FUEL = 245. TRAPPED FUEL = 150.

TOTAL FUEL = 5290.

## 1995 Medium Internal Attack Maneuver Performance

	CONDITIONS	PS	NZ	TDOT	RADIUS	ALPHA	CL	CD
M= 0.85 H= 100.	1 G FLIGHT SUSTAINED MAX. INST.	100.1 0.0 -51.9	1.00 5.25 6.50	0.00 10.02 12.48	0. 5426. 4355.	0.42 0.83 2.73	0.058 0.116 0.372	0.0129 0.0136 0.0222
	COMBAT ENERGY	Z = 0.1	20127E	+05				
M= 0.20 H= 100.	1 G FLIGHT SUSTAINED MAX. INST. COMBAT ENERGY	83.1 0.0 64.8 7 = 0.4	1.00 1.50 1.50 98788E	0.00 9.24 9.24 +03	0. 1384. 1384.	10.55 15.00 15.00	0.948 1.311 1.311	0.0801 0.1431 0.1431

# 1995 Medium Internal Attack Aerodynamics

Mach =	0.90	Altitu	ide =	100.				
Parasite I Friction Body Wing Strakes H. Tail V. Tail Canard Pods Engine Cowl Boattail Interferen	.0106 .0032 .0054 .0000 .0011 .0009 .0000 .0000	2.0 0 3.0 0 4.0 0 5.0 0 6.0 0 8.0 0 10.0 1 12.0 1	C1 .000 .302 .450 .544 .634 .721 .891 .006 .095	Cd 0.0216 0.0278 0.0392 0.0585 0.0751 0.0949 0.1437 0.2276 0.2869 0.3865	L/D 0.0 10.9 11.5 9.3 8.4 7.6 6.2 4.4 3.8 3.1	120	e 0.00 1.01 0.79 0.55 0.52 0.49 0.45 0.34 0.31 0.28	
External	.0000				e Fact	ors		
Tanks Bombs Stores Extra Camber	.0000 .0000 .0000 .0000				Alpha 1^.5Al	pha		0.0809 0.0403
Cdmin	.0216							
Mach =	0.60	Altitu	ide =	35000.				
Parasite I Friction Body Wing Strakes H. Tail V. Tail Canard Pods Engine Cowl Boattail Interferen	0rag .0111 .0034 .0056 .0000 .0012 .0009 .0000 .0000 .0000 .0000	Induced Dr Alpha 0.0 0 2.0 0 3.0 0 4.0 0 5.0 0 6.0 0 8.0 0 10.0 0		Cd 0.0131 0.0164 0.0205 0.0261 0.0362 0.0671 0.1066 0.1569 0.2175 0.3261	L/D 0.0 13.3 15.8 16.4 14.7 9.2 7.3 5.9 4.9 3.9	016 023 030 038 058 080 105 147	e 0.00 0.98 0.98 0.97 0.85 0.48 0.44 0.41 0.39 0.35	
Parasite I Friction Body Wing Strakes H. Tail V. Tail Canard Pods Engine Cowl Boattail Interferen	0rag .0111 .0034 .0056 .0000 .0012 .0009 .0000 .0000 .0000	Induced Dr Alpha 0.0 0 2.0 0 3.0 0 4.0 0 5.0 0 6.0 0 8.0 0 10.0 0	C1 .000 .218 .325 .429 .533 .617 .776 .928 .070	Cd 0.0131 0.0164 0.0205 0.0261 0.0362 0.0671 0.1066 0.1569 0.2175 0.3261	0.0 13.3 15.8 16.4 14.7 9.2 7.3 5.9 4.9	0.000 010 016 023 030 038 058 080 105 147	0.00 0.98 0.98 0.97 0.85 0.48 0.44 0.41	0.0843 0.0373

## 1995 Medium Internal Attack Propulsion

#### PHYSICAL ATTRIBUTES

ESF = 0.565 WEIGHT = 1347.763 LENGTH = 9.395 DIAM = 3.149

POWER	MACH	ALT (ft)	THRUST (lb)	SFC	FFLOW (lb/hr)	WAF (lb/sec)
100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.0 0.0 0.0 0.0 0.0 0.0	12646. 11065. 9484. 7904. 6323. 4742. 3161. 1581.	0.449 0.434 0.425 0.413 0.395 0.387 0.412 0.487	5677.9 4799.5 4032.9 3266.4 2499.8 1837.3 1303.5 769.7	280. 259. 237. 218. 201. 168. 127. 100.
100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.600 0.600 0.600 0.600 0.600 0.600 0.600	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	3280. 2870. 2460. 2050. 1640. 1230. 820. 410.	0.598 0.599 0.601 0.603 0.610 0.651 0.733 0.979	1961.6 1719.6 1477.5 1235.4 1000.7 801.0 601.2 401.4	280. 264. 249. 235. 220. 196. 176.
100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.800 0.800 0.800 0.800 0.800 0.800 0.800	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	3633. 3179. 2724. 2270. 1816. 1362. 908. 454.	0.668 0.670 0.672 0.676 0.687 0.733 0.826 1.102	2426.7 2129.0 1831.4 1533.7 1248.1 999.2 750.2 500.4	280. 264. 250. 236. 222. 201. 184. 155.
100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.900 0.900 0.900 0.900 0.900 0.900 0.900	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	3801. 3325. 2850. 2375. 1900. 1425. 950. 475.	0.723 0.728 0.734 0.742 0.760 0.820 0.941 1.302	2748.1 2419.6 2091.1 1762.5 1444.1 1168.9 893.7 618.6	280. 265. 251. 238. 224. 205. 188. 173.

# 1995 Medium Internal Attack Weights

COMPONENT	POUNDS	KILOGRAMS	PERCENT
WING	2774. 776. 255. 589. 150.	1362. 1258. 352. 116. 267. 68.	9.53 2.67 0.88 2.02 0.52 4.12
PROPULSION ENGINES (1) FUEL SYSTEM	2077. 1578. 499.	942. 716. 226.	7.14 5.42 1.72
(COMPONENTS BELOW DO NOT HYD. + PNEU. ELECTRICAL	1NCLUDE TECH 244. 817. 2790. 219.	111. 370. 1266. 99.	0.84 2.81 9.59
FUEL	5290.	2400.	18.18
PAYLOAD  FLIGHT CREW ( 2)  ARMAMENT  AMMUNITION  SHORT RANGE MISSILES  SRM LAUNCHERS  LASER GUIDED BOMBS  LGB PYLONS AND EJECTORS  EXTERNAL TANKS	287. 398. 200. 4364.	163. 278. 130. 181.	22.07 1.24 2.10 0.99 1.37 0.69 15.00 0.69 0.00
TOTAL WEIGHT	29095.	13197.	100.00

## 1995 MRF Summary

## Standard English Units

GENERAL	FUSELAGE		WING	HTAIL	VTAIL
TOGW 41604. W/S 67.6 T/W DRY 0.78 T/W WET 1.24 CREW 1 N(Z) ULT 13.5	LENGTH 51.5 DIAMETER 5.1 VOLUME 817.5 WETTED AREA 701.4 FINENESS RATIO 10.0	AREA WETTED AREA SPAN L.E. SWEEP C/4 SWEEP ASPECT RATIO TAPER RATIO	615.4 913.1 35.1 42.1 24.3 2.00 0.05	234.9 282.3 21.7 42.1 24.3 2.00 0.05	93.4 186.9 9.7 53.6 24.3 1.00 0.05
ENGINE	WEIGHTS	T/C ROOT T/C TIP	0.05	0.05	0.05
NUMBER 1 LENGTH 16.1 DIAM. 3.7 WEIGHT 3118.8 TSLS 32474. SFCSLS 0.75	W % STRUCT. 10402. 25.0 PROPUL. 4935. 11.9 FIX. EQ. 4585. 11.0 FUEL 17330. 41.7 PAYLOAD 4351. 10.4	ROOT CHORD TIP CHORD M.A. CHORD LOC. OF L.E.	33.4 1.7 22.3 14.8	20.6 1.0 13.8 37.5	18.4 0.9 12.3 33.1

### MISSION SUMMARY

PHASE	MACH	ALT	FUEL	TIME	DIST	L/D	THRUST	SFC	Q
======	====	=====	=====	=====	=====	=====	======	=====	======
TAKEOFF	0.00	0.	635.	10.5					
CRUISE	0.85	100.	5088.	26.7	250.0	4.78	7858.1	1.449	1066.4
CLIMB	0.92	36296.	544.	1.9	16.4	8.74	9623.1	0.922	275.3
LOITER	0.80	37482.	3492.	60.0	458.9	8.41	3989.9	0.848	199.6
CLIMB	0.89	50000.	519.	1.4	9.7	7.39	9705.0	1.933	135.7
ACCEL	1.50	50000.	599.	1.4	16.4	3.56	17565.6	2.019	383.7
CRUISE	1.50	50000.	1669.	10.5	150.0	3.47	8535.6	1.113	383.7
COMBAT	1.50	50000.	642.	2.0	28.7	4.79	11967.8	1.610	383.7
CRUISE	0.91	42000.	2150.	46.0	400.0	8.87	3018.2	0.900	207.1
LOITER	0.30	100.	1023.	20.0	66.1	7.91	3320.2	0.924	132.8

BLOCK TIME = 2.840 HR BLOCK RANGE = 1401.0 NM

### COMBAT PHASES

MACH	ALT	PS1G	NZS	CLS	CDS	ALS	NZI	PSI	CLI	CDI	ALI	CBE
1.50	50000.	0.	1.0	0.130	0.0366	2.6	6.2	-2338.	0.799	0.2448	15.0	0.
1.50	50000.	454.	3.0	0.242	0.0505	4.7	6.6	-2041.	0.799	0.2448	15.0	54432.
0.20	100.	397.	1.6	0.781	0.1888	15.0	1.6	369.	0.781	0.1888	15.0	2380.
0.90	30000.	530.	3.8	0.580	0.1093	10.7	5.3	-554.	0.811	0.2056	15.0	11130.

## 1995 MRF Geometry

	WING	H.TAIL	V.TAIL	CANARD	UNITS
PLAN AREA	615.4	234.9	93.4	0.0	(SQ.FT.)
SURFACE AREA	913.1	282.3	186.9	0.0	(SQ.FT.)
VOLUME	340.2	107.4	38.1	0.0	(CU.FT.)
SPAN	35.084	21.673	9.662	0.000	(FT.)
L.E. SWEEP	42.138	42.138	42.138	0.000	(DEG.)
C/4 SWEEP	24.341	24.341	24.341	0.000	(DEG.)
T.E. SWEEP	-42.138	-42.138	-42.138	0.000	(DEG.)
ASPECT RATIO	2.000	2.000	1.000	0.000	
ROOT CHORD	33.413	20.641	18.405	0.000	(FT.)
ROOT THICKNESS	20.048	12.384	11.043	0.000	(IN.)
ROOT T/C	0.050	0.050	0.050	0.000	
TIP CHORD	1.671	1.032	0.920	0.000	(FT.)
TIP THICKNESS	0.802	0.495	0.442	0.000	(IN.)
TIP T/C	0.040	0.040	0.040	0.000	
TAPER RATIO	0.050	0.050	0.050	0.000	
MEAN AERO CHORD	22.329	13.793	12.299	0.000	(FT.)
LE ROOT AT	14.804	37.509	33.055	0.000	(FT.)
C/4 ROOT AT	23.157	42.669	37.657	0.000	(FT.)
TE ROOT AT	48.217	58.150	51.460	0.000	(FT.)
LE M.A.C. AT	20.346	40.933	36.108	0.000	(FT.)
C/4 M.A.C. AT	25.928	44.381	39.183	0.000	(FT.)
TE M.A.C. AT	42.675	54.726	48.407	0.000	(FT.)
Y M.A.C. AT	6.126	3.784	3.374	0.000	
LE TIP AT	30.675	47.313	41.798	0.000	(FT.)
C/4 TIP AT	31.093	47.571	42.028	0.000	(FT.)
TE TIP AT	32.346	48.346	42.718	0.000	(FT.)
ELEVATION	0.232	-0.257	2.573	0.000	(FT.)
VOLUME COEFF		0.315	0.057	0.000	

AIRCRAFT WEIGHT = 41603.836 Lbs. AIRCRAFT VOLUME = 1341.306 Cu.Ft. AIRCRAFT DENSITY = 31.017 Lbs./Cu.Ft.

1995 MRF Mission Performance

PHASE	M	H	CL	ALPHA	WFUEL	TIME	VEL
	SFC(I)	THRUST(I)	CD	GAMMA	W	WA	Q
	SFC(U)	THRUST(U)	CDINST	L/D	THR/THA	PR	X
CRUISE	0.85	100.	0.0572	0.99	5088.1	26.69	949.
	1.45	7858.	0.0120	0.00	35881.1	0.00	1066.
	0.00	22720.	0.0000	4.78	0.30	0.00	250.
CLIMB	0.92	36296.	0.2183	3.90	544.2	1.94	886.
	0.92	9623.	0.0250	8.77	35336.8	0.00	275.
	0.00	0.	0.0000	8.74	1.00	0.00	16.
LOITER	0.80	37482.	0.2730	5.07	3491.9	60.00	774.
	0.85	3990.	0.0325	0.00	31845.0	0.00	200.
	0.00	6357.	0.0000	8.41	0.48	0.00	459.
CLIMB	0.89	50000.	0.3624	6.66	519.2	1.35	863.
	1.93	9705.	0.0490	10.31	31325.7	0.00	136.
	0.00	0.	0.0000	7.39	1.97	0.00	10.
ACCEL	1.50	50000.	0.1304	2.56	599.0	1.42	1452.
	2.02	17566.	0.0366	0.00	30726.7	0.00	384.
	0.00	24661.	0.0000	3.56	2.03	0.00	16.
COMBAT	1.50	50000.	0.1301	2.56	0.3	0.10	1452.
	1.12	8632.	0.0366	0.00	30726.4	0.00	384.
	0.00	15727.	0.0000	3.56	1.00	0.00	1.
CRUISE	1.50	50000.	0.1254	2.47	1669.3	10.46	1452.
	1.11	8536.	0.0361	0.00	29057.1	0.00	384.
	0.00	15605.	0.0000	3.47	0.99	0.00	150.
COMBAT	1.50	50000.	0.2420	4.67	642.4	2.00	1452.
	1.61	11968.	0.0505	1.07	28414.6	0.00	384.
	0.00	24661.	0.0000	4.79	1.39	0.00	29.
CRUISE	0.91	42000.	0.2102	3.75	2149.9	45.98	881.
	0.90	3018.	0.0237	0.00	26264.7	0.00	207.
	0.00	5297.	0.0000	8.87	0.41	0.00	400.
LOITER	0.30	100.	0.3213	6.16	1023.0	20.00	335.
	0.92	3320.	0.0406	0.00	25241.7	0.00	133.
	0.00	4867.	0.0000	7.91	0.11	0.00	66.

### FUEL SUMMARIES

MISSION FUEL = 16362. RESERVE FUEL = 818. TRAPPED FUEL = 150.

TOTAL FUEL = 17330.

# 1995 MRF Maneuver Performance

	CONDITIONS	PS	NZ	TDOT	RADIUS	ALPHA	CL	CD
M= 1.50 H=50000.	1 G FLIGHT SUSTAINED MAX. INST. COMBAT ENERG	0.0 -2337.9		7.78	465095.		0.130 0.130 0.799	0.0366 0.0365 0.2448
M= 1.50 H=50000.	1 G FLIGHT SUSTAINED MAX. INST. COMBAT ENERG	0.0 -2041.0	2.99 6.65	3.58 8.34	23234.		0.123 0.242 0.799	0.0359 0.0505 0.2448
M= 0.20 H= 100.	1 G FLIGHT SUSTAINED MAX. INST. COMBAT ENERG	0.0 369.1	1.64 1.64	10.74	0. 1191. 1191.	13.28 15.00 15.00	0.695 0.781 0.781	0.1504 0.1888 0.1888
M= 0.90 H=30000.	1 G FLIGHT SUSTAINED MAX. INST. COMBAT ENERG	530.0 0.0 -553.8 GY = 0.1	3.81 5.31	0.00 7.58 10.74 +05	0. 6769. 4777.	2.75 10.69 15.00	0.158 0.580 0.811	0.0181 0.1093 0.2056

## 1995 MRF Propulsion

## PHYSICAL ATTRIBUTES

ESF = 1.214 WEIGHT = 3118.777 LENGTH = 16.087 DIAM = 3.713

POWER	MACH	ALT (ft)	THRUST (lb)	SFC	FFLOW (lb/hr)	WAF (lb/sec)
100.00 100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.0 0.0 0.0 0.0 0.0 0.0 0.0	51449. 32474. 28414. 24355. 20296. 16237. 12178. 8118. 4059.	1.770 0.754 0.731 0.701 0.661 0.655 0.646 0.629 0.690	91064.2 24485.0 20775.9 17066.7 13410.8 10641.6 7872.5 5103.3 2801.3	382. 382. 351. 324. 298. 253. 218. 190. 123.
100.00 100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.600 0.600 0.600 0.600 0.600 0.600 0.600	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	19311. 10128. 8862. 7596. 6330. 5064. 3798. 2532. 1266.	1.936 0.829 0.811 0.787 0.777 0.779 0.783 0.821 0.958	37387.0 8396.1 7188.3 5980.5 4918.1 3945.2 2972.4 2078.0 1212.7	382. 382. 357. 334. 300. 265. 235. 195. 160.
100.00 100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.800 0.800 0.800 0.800 0.800 0.800 0.800 0.800	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	22558. 11675. 10215. 8756. 7297. 5837. 4378. 2919. 1459.	1.931 0.889 0.878 0.864 0.866 0.889 0.927 1.025 1.361	43559.5 10378.9 8971.4 7564.0 6315.7 5186.5 4057.2 2992.8 1986.7	382. 382. 359. 338. 308. 275. 247. 212.
100.00 100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.900 0.900 0.900 0.900 0.900 0.900 0.900	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	24529. 12519. 10954. 9389. 7824. 6259. 4695. 3130. 1565.	1.948 0.944 0.934 0.922 0.926 0.955 1.002 1.116 1.503	47784.6 11813.8 10235.2 8656.7 7245.5 5974.8 4704.1 3494.2 2352.3	382. 382. 359. 338. 309. 277. 249. 216. 180.

# 1995 MRF Weights

COMPONENT	POUNDS	KILOGRAMS	PERCENT
AIRFRAME STRUCTURE WING FUSELAGE HORIZONTAL TAIL VERTICAL TAIL REACTION CONTROL SYSTEM WING FOLD INTERNAL BAY STRUCTURE ALIGHTING GEAR	150.	4718. 1422. 1481. 448. 369. 0. 68. 272. 658.	25.00 7.54 7.85 2.38 1.96 0.00 0.36 1.44 3.49
PROPULSION ENGINES (1) FUEL SYSTEM	4936. 3618. 1318.	2239. 1641. 598.	11.86 8.70 3.17
FIXED EQUIPMENT (COMPONENTS BELOW DO NOT HYD. + PNEU. ELECTRICAL AVIONICS INSTRUMENTATION DE-ICE/AIR CONDITION AUXILIARY GEAR FURNISH. + EQPT. FLIGHT CONTROLS	4585. INCLUDE TEC 605. 544. 1652. 94. 610. 200. 375. 1314.	CH FACTOR=0.85) 274. 247. 749. 43.	11.02 1.45 1.31 3.97 0.23 1.47 0.48 0.90 3.16
FUEL	17330.	7861.	41.66
PAYLOAD  FLIGHT CREW ( 1)  ARMAMENT  AMMUNITION  LONG RANGE MISSILES  LRM PYLONS & LAUNCHERS  SHORT RANGE MISSILES  SRM LAUNCHERS  EXTERNAL TANKS	4351. 180. 612. 287. 1974. 700. 398. 200.	1974. 82. 278. 130. 895. 318. 181. 91. 0.	10.46 0.43 1.47 0.69 4.74 1.68 0.96 0.48 0.00
TOTAL WEIGHT	41604.	18871.	100.00

# 1995 NFA Summary

# Standard English Units

GENERAL	FUSELAGE		WING	HTAIL	VTAIL
TOGW 49471. W/S 66.1	LENGTH 52.7 DIAMETER 5.3	AREA WETTED AREA	748.4 1136.1	285.6 357.7	113.5 227.3
T/W DRY 0.77 T/W WET 1.22	VOLUME 885.8 WETTED AREA 739.0	SPAN L.E. SWEEP	38.7 42.1	23.9 42.1 24.3	10.7 53.6 24.3
CREW 1 N(Z) ULT 13.5	FINENESS RATIO 10.0	C/4 SWEEP ASPECT RATIO TAPER RATIO	24.3 2.00 0.05	2.00 0.05	1.00 0.05
ENGINE	WEIGHTS	T/C ROOT T/C TIP	0.05	0.05	0.05
NUMBER 1 LENGTH 17.5 DIAM. 4.0	W % STRUCT. 13995. 28.3 PROPUL. 5861. 11.8	ROOT CHORD TIP CHORD M.A. CHORD	36.8 1.8 24.6	22.8 1.1 15.2	20.3 1.0 13.6
DIAM. 4.0 WEIGHT 3703.6 TSLS 38248. SFCSLS 0.75	FIX. EQ. 4893. 9.9 FUEL 20371. 41.2 PAYLOAD 4351. 8.8	LOC. OF L.E.	14.5	36.8	32.4

### MISSION SUMMARY

PHASE	MACH	ALT	FUEL	TIME	DIST	L/D	THRUST	SFC	Q
======	====	=====	=====	=====	======	=====	======	=====	=====
TAKEOFF	0.00	0.	748.	10.5					
CRUISE	0.85	100.	5979.	26.7	250.0	4.85	9221.3	1.451	1066.4
CLIMB	0.92	36296.	648.	2.0	16.6	8.87	11341.1	0.922	275.7
LOITER	0.80	37464.	4100.	60.0	458.9	8.54	4684.6	0.848	199.7
CLIMB	0.89	50000.	620.	1.4	9.8	7.53	11430.8	1.933	135.7
ACCEL	1.50	50000.	713.	1.4	16.6	3.62	20689.3	2.019	383.7
CRUISE	1.50	50000.	1962.	10.5	150.0	3.52	10036.3	1.113	383.7
COMBAT	1.50	50000.	753.	2.0	28.7	4.87	14062.4	1.607	383.7
CRUISE	0.91	42000.	2530.	46.0	400.0	9.01	3553.7	0.900	207.1
LOITER	0.30	100.	1205.	20.0	66.1	8.03	3911.8	0.924	132.8

BLOCK TIME = 2.841 HR BLOCK RANGE = 1401.4 NM

#### COMBAT PHASES

MACH	ALT	PS1G	NZS	CLS	CDS	ALS	NZI	PSI	CLI	CDI	ALI	CBE
1.50	50000.	1.	1.0	0.128	0.0354	2.5	6.3	-2383.	0.799	0.2438	15.0	5.
1.50	50000.	448.	3.0	0.238	0.0488	4.6	6.8	-2093.	0.799	0.2438	15.0	53762.
0.20	100.	390.	1.6	0.778	0.1869	15.0	1.6	362.	0.778	0.1869	15.0	2342.
0.90	30000.	524.	3.8	0.569	0.1054	10.6	5.4	-573.	0.807	0.2036	15.0	11007.

## 1995 NFA Geometry

	WING	H.TAIL	V.TAIL	CANARD	UNITS
PLAN AREA	748.4	285.6	113.5	0.0	(SQ.FT.)
SURFACE AREA	1136.1	357.7	227.3	0.0	(SQ.FT.)
VOLUME	466.6	144.0	51.1	0.0	(CU.FT.)
SPAN	38.689	23.900	10.655	0.000	(FT.)
L.E. SWEEP	42.138	42.138	42.138	0.000	(DEG.)
C/4 SWEEP	24.341	24.341	24.341	0.000	(DEG.)
T.E. SWEEP	-42.138	-42.138	-42.138	0.000	(DEG.)
ASPECT RATIO	2.000	2.000	1.000	0.000	
ROOT CHORD	36.847	22.762	20.296	0.000	(FT.)
ROOT THICKNESS	22.108	13.657	12.178	0.000	(IN.)
ROOT T/C	0.050	0.050	0.050	0.000	
TIP CHORD	1.842	1.138	1.015	0.000	(FT.)
TIP THICKNESS	0.884	0.546	0.487	0.000	(IN.)
TIP T/C	0.040	0.040	0.040	0.000	
TAPER RATIO	0.050	0.050	0.050	0.000	
MEAN AERO CHORD	24.623	15.211	13.563	0.000	(FT.)
LE ROOT AT	14.503	36.789	32.404	0.000	(FT.)
C/4 ROOT AT	23.715	42.480	37.478	0.000	(FT.)
TE ROOT AT	51.350	59.551	52.700	0.000	(FT.)
LE M.A.C. AT	20.615	40.565	35.771	0.000	(FT.)
C/4 M.A.C. AT	26.771	44.367	39.161	0.000	(FT.)
TE M.A.C. AT	45.238	55.775	49.333	0.000	(FT.)
Y M.A.C. AT	6.755	4.173	3.721	0.000	
LE TIP AT	32.006	47.601	42.045	0.000	(FT.)
C/4 TIP AT	32.466	47.886	42.298	0.000	(FT.)
TE TIP AT	33.848	48.739	43.059	0.000	(FT.)
ELEVATION	0.237	-0.264	2.635	0.000	(FT.)
VOLUME COEFF		0.273	0.049	0.000	

AIRCRAFT WEIGHT = 49471.258 Lbs. AIRCRAFT VOLUME = 1598.504 Cu.Ft. AIRCRAFT DENSITY = 30.948 Lbs./Cu.Ft.

## 1995 NFA Mission Performance

PHASE	M	H	CL	ALPHA	WFUEL	TIME	VEL
	SFC(I)	THRUST(I)	CD	GAMMA	W	WA	Q
	SFC(U)	THRUST(U)	CDINST	L/D	THR/THA	PR	X
CRUISE	0.85	100.	0.0560	0.99	5979.0	26.69	949.
	1.45	9221.	0.0116	0.00	42744.7	0.00	1066.
	0.00	26716.	0.0000	4.85	0.30	0.00	250.
CLIMB	0.92	36296.	0.2130	3.85	647.6	1.96	887.
	0.92	11341.	0.0240	8.72	42097.1	0.00	276.
	0.00	0.	0.0000	8.87	1.00	0.00	17.
LOITER	0.80	37464.	0.2675	5.02	4099.7	60.00	774.
	0.85	4685.	0.0313	0.00	37997.4	0.00	200.
	0.00	7471.	0.0000	8.54	0.48	0.00	459.
CLIMB	0.89	50000.	0.3544	6.58	619.6	1.37	863.
	1.93	11431.	0.0471	10.23	37377.8	0.00	136.
	0.00	0.	0.0000	7.53	1.97	0.00	10.
ACCEL	1.50	50000.	0.1280	2.51	713.1	1.43	1452.
	2.02	20689.	0.0354	0.00	36664.8	0.00	384.
	0.00	29046.	0.0000	3.62	2.03	0.00	17.
CRUISE	1.50	50000.	0.1231	2.42	1961.8	10.46	1452.
	1.11	10036.	0.0349	0.00	34702.6	0.00	384.
	0.00	18358.	0.0000	3.52	0.99	0.00	150.
COMBAT	1.50	50000.	0.2378	4.58	753.4	2.00	1452.
	1.61	14062.	0.0488	1.07	33949.2	0.00	384.
	0.00	29046.	0.0000	4.87	1.38	0.00	29.
CRUISE	0.91 0.90 0.00	42000. 3554. 6238.	0.2067 0.0229 0.0000	3.73 0.00 9.01	2530.4 31418.8 0.41		881. 207. 400.
LOITER	0.30	100.	0.3160	6.12	1205.2	20.00	335.
	0.92	3912.	0.0393	0.00	30213.6	0.00	133.
	0.00	5734.	0.0000	8.03	0.11	0.00	66.

### FUEL SUMMARIES

MISSION FUEL = 19258. RESERVE FUEL = 963. TRAPPED FUEL = 150.

TOTAL FUEL = 20371.

# 1995 NFA Maneuver Performance

	CONDITIONS	PS	NZ	TDOT	RADIUS	ALPHA	CL	CD
M= 1.50 H=50000.	1 G FLIGHT SUSTAINED MAX. INST COMBAT ENERG		1.00 1.02 6.33 60688E	7.93	0. 366342. 10489.	2.51 2.51 15.00	0.128 0.128 0.799	0.0353 0.0354 0.2438
M= 1.50 H=50000.	1 G FLIGHT SUSTAINED MAX. INST COMBAT ENERG	0.0 -2093.0			0. 23172. 9797.	2.37 4.58 15.00	0.121 0.238 0.799	0.0348 0.0488 0.2438
M= 0.20 H= 100.	1 G FLIGHT SUSTAINED MAX. INST. COMBAT ENERG	390.3 0.0 361.8 GY = 0.2	1.65 1.65	0.00 10.80 10.80 +04	0. 1184. 1184.	13.13 15.00 15.00	0.684 0.778 0.778	0.1455 0.1869 0.1869
M= 0.90 H=30000.	1 G FLIGHT SUSTAINED MAX. INST. COMBAT ENERG	524.2 0.0 -573.1 SY = 0.1	3.83 5.39	0.00 7.60 10.91 +05	0. 6747. 4702.	2.73 10.55 15.00	0.155 0.569 0.807	0.0174 0.1054 0.2036

## 1995 NFA Aerodynamics

Mach =	0.80	Altitude = 40000.	
Parasite Drag Friction Body Wing Strakes H. Tail V. Tail Canard Pods Engine Cowl Boattail Interference Wave External	.0094 .0023 .0040 .0000 .0014 .0018 .0000 .0000 .0000 .0000 .0000 .0013 .0000 .0000	Induced Drag  Alpha Cl Cd L/D Cm e  0.0 0.000 0.0108 0.0 0.000 0.00  2.0 0.112 0.0143 7.8005 0.57  3.0 0.164 0.0184 8.9008 0.56  4.0 0.215 0.0239 9.0011 0.56  5.0 0.266 0.0311 8.5015 0.55  6.0 0.319 0.0400 8.0019 0.55  8.0 0.425 0.0630 6.7029 0.55  10.0 0.532 0.0931 5.7040 0.55  12.0 0.639 0.1302 4.9053 0.54  15.0 0.798 0.1990 4.0075 0.54	0.0522
Tanks Bombs	.0000	ClAlpha Cdl^.5Alpha	0.0532 0.0289
Stores Extra	.0000		
Camber	.0000		
Cdmin	.0108		
Mach =	1.50	Altitude = 50000.	
Parasite Drag Friction Body Wing Strakes H. Tail V. Tail Canard Pods Engine Cowl Boattail Interference	.0080 .0019 .0034 .0000 .0012 .0015 .0000 .0000 .0000	Altitude = 50000.  Induced Drag Alpha Cl Cd L/D Cm e 0.0 0.000 0.0298 0.0 0.000 0.00 2.0 0.101 0.0333 3.0015 0.46 3.0 0.154 0.0378 4.1023 0.47 4.0 0.207 0.0442 4.7031 0.47 5.0 0.260 0.0525 5.0039 0.47 6.0 0.314 0.0628 5.0047 0.48 8.0 0.423 0.0892 4.7064 0.48 10.0 0.533 0.1237 4.3082 0.48 12.0 0.641 0.1660 3.9100 0.48 15.0 0.799 0.2438 3.3126 0.47	
Parasite Drag Friction Body Wing Strakes H. Tail V. Tail Canard Pods Engine Cowl Boattail	.0080 .0019 .0034 .0000 .0012 .0015 .0000 .0000 .0000	Induced Drag Alpha Cl Cd L/D Cm e 0.0 0.000 0.0298 0.0 0.000 0.00 2.0 0.101 0.0333 3.0015 0.46 3.0 0.154 0.0378 4.1023 0.47 4.0 0.207 0.0442 4.7031 0.47 5.0 0.260 0.0525 5.0039 0.47 6.0 0.314 0.0628 5.0047 0.48 8.0 0.423 0.0892 4.7064 0.48 10.0 0.533 0.1237 4.3082 0.48 12.0 0.641 0.1660 3.9100 0.48	0.0532

# 1995 NFA Propulsion

### PHYSICAL ATTRIBUTES

ESF = 1.430 WEIGHT = 3703.564 LENGTH = 17.459 DIAM = 4.030

POWER	MACH	ALT (ft)	THRUST (1b)	SFC	FFLOW (lb/hr)	WAF (lb/sec)
100.00 100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.000 0.000 0.000 0.000 0.000 0.000 0.000	0.0 0.0 0.0 0.0 0.0 0.0 0.0	60598. 38248. 33467. 28686. 23905. 19124. 14343. 9562. 4781.	1.770 0.754 0.731 0.701 0.661 0.655 0.646 0.629 0.690	107257.9 28839.2 24470.4 20101.7 15795.6 12534.0 9272.4 6010.9 3299.5	450. 450. 414. 382. 351. 299. 257. 223. 145.
100.00 100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.600 0.600 0.600 0.600 0.600 0.600 0.600	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	22745. 11929. 10438. 8947. 7456. 5964. 4473. 2982. 1491.	1.936 0.829 0.811 0.787 0.777 0.779 0.783 0.821 0.958	44035.4 9889.2 8466.6 7044.0 5792.6 4646.8 3501.0 2447.6 1428.4	450. 450. 420. 393. 353. 312. 277. 230. 188.
100.00 100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	0.900 0.900 0.900 0.900 0.900 0.900 0.900	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	28891. 14745. 12902. 11059. 9216. 7372. 5529. 3686. 1843.	1.948 0.944 0.934 0.922 0.926 0.955 1.002 1.116 1.503	56282.0 13914.6 12055.3 10196.1 8533.9 7037.2 5540.6 4115.5 2770.6	450. 450. 423. 398. 364. 326. 294. 254.
100.00 100.00 87.50 75.00 62.50 50.00 37.50 25.00 12.50	1.500 1.500 1.500 1.500 1.500 1.500 1.500	50000.0 50000.0 50000.0 50000.0 50000.0 50000.0 50000.0	20689. 10167. 8896. 7625. 6355. 5084. 3813. 2542. 1271.	2.019 1.116 1.099 1.090 1.077 1.098 1.153 1.267	41761.9 11342.4 9773.7 8309.8 6845.8 5583.8 4396.9 3220.7 2179.7	450. 450. 425. 397. 371. 335. 300. 268. 222.

## 1995 NFA Weights

COMPONENT	POUNDS	KILOGRAMS	PERCENT
AIRFRAME STRUCTURE WING FUSELAGE HORIZONTAL TAIL VERTICAL TAIL REACTION CONTROL SYSTEM WING FOLD INTERNAL BAY STRUCTURE ALIGHTING GEAR	3994. 4648. 1333. 1029. 0.	6350. 1812. 2108. 604. 467. 0. 68. 272.	28.29 8.07 9.40 2.69 2.08 0.00 0.30 1.21 4.53
PROPULSION ENGINES (1) FUEL SYSTEM	5861. 4296. 1565.	2659. 1949. 710.	11.85 8.68 3.16
(COMPONENTS BELOW DO NOT HYD. + PNEU. ELECTRICAL AVIONICS INSTRUMENTATION DE-ICE/AIR CONDITION AUXILIARY GEAR	719. 544. 1652. 94. 610. 200.	FACTOR=0.85) 326. 247.	
FUEL	20371.	9240.	41.18
PAYLOAD  FLIGHT CREW ( 1)  ARMAMENT  AMMUNITION  LONG RANGE MISSILES  LRM PYLONS & LAUNCHERS  SHORT RANGE MISSILES  SRM LAUNCHERS  EXTERNAL TANKS	4351. 180. 612. 287. 1974. 700. 398. 200. 0.	1974. 82. 278. 130. 895. 318. 181. 91.	8.79 0.36 1.24 0.58 3.99 1.41 0.80 0.40 0.00
TOTAL WEIGHT	49471.	22440.	100.00

### 1995 STOVL SUMMARY

#### Standard English Units

GENERAL	FUSELAGE		WING	HTAIL	VTAIL
TOGW 46276.	LENGTH 56.1	AREA	724.1	221.1	87.9
W/S 63.9	DIAMETER 5.6	WETTED AREA	1072.9	247.2	176.0
T/W DRY 0.77	VOLUME 1051.1	SPAN	38.1	21.0	9.4
T/W A/B 1.22	WETTED AREA 830.0	L.E. SWEEP	42.1	42.1	53.6
CREW 1	FINENESS RATIO 10.0	C/4 SWEEP	24.3	24.3	24.3
N(Z) ULT 13.5		ASPECT RATIO	2.00	2.00	1.00
•		TAPER RATIO	0.05	0.05	0.05
ENGINE	WEIGHTS	T/C ROOT	0.05	0.05	0.05
		T/C TIP	0.04	0.04	0.04
NUMBER 1	W %	ROOT CHORD	36.2	20.0	17.9
LENGTH 16.9	STRUCT. 11722. 25.3	TIP CHORD	1.8	1.0	0.9
DIAM. 3.9	PROPUL. 7040. 15.2	M.A. CHORD	24.2	13.4	11.9
WEIGHT 5069.1	FIX. EQ. 4768. 10.3	LOC. OF L.E.	16.2	43.3	38.2
TSLS 35731.	FUEL 18395. 39.8				
SFCSLS 0.75	PAYLOAD 4351. 9.40				

#### MISSION SUMMARY

PHASE	MACH	ALT	FUEL	TIME	DIST	L/D	THRUST	SFC	Q
======	====	=====	=====	=====	=====	=====	======	=====	=====
TAKEOFF	0.00	0.	748.	10.5			-		
CRUISE	0.85	100.	5579.	26.7	250.0	4.87	8598.0	1.452	1066.4
CLIMB	0.92	35000.	578.	1.8	15.2	8.97	11287.2	0.924	293.4
LOITER	0.79	36321.	3794.	60.0	454.3	8.71	4298.6	0.855	207.3
CLIMB	0.89	50000.	582.	1.4	9.9	7.52	10678.6	1.933	135.7
ACCEL	1.50	50000.	670.	1.4	16.7	3.62	19327.8	2.019	383.7
CRUISE	1.50	50000.	1837.	10.5	150.0	3.53	9395.0	1.113	383.7
COMBAT	1.50	50000.	709.	2.0	28.7	4.87	13186.1	1.612	383.7
CRUISE	0.91	41000.	2368.	46.0	400.0	9.12	3294.7	0.910	217.2
LOITER	0.30	100.	560.	10.0	33.1	8.11	3630.6	0.926	132.8

BLOCK TIME = 2.666 HR BLOCK RANGE = 1360.2 NM

#### COMBAT PHASES

MACH	ALT	PS1G	NZS	CLS	CDS	ALS	NZI	PSI	CLI	CDI	ALI	CBE
1.50	50000.	0.	1.0	0.124	0.0342	2.5	6.3	-2373.	0.770	0.2352	15.0	0.
0.90	30000.	521.	3.8	0.553	0.1024	10.5	5.4	-569.	0.779	0.1965	15.0	3125.
1 50	50000	446	3.0	0.230	0.0473	4.6	6.7	-2083.	0.770	0.2352	15.0	53473.

### 1995 STOVL Geometry

	WING	H.TAIL	V.TAIL	CANARD	UNITS
PLAN AREA	724.1	221.1	87.9	0.0	(SQ.FT.)
SURFACE AREA	1072.9	247.2	176.0	0.0	(SQ.FT.)
VOLUME	433.7	98.1	34.8	0.0	(CU.FT.)
SPAN	38.056	21.028	9.376	0.000	(FT.)
L.E. SWEEP	42.138	42.138	42.138	0.000	(DEG.)
C/4 SWEEP	24.341	24.341	24.341	0.000	(DEG.)
T.E. SWEEP	-42.138	-42.138	-42.138	0.000	(DEG.)
ASPECT RATIO	2.000	2.000	1.000	0.000	
ROOT CHORD	36.244	20.026	17.859	0.000	(FT.)
ROOT THICKNESS	21.746	12.016	10.716	0.000	(IN.)
ROOT T/C	0.050	0.050	0.050	0.000	
TIP CHORD	1.812	1.001	0.893	0.000	(FT.)
TIP THICKNESS	0.870	0.481	0.429	0.000	(IN.)
TIP T/C	0.040	0.040	0.040	0.000	
TAPER RATIO	0.050	0.050	0.050	0.000	
MEAN AERO CHORD	24.220	13.383	11.934	0.000	(FT.)
LE ROOT AT	16.165	43.318	38.198	0.000	(FT.)
C/4 ROOT AT	25.226	48.325	42.663	0.000	(FT.)
TE ROOT AT	52.409	63.344	56.057	0.000	(FT.)
LE M.A.C. AT	22.177	46.640	41.160	0.000	(FT.)
C/4 M.A.C. AT	28.232	49.986	44.144	0.000	(FT.)
TE M.A.C. AT	46.397	60.023	53.095	0.000	(FT.)
Y M.A.C. AT	6.645	3.671	3.274	0.000	(DD )
LE TIP AT	33.381	52.831	46.681	0.000	(FT.)
C/4 TIP AT	33.834	53.081	46.904	0.000	(FT.)
TE TIP AT	35.193	53.832	47.574	0.000	(FT.)
ELEVATION	0.252	-0.280 0.274	2.803	0.000	(FT.)
VOLUME COEFF		0.2/4	0.051	0.000	

AIRCRAFT WEIGHT = 46272.629 Lbs. AIRCRAFT VOLUME = 1652.424 Cu.Ft. AIRCRAFT DENSITY = 28.003 Lbs./Cu.Ft.

1995 STOVL Mission Performance

PHASE	SFC(I)	H THRUST(I) THRUST(U)	CD	GAMMA	WFUEL W THR/THA	WA	0
CRUISE	1.45	100. 8598. 24936.	0.0111	0.00	39995.7	0.00	1066.
CLIMB	0.92 0.92 0.00	35000. 11287. 0.	0.1972 0.0220 0.0000	3.59 9.65 8.97	578.4 39417.3 1.00	1.80 0.00 0.00	892. 293. 15.
LOITER	0.85	36321. 4299. 6951.	0.0286	0.00	35623.0	0.00	207.
CLIMB	0.89 1.93 0.00	50000. 10679. 0.	0.3483 0.0463 0.0000	6.60 10.06 7.52	582.3 35040.7 1.97	1.38 0.00 0.00	863. 136. 10.
	2.02	50000. 19328. 27135.	0.0342	0.00	34370.8	0.00	384.
CRUISE	1.50 1.11 0.00	50000. 9395. 17174.	0.1193 0.0338 0.0000	2.43 0.00 3.53	1837.4 32533.0 0.99	10.46 0.00 0.00	1452. 384. 150.
COMBAT	1.61	50000. 13186. 27135.	0.0473	1.07	31824.4	0.00	384.
CRUISE	0.91 0.91 0.00	41000. 3295. 5918.	0.1909 0.0209 0.0000	3.48 0.00 9.12	2367.6 29456.8 0.39	45.98 0.00 0.00	881. 217. 400.
	0.93	100. 3631. 5329.	0.0377	0.00	28896.4	0.00	133.

### FUEL SUMMARIES

MISSION FUEL = 17376. RESERVE FUEL = 869. TRAPPED FUEL = 150.

TOTAL FUEL = 18395.

## 1995 STOVL Maneuver Performance

	CONDITIONS	PS	NZ	TDOT	RADIUS	ALPHA	CL	CD
M= 1.50 H=50000.	1 G FLIGHT SUSTAINED MAX. INST COMBAT ENERG		1.00 1.00 6.30 55245E	7.89	0. 465095. 10539.	2.52 3.33 15.00	0.124 0.165 0.770	0.0342 0.0395 0.2352
M= 0.90 H=30000.	1 G FLIGHT SUSTAINED MAX. INST. COMBAT ENERG	520.8 0.0 -568.9 Y = 0.3	1.00 3.81 5.36 12491E	0.00 7.57 10.83 +04	0. 6775. 4736.	2.68 10.55 15.00	0.151 0.553 0.779	0.0168 0.1024 0.1965
M= 1.50 H=50000.	1 G FLIGHT SUSTAINED MAX. INST COMBAT ENERG		1.00 2.99 6.73 34733E	0.00 3.57 8.45	0. 23288. 9843.	2.39 4.60 15.00	0.117 0.230 0.770	0.0336 0.0473 0.2352

# 1995 STOVL Aerodynamics

Mach :	=	0.80	Altitude	= 400	00.					
Parasite I Friction Body Wing Strakes H. Tail V. Tail Canard Pods Engine Cowl Boattail Interfered		.0090 .0026 .0039 .0000 .0010 .0014 .0000 .0000 .0000	Induced Alpha 0.0 2.0 3.0 4.0 5.0 6.0 8.0 10.0 12.0 15.0	C1 0.000 0.111 0.162 0.211 0.262 0.312 0.415 0.518 0.620 0.770	Cd 0.0104 0.0139 0.0179 0.0234 0.0305 0.0392 0.0615 0.0906 0.1263 0.1920	L/D 0.0 8.0 9.0 8.6 8.7 5.7 4.9	Cm 0.000 005 009 013 017 022 032 044 058 082	e 0.00 0.56 0.55 0.55 0.54 0.54 0.53 0.53		
Wave External Tanks Bombs Stores Extra Camber		.0000 .0000 .0000 .0000 .0000			ClA	e Fact Alpha L^.5Al			0.0513 0.0284	
Cdmin	-	.0104								
Ma ala	_	1 50 31		F0000						
Mach :	=	1.50 AI	titude =	50000.						
Parasite I Friction Body Wing Strakes H. Tail V. Tail Canard Pods Engine Cowl Boattail Interfered	Drag	.0077 .0022 .0034 .0000 .0008 .0012 .0000 .0000 .0000 .0000	Induced Alpha 0.0 2.0 3.0 4.0 5.0 6.0 8.0 10.0 12.0		Cd 0.0288 0.0322 0.0365 0.0427 0.0507 0.0606 0.0861 0.1193 0.1601 0.2352	L/D 0.0 3.0 4.1 4.7 4.9 5.0 4.7 4.3 3.9 3.3	Cm 0.000 016 024 032 040 067 086 104 132	e 0.00 0.45 0.45 0.46 0.46 0.46 0.46 0.46		
Parasite 1 Friction Body Wing Strakes H. Tail V. Tail Canard Pods Engine Cowl Boattail	Drag	.0077 .0022 .0034 .0000 .0008 .0012 .0000 .0000 .0000	Induced Alpha 0.0 2.0 3.0 4.0 5.0 6.0 8.0 10.0 12.0	Drag Cl 0.000 0.098 0.148 0.199 0.251 0.303 0.408 0.514 0.618	0.0288 0.0322 0.0365 0.0427 0.0507 0.0606 0.0861 0.1193 0.1601 0.2352	0.0 3.0 4.1 4.7 4.9 5.0 4.7 4.3 3.9	0.000 016 024 032 040 049 067 086 104 132	0.00 0.45 0.45 0.45 0.46 0.46 0.46 0.46	0.051 0.030	

## 1995 STOVL Propulsion

PHYSICAL .	ATTRIBUTES	HC	VER PERFO		T. 777	
ESF = WEIGHT = LENGTH = DIAM =	1.336 5069.139 16.875 3.895		T = 3 T/W = TLOW = SFC =	RY 5650. 7.033 462. 0.778 0.000	WET 35650. 7.033 462. 0.778 0.000	lb/hr lb/(lb-hr)
POWER	MACH	ALT (ft)	THRUST (1b)	SFC	FFLOW (lb/hr)	WAF (lb/sec)
100.0 100.0 87.5 75.0 62.5 50.0 37.5 25.0	0 0.000 0 0.000 0 0.000 0 0.000 0 0.000 0 0.000	0.0 0.0 0.0 0.0 0.0 0.0 0.0	56610. 35731. 31265. 26798. 22332. 17866. 13399. 8933. 4466.	1.770 0.754 0.731 0.701 0.661 0.655 0.646 0.629 0.690	100199.9 26941.4 22860.2 18778.9 14756.1 11709.2 8662.3 5615.3 3082.4	421. 421. 387. 357. 328. 279. 240. 209. 136.
100.0 100.0 87.5 75.0 62.5 50.0 37.5 25.0	0 0.600 0 0.600 0 0.600 0 0.600 0 0.600 0 0.600	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	21249. 11144. 9751. 8358. 6965. 5572. 4179. 2786. 1393.	1.936 0.829 0.811 0.787 0.777 0.779 0.783 0.821 0.958	41137.7 9238.4 7909.4 6580.4 5411.4 4341.0 3270.6 2286.5 1334.4	421. 421. 393. 367. 330. 291. 259. 215. 176.
100.0 100.0 87.5 75.0 62.5 50.0 37.5 25.0	0 0.900 0 0.900 0 0.900 0 0.900 0 0.900 0 0.900 0 0.900	30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0 30000.0	26989. 13775. 12053. 10331. 8609. 6887. 5165. 3444. 1722.	1.948 0.944 0.934 0.922 0.926 0.955 1.002 1.116 1.503	52578.4 12998.9 11262.0 9525.1 7972.4 6574.2 5176.0 3844.7 2588.3	421. 421. 395. 372. 340. 304. 274. 237. 198.
100.0 100.0 87.5 75.0 62.5 50.0 37.5 25.0	0 1.500 0 1.500 0 1.500 0 1.500 0 1.500 0 1.500 0 1.500	50000.0 50000.0 50000.0 50000.0 50000.0 50000.0 50000.0 50000.0	19328. 9498. 8311. 7124. 5936. 4749. 3562. 2375. 1187.	2.019 1.116 1.099 1.090 1.077 1.098 1.153 1.267	39013.8 10596.0 9130.6 7762.9 6395.3 5216.4 4107.5 3008.8 2036.2	421. 421. 397. 371. 347. 313. 280. 250. 207.

## 1995 STOVL Weights

COMPONENT	POUNDS	KILOGRAMS	PERCENT
AIRFRAME STRUCTURE WING FUSELAGE HORIZONTAL TAIL VERTICAL TAIL REACTION CONTROL SYSTEM WING FOLD INTERNAL BAY STRUCTURE ALIGHTING GEAR	112. 150. 600. 1613.	5318. 1697. 1760. 394. 343. 51. 68. 272. 731.	25.33 8.08 8.39 1.87 1.64 0.24 0.32 1.30 3.48
PROPULSION ENGINES (1) FUEL SYSTEM	7040. 5586. 1454.	3194. 2534. 659.	
AVIONICS INSTRUMENTATION DE-ICE/AIR CONDITION AUXILIARY GEAR FURNISH. + EQPT. FLIGHT CONTROLS	INCLUDE TECH 672. 544. 1652. 94. 610. 200. 375. 1462.	FACTOR=0.85) 305. 247. 749. 43. 277. 91. 170. 663.	1.45 1.18 3.57 0.20 1.32 0.43 0.81 3.16
PAYLOAD FLIGHT CREW ( 1) ARMAMENT AMMUNITION LONG RANGE MISSILES LRM PYLONS & LAUNCHERS SHORT RANGE MISSILES SRM LAUNCHERS EXTERNAL TANKS	287.	1974.	9.40 0.39 1.32 0.62 4.27 1.51 0.86 0.43 0.00
TOTAL WEIGHT	46276.	20991.	100.00

## **Appendix B – SSF DOC Mission Definitions**

Payload
2 Long-Range, Air-to-Air Missiles
2 Short-Range, Air-to-Air Missiles
Gun and Ammunition

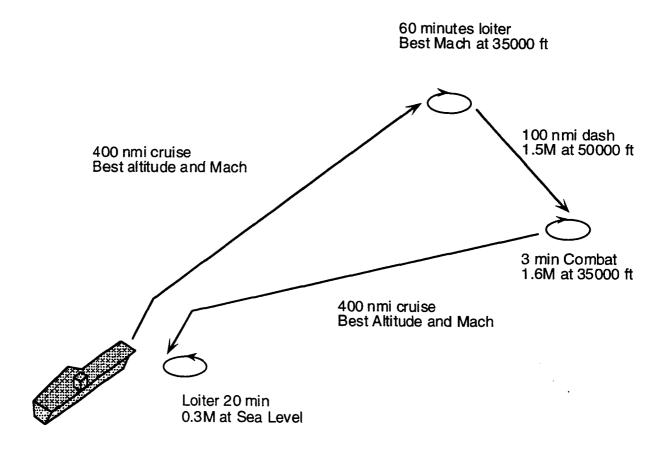


Figure B1. Combat Air Patrol fallout mission.

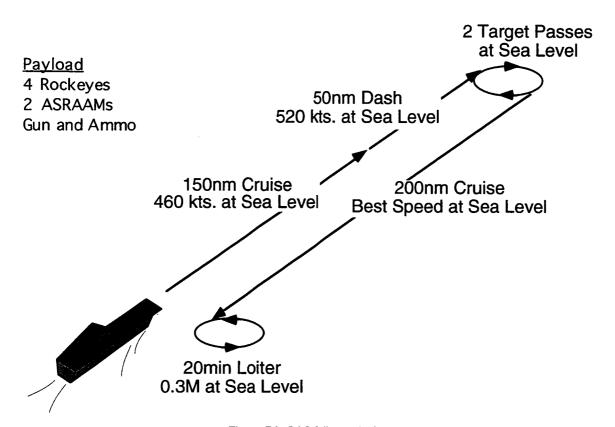


Figure B2. CAS fallout mission.

<u>Design Weapons Retained</u>
4 Long-Range, Air-to-Air Missiles
2 Short-Range, Air-to-Air Missiles
Gun and Ammo

1 min Combat at maximum A/B

300 nmi cruise
Best altitude at 1.5M

300 nmi cruise
Best Altitude and Mach

Loiter 20 min
0.3M at Sea Level

Figure B3. Deck Launched Intercept fallout mission.

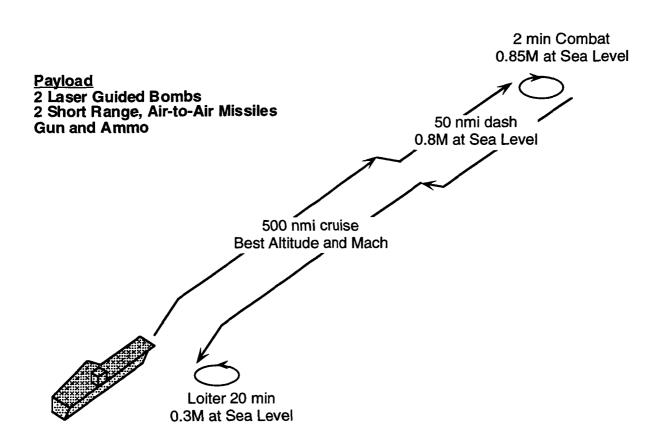


Figure B4. Interdiction fallout mission.

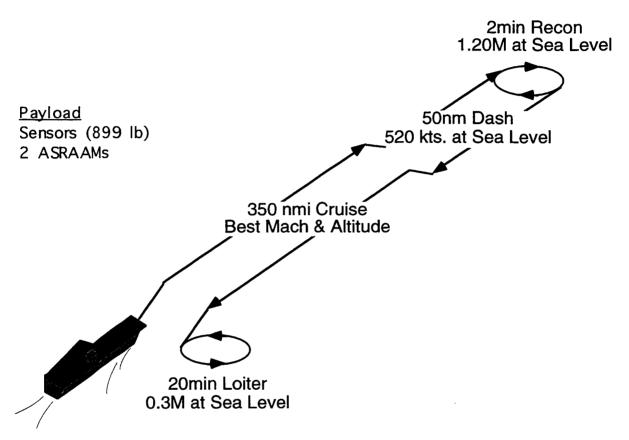


Figure B5. Reconnaissance fallout mission.

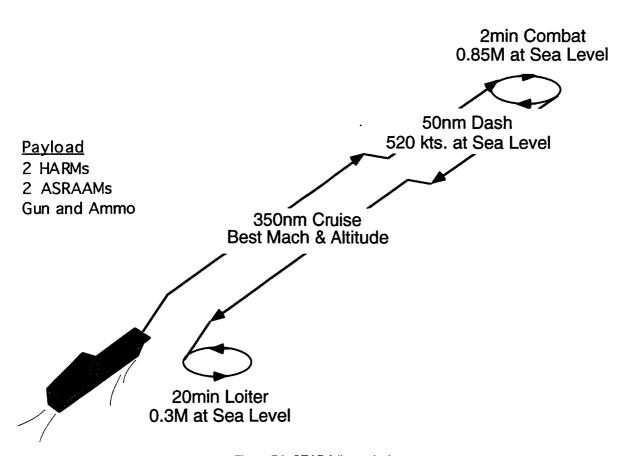


Figure B6. SEAD fallout mission.

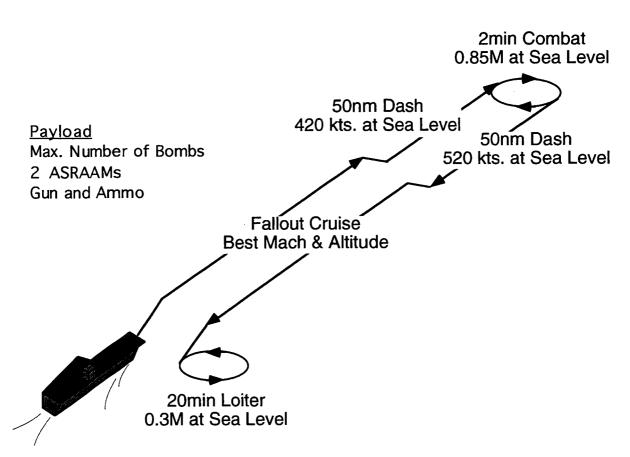


Figure B7. Strike fallout mission.

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classes of tactical naval aircraft aircraft classes. This study use comparative studies require "n different methods and database with consistent methods which analysis trends. The multimiss requirements. This compariso the Short Takeoff and Vertical The subsonic attack aircraft ev	ft, including subsonic as ed an approach that wan normalizing" aircraft the es. All aircraft were even hallow the aircraft to be sion aircraft were compon highlights the effect Landing (STOVL) airc valuation compared fly	attack, supersonic fighters internally consistent at are developed by different additional attack in two technologies directly compared in pared to evaluate the effect of changing technology craft and addresses the	ferent design groups using ogy timeframes and were sized operational utility or cost fect of technology and mission of an and mission requirements on impact of aircraft navalization. al designs, one- versus two-

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